

# R&D Activities for ARES Upgrade

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*High Energy Accelerator Research Organization (KEK)*

## < Outline >

1. R&D programs for SuperKEKB
2. L-band HOM-load test stand
3. Input couplers with TiN coating
4. New copper electroplating for S-cav
5. Summary

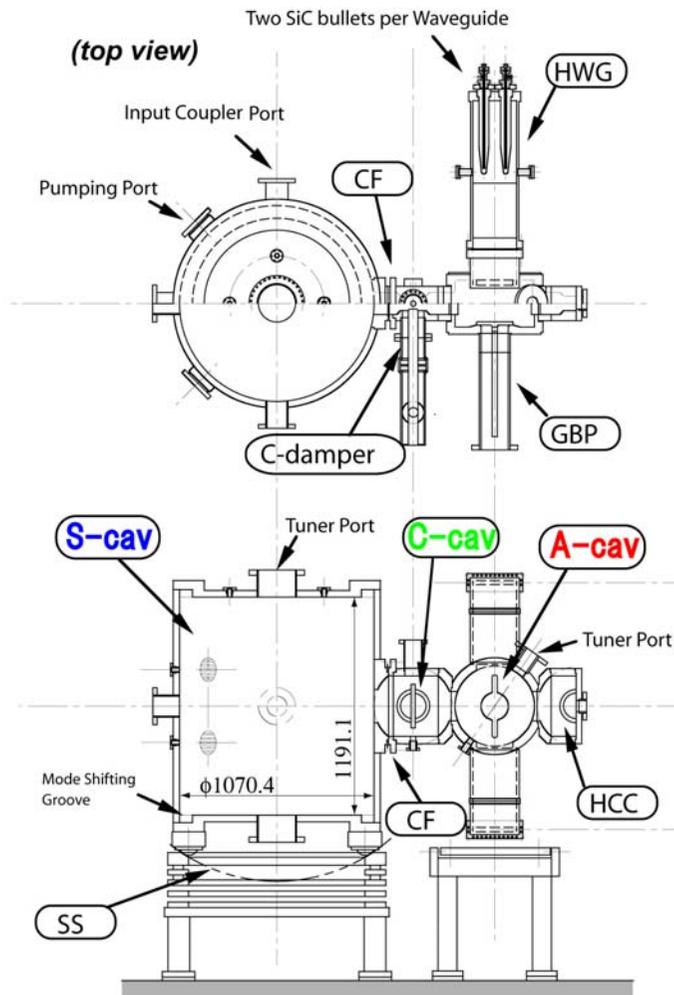
*KEKB Review*

*@KEK*

*2005.02.22*

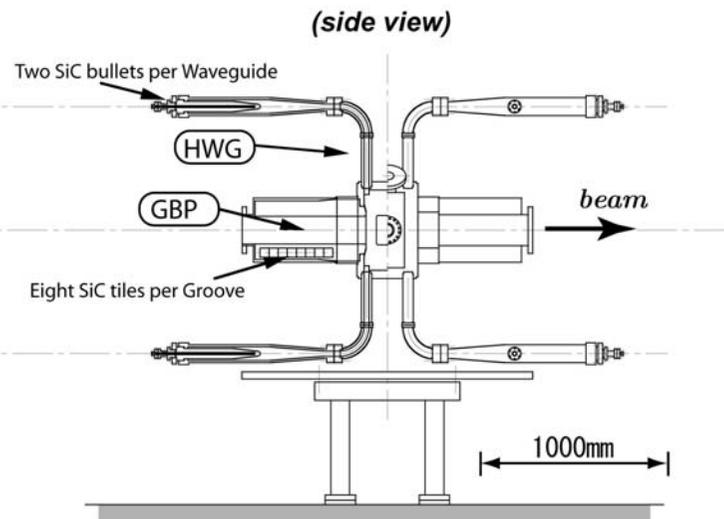
# Accelerator Resonantly-coupled with Energy Storage

## 3-cavity system stabilized with the $\pi/2$ -mode operation



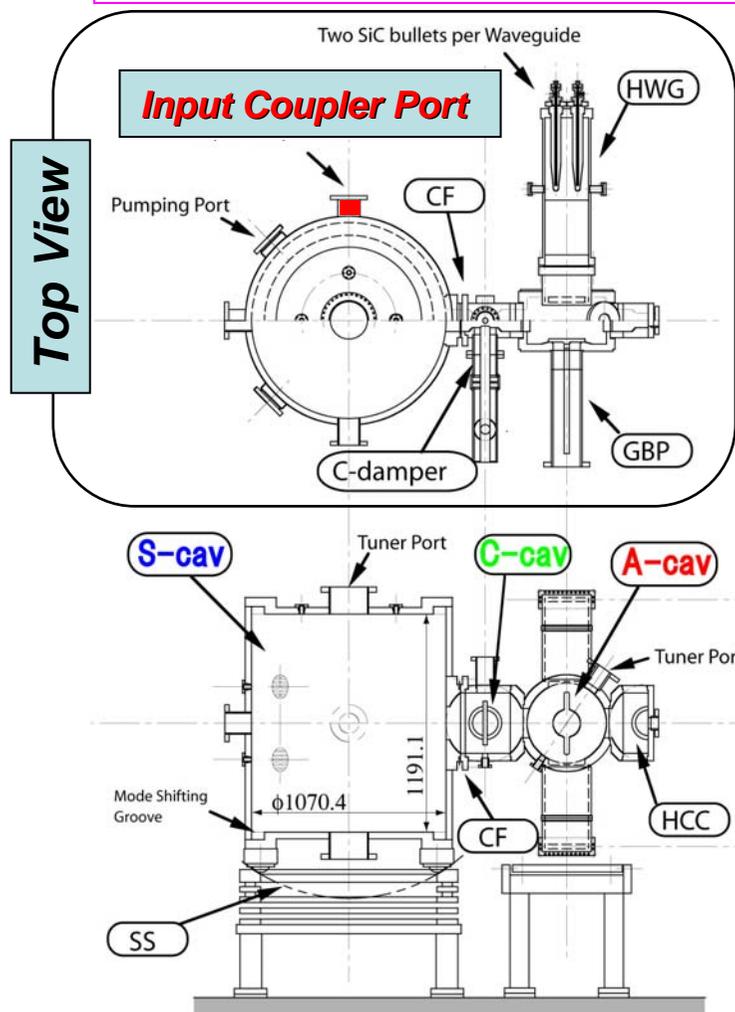
consists of

- HOM-damped accelerating cavity (**A-cav**)
- Energy-storage cavity with  $TE_{013}$  (**S-cav**)
- Coupling cavity (**C-cav**)  
with a parasitic-mode damper



# Accelerator Resonantly-coupled with Energy Storage

## 3-cavity system stabilized with the $\pi/2$ -mode operation



consists of

- HOM-damped accelerating cavity (**A-cav**)
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# Upgrade Items toward



*Measures against*

## **Larger detuning**

- Increase the energy ratio:  $U_s/U_a = 9 \rightarrow 15$ .
- Reported in the previous KEKB review
- Skipped this time

$$\Delta f_{\pi/2} = \frac{\Delta f_a}{1 + U_s/U_a}$$

## **Higher HOM powers**

- HOM-load upgrade

## **Higher input RF powers** (400kW/cav → 800kW/cav)

- TiN coating on the coaxial line
- Coupler test stand upgraded for ~800kW(CW)

## R&D Programs 2004(JFY)

### [1] Construction of a new **L-band HOM-load test stand**

- Using 1.25GHz klystron (1.2MW, CW)
- The 1<sup>st</sup> stage just finished

### [2] Input couplers **with TiN coating**

- Against multipactoring in the coaxial line
- TiN(Titanium Nitride) has low secondary-electron yields and is good for vacuum.
- Two couplers have been completed.
- Being tested in the **upgraded coupler test stand up to 800kW.**

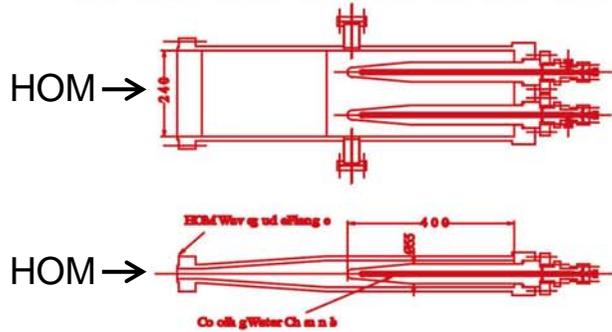
### [3] New **highly-pure copper electroplating** for **S-cav**

- The old facility has been retired.
- Reusing a facility being used for J-PARC.

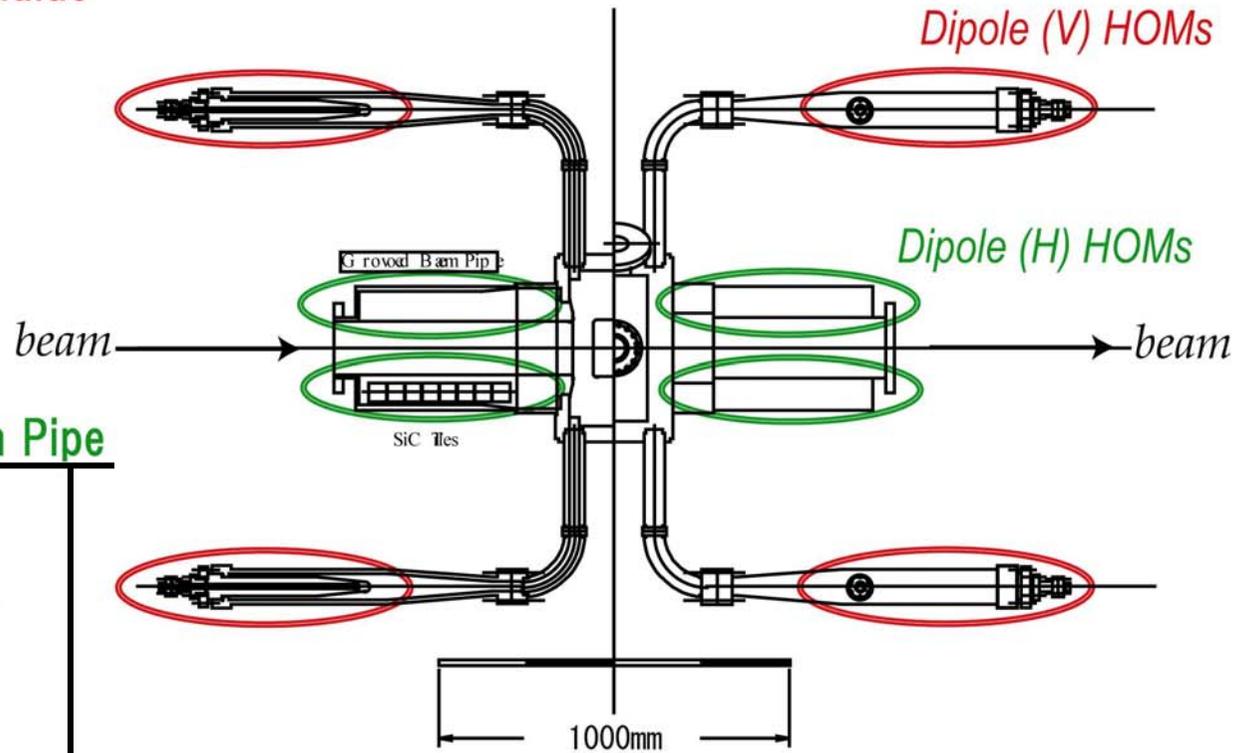
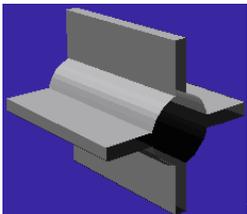
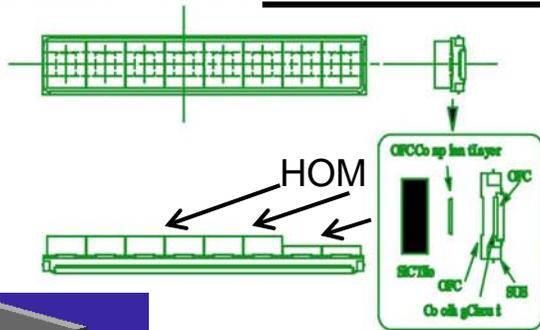
# [1] L-band HOM Test Stand

## ARES HOM-damped Structure

Two Bullet-shaped SiC-absorbers at the end of the HOM WaveGuide



SiC-tiles in the Grooved Beam Pipe



(Side view)

# SiC Absorbers

## In the HOM Wave Guide (WG)

- Direct water cooling



- Limit: >26kW/cav (HPT)



## In the Grooved Beam Pipe (GBP)

- Indirect water cooling  
→ via the copper plate
- Limit: ~3.6kW/cav (HPT)



**Max. power which can be supplied by the old L-band klystron.**

# HOM Extrapolation for Super-KEKB LER

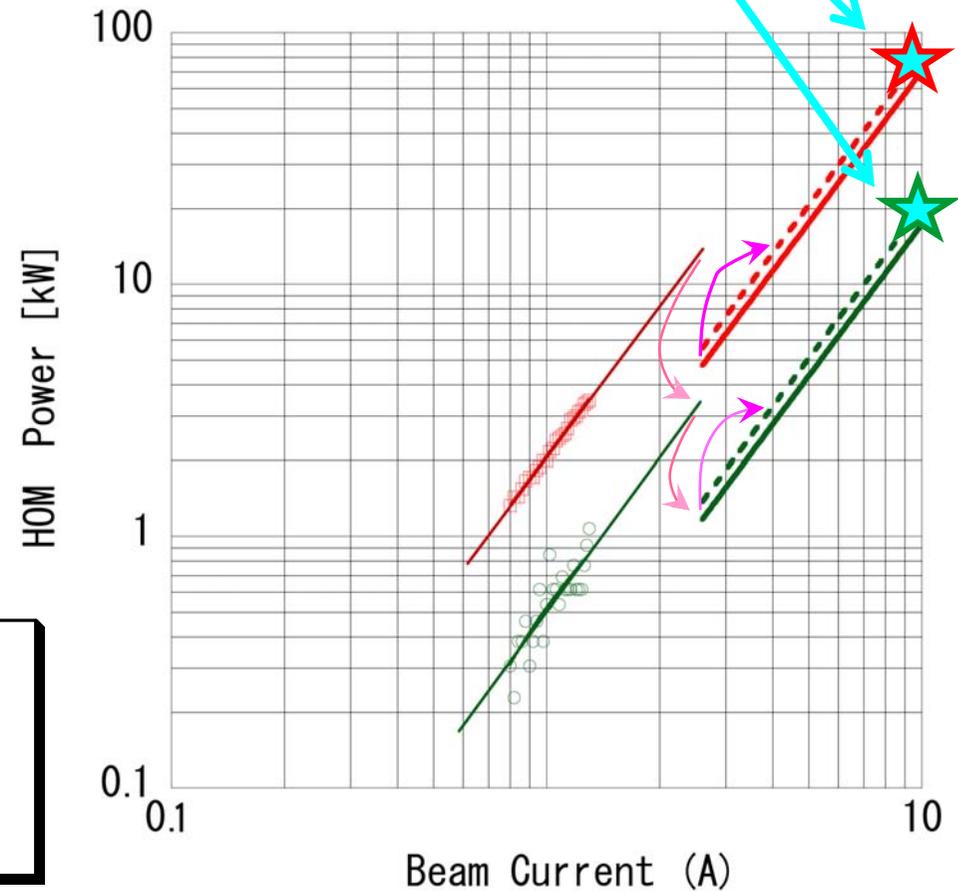
**HOM in WG load (LER):**  
**26kW/cav (HPT)**  
**→ 80kW/cav (SuperKEKB)**

- Need HPTs over 26kW
- Increase # of absorbers /WG
- Enhanced water cooling

**HOM in GBP load (LER):**  
**3.6kW/cav (HPT)**  
**→ 20kW/cav (SuperKEKB)**  
 → Need direct water cooling like in...

(KEKB)	(Super-KEKB)
Nb: 1224	→ 4896 (full)
$\sigma_z$ : 7mm	→ 3mm

○	2 x GBP (Nb=1224, BL=7mm)
—	2 x GBP (Nb=4896, BL=4mm)
- - -	2 x GBP (Nb=4896, BL=3mm)
□	4 x HOM WG (Nb=1224, BL=7mm)
—	4 x HOM WG (Nb=4896, BL=4mm)
- - -	4 x HOM WG (Nb=4896, BL=3mm)

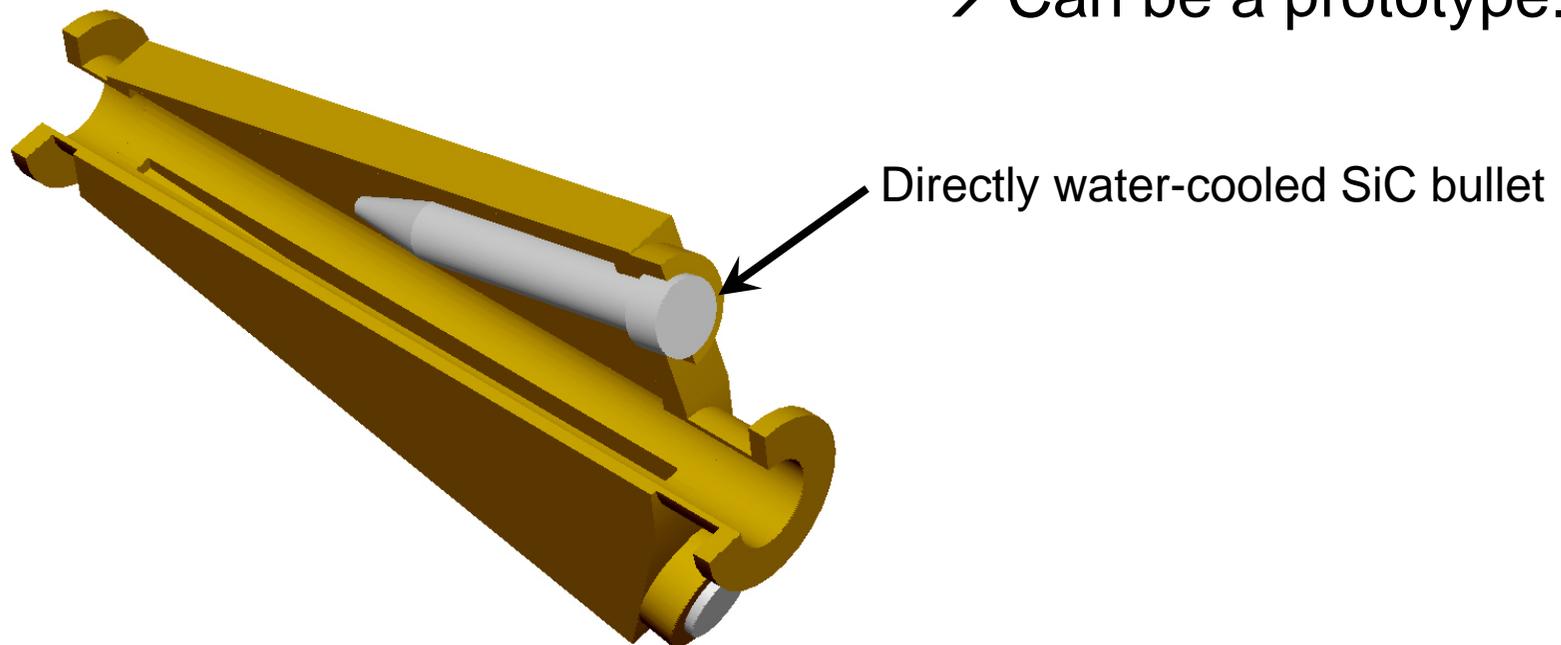


# Winged chamber loaded with SiC Absorbers

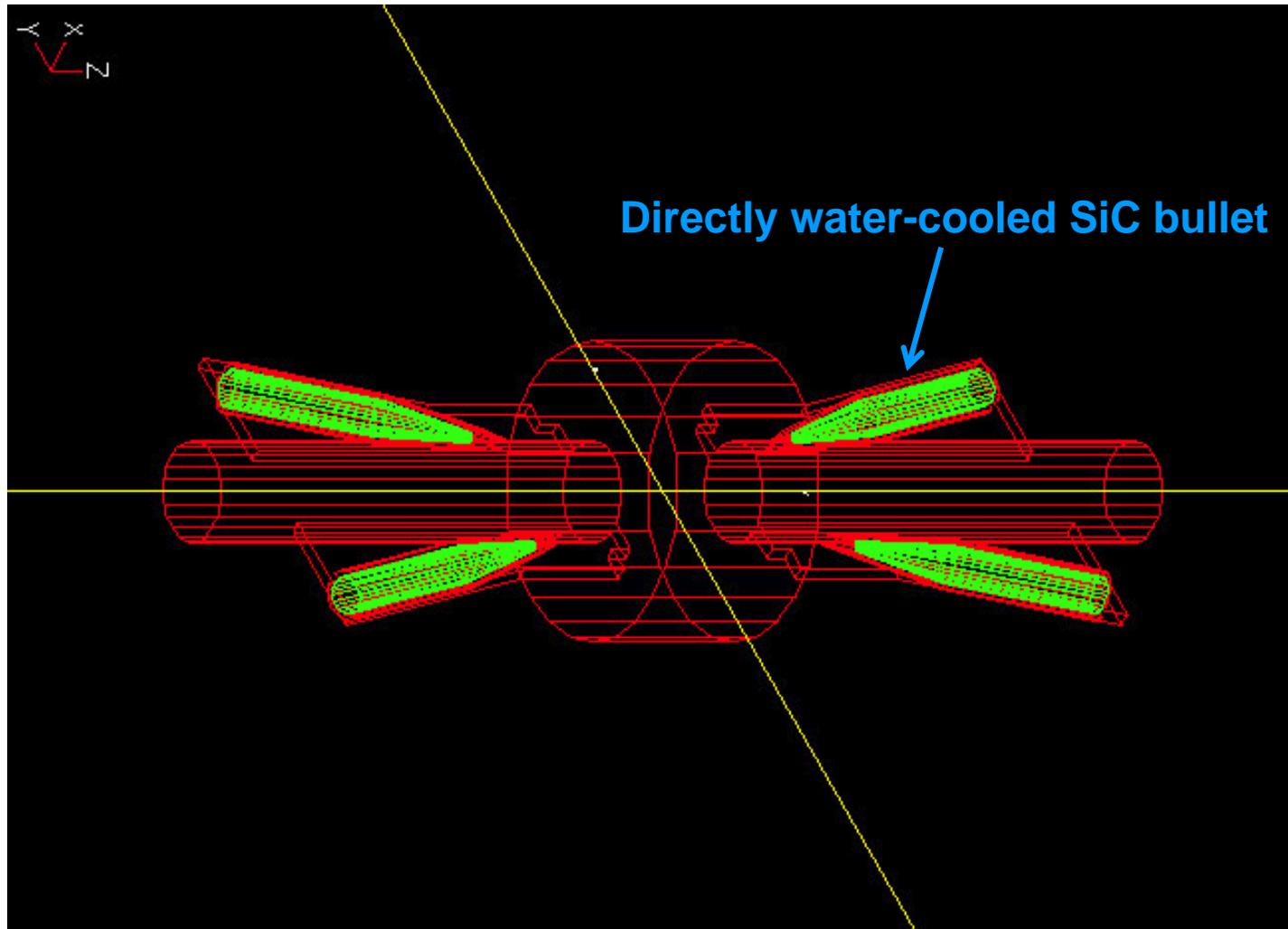
(used in the movable-mask sections)

Y. Suetsugu et al., "Development of Winged  
HOM Damper for Movable Mask in KEKB",  
Proc. PAC2003.

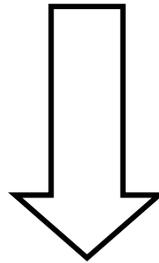
→ Can be a prototype.



# New A-cav Design with Winged Chambers



**We cannot test HOM loads with high powers  
for SuperKEKB.**

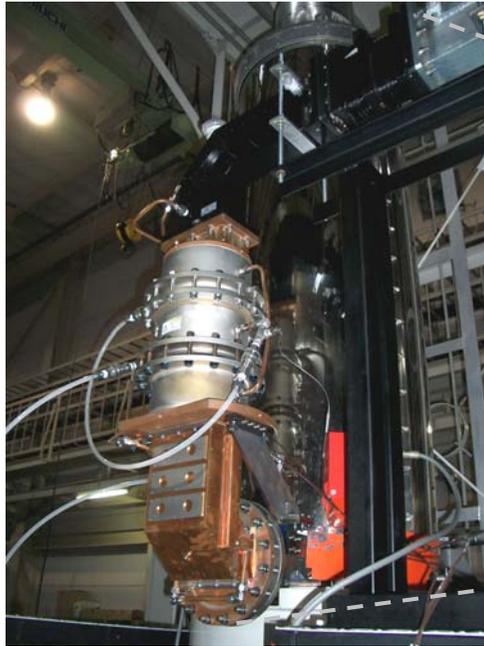


**More powerful klystron is needed  
to upgrade the HOM loads.**

# Construction of New Test Stand for the HOM-load Upgrade

- ✎ Reusing an L-band klystron, which is capable of 1.2 MW CW power ( freq. = 1.25 GHz).
- ✎ Operating conditions (HV & cooling system etc.) are going to be regulated for our purpose.
- ✎ The 1<sup>st</sup> stage of the construction has been just finished.

# D01C/ARES HOM-load Test Stand



Output from the klystron



L-band klystron

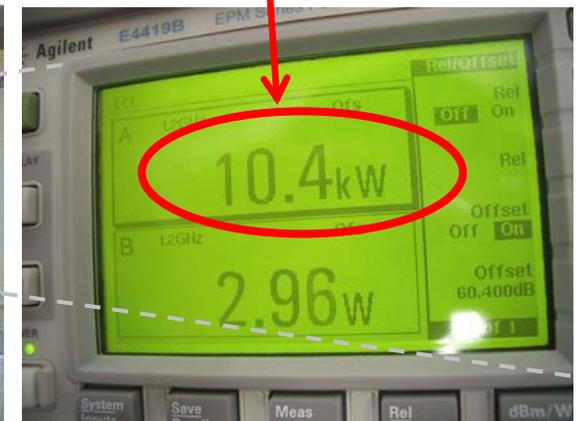
Water dummy load



# The 1<sup>st</sup> RF Power Comes!



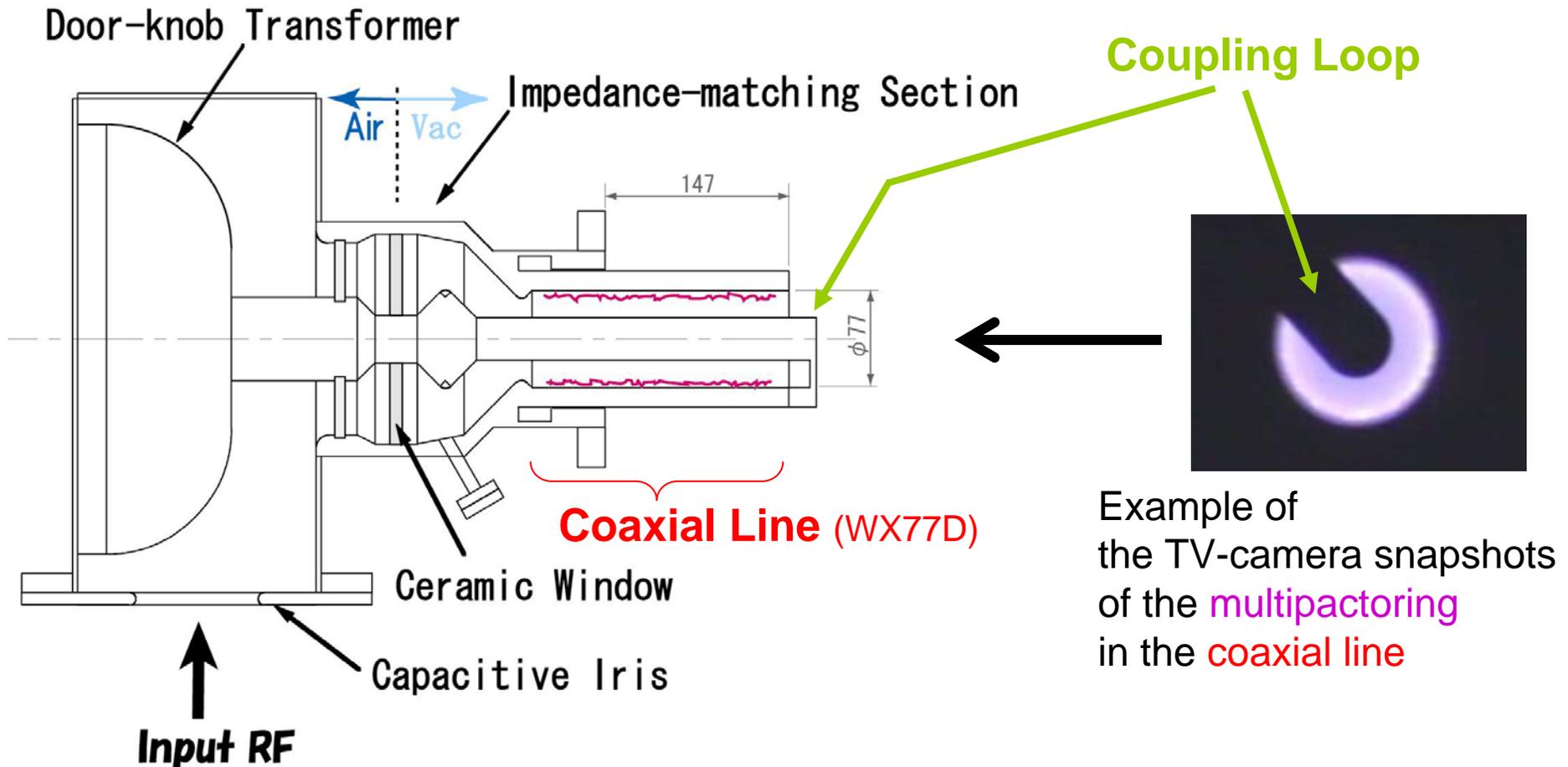
Output power beyond the max. obtained in the old L-band test stand (3.3kW)



→ *Tuning to deliver more RF power up to 100 kW*

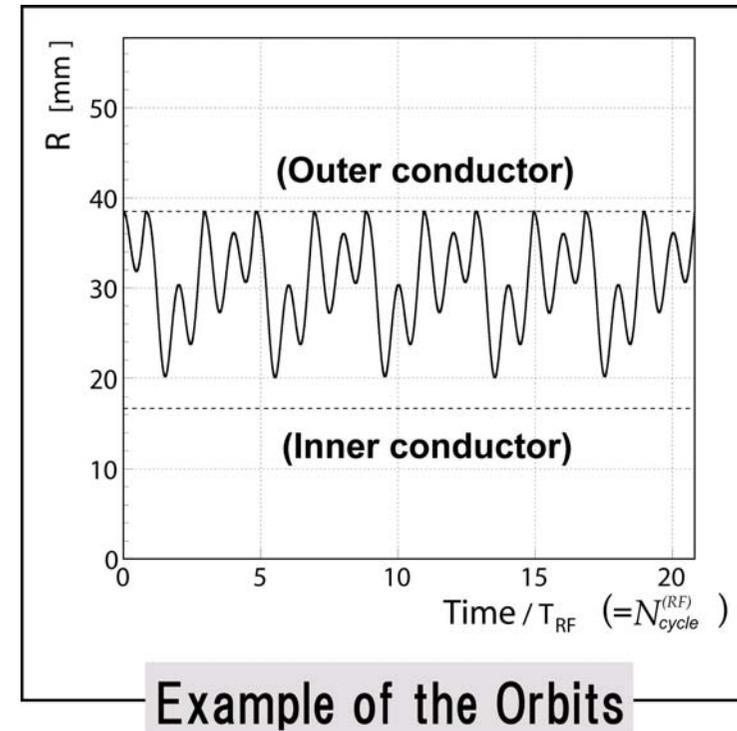
# [2] Input Couplers with TiN Coating

The problem is the *multipactoring* in the **coaxial line**.



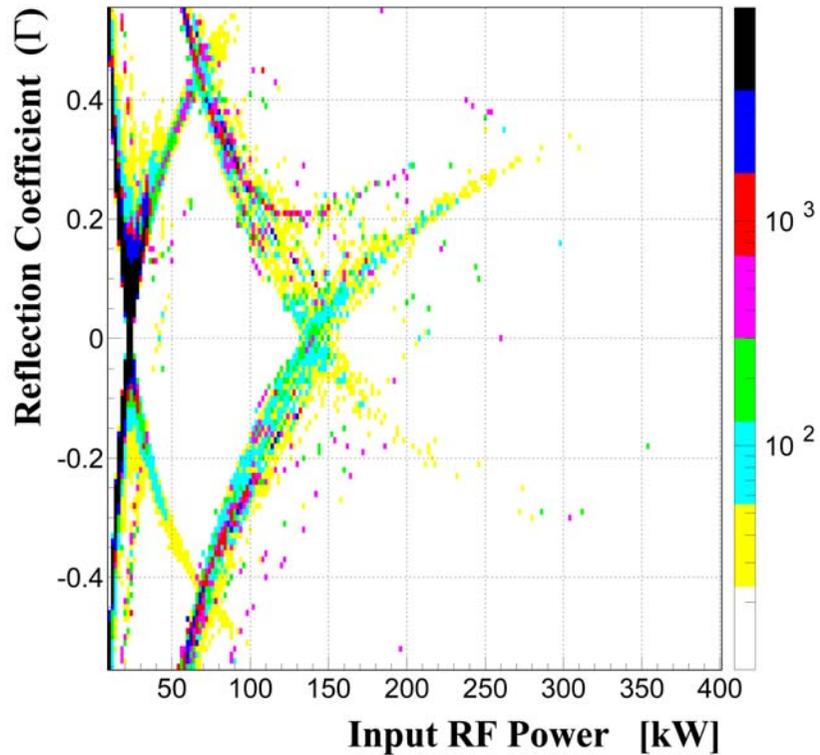
# Simulation Study

-  Solving eq. of motion with the Runge-Kutta method
-  Assuming the SEY of conditioned copper
-  Count number of collisions.

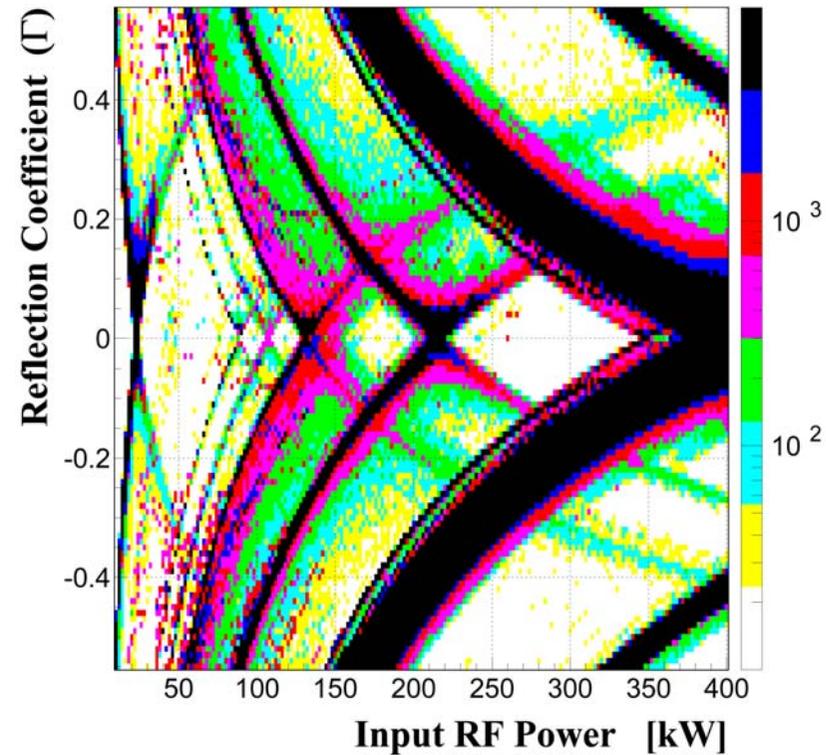


# On Which Side?

On the **inner** conductor

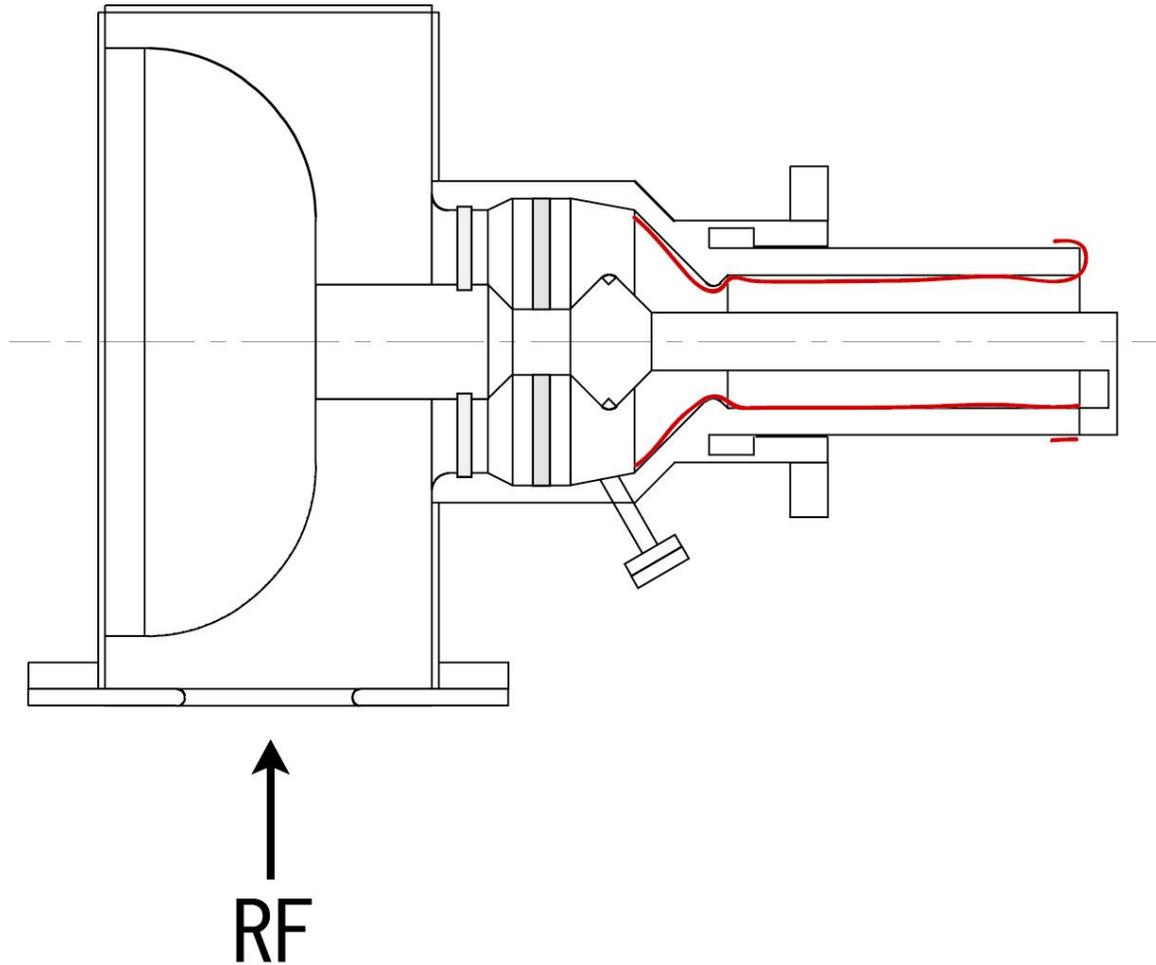


On the **outer** conductor



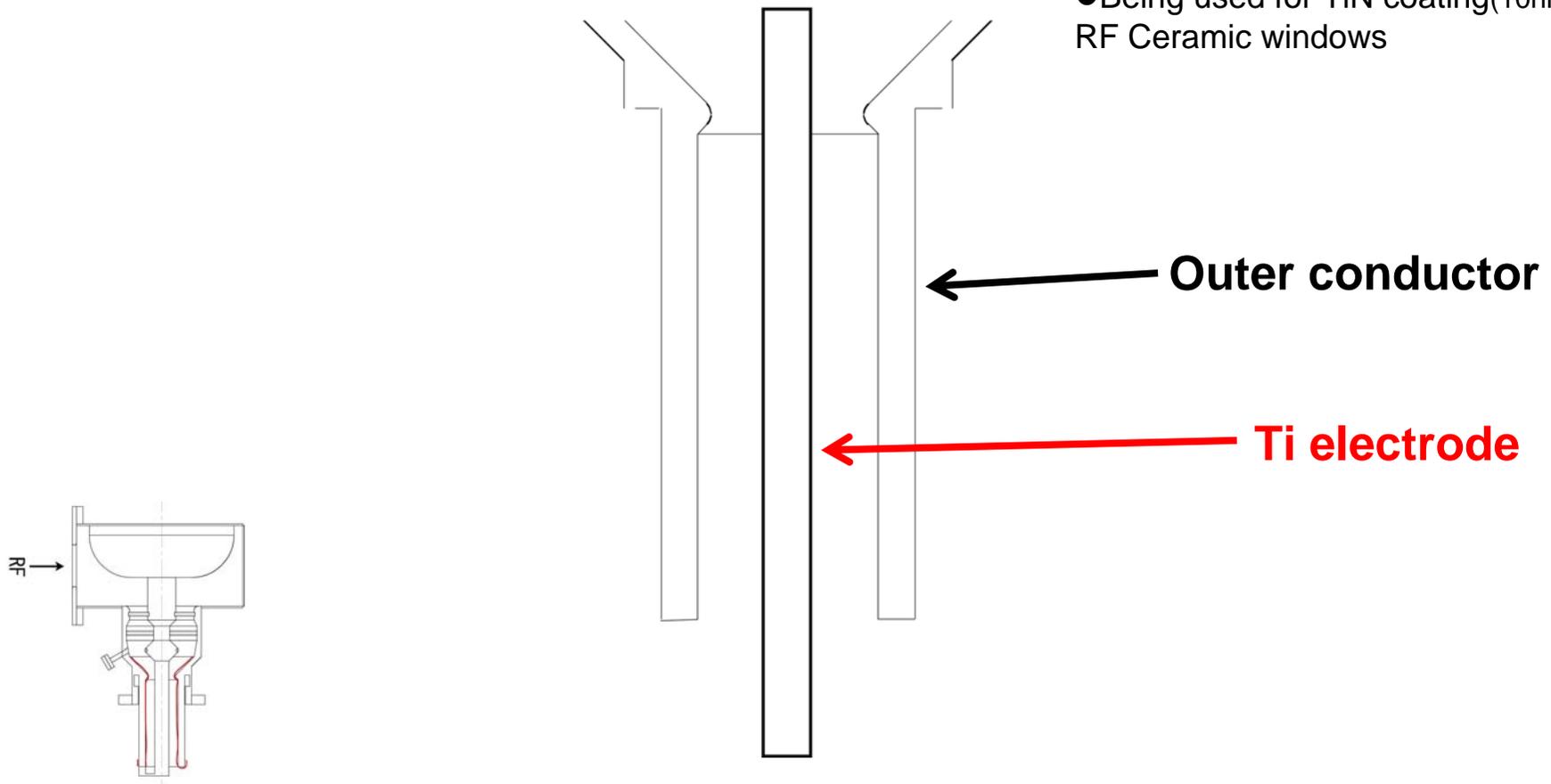
Almost **single-side** multipactoring on the **outer** conductor

## Coating Area



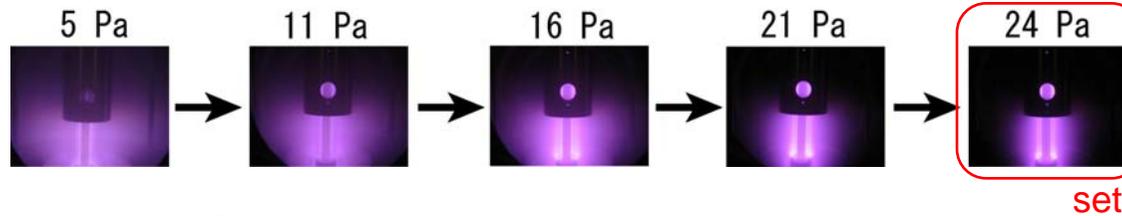
# Setup of the TiN Coating (DC Sputtering)

- $3\text{E-}4\text{Pa}$  before coating
- Injected gas: **Ar** and **N<sub>2</sub>**
- Being used for TiN coating(10nm) of RF Ceramic windows



# Studies on

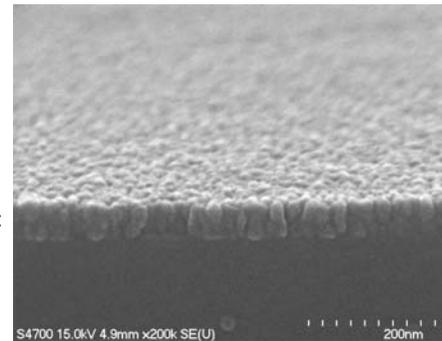
## Total gas pressure



## Gas mixture ratio (Ar:N<sub>2</sub>)

## Thickness meas. done by direct observation using SEM

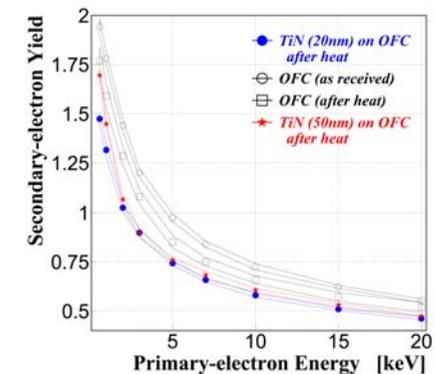
~50nm ⇕



← TiN coating

← Glass plate

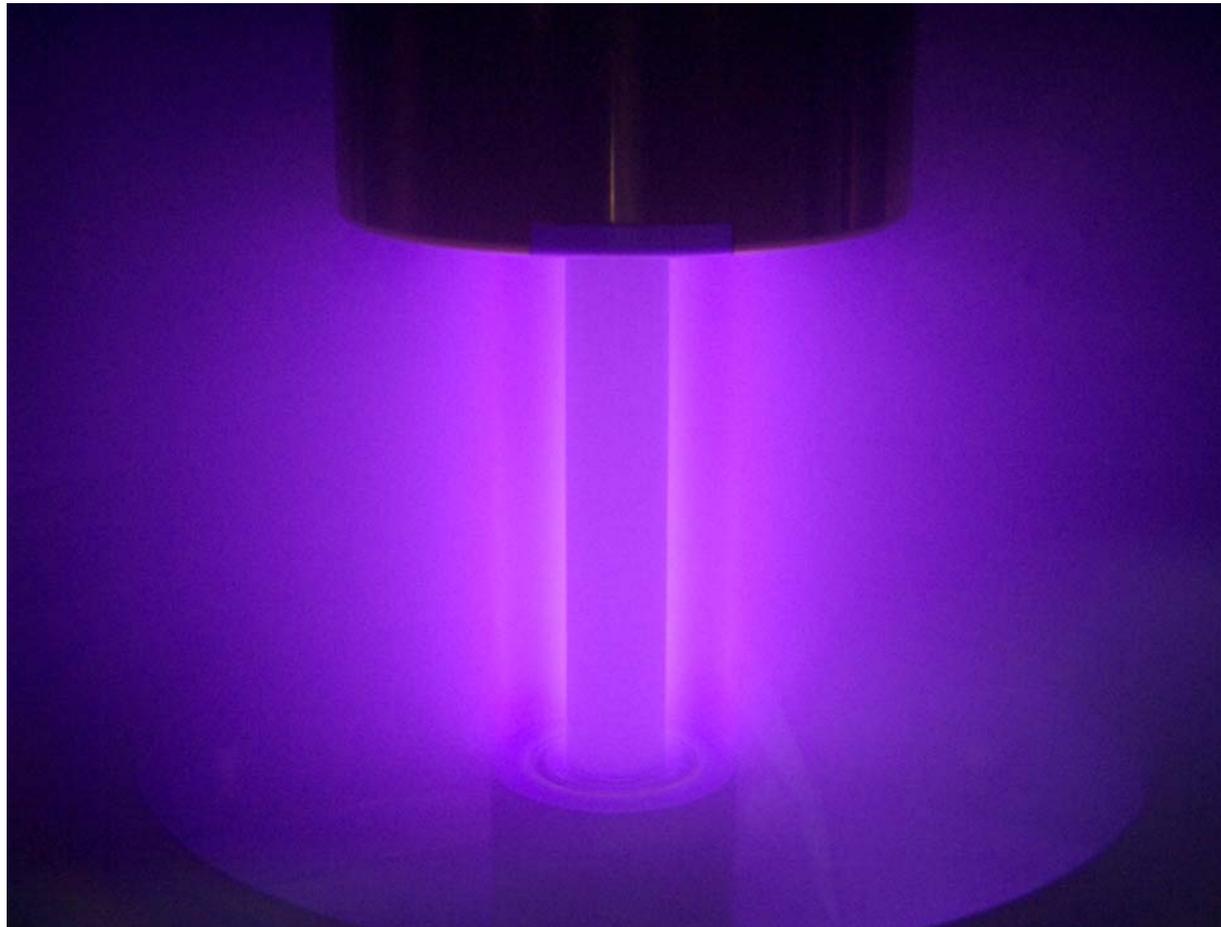
## Secondary electron yields



For the details, see the slides presented in the 6th Workshop on a Higher Luminosity B Factory:

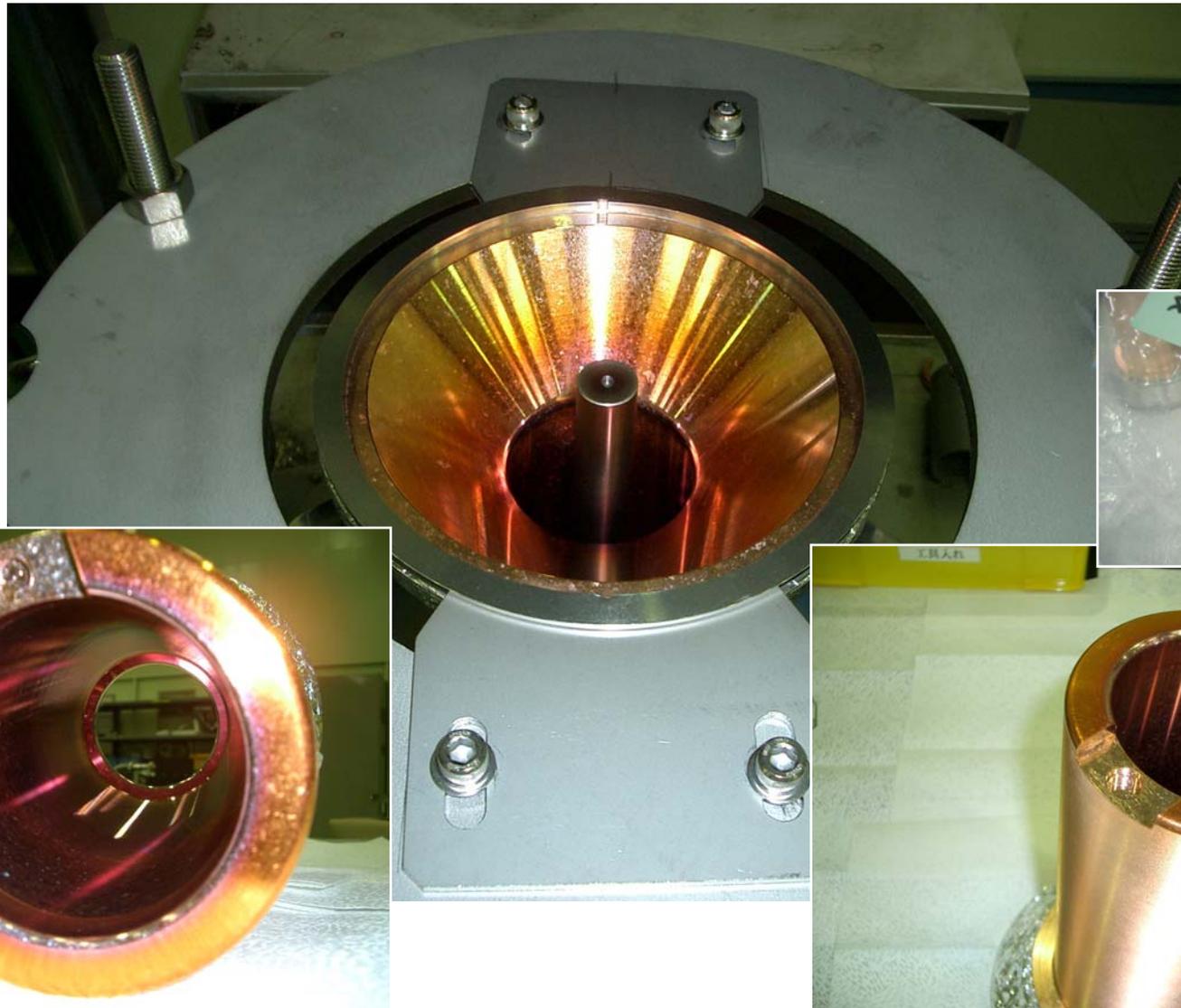
<http://belle.kek.jp/superb/workshop/2004/HL6/program.html> .

***Two input couplers have been TiN-coated  
with the final condition.***

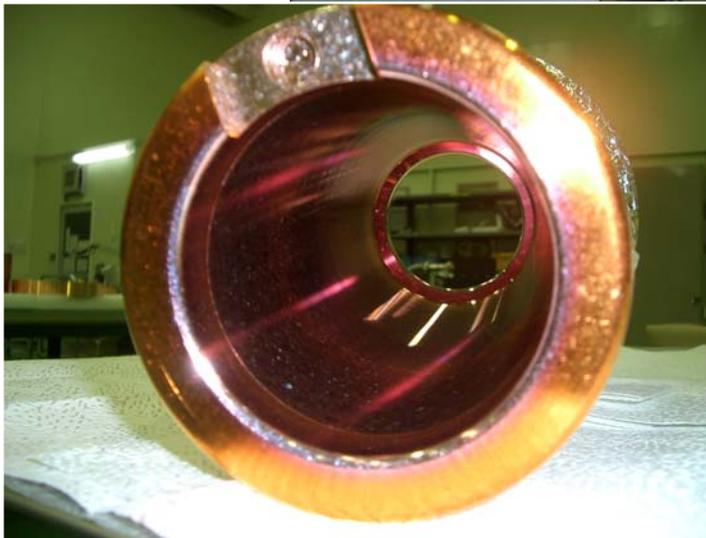


(taken on 2004.11.10)

# After Coating



Before coating



# Fabrication

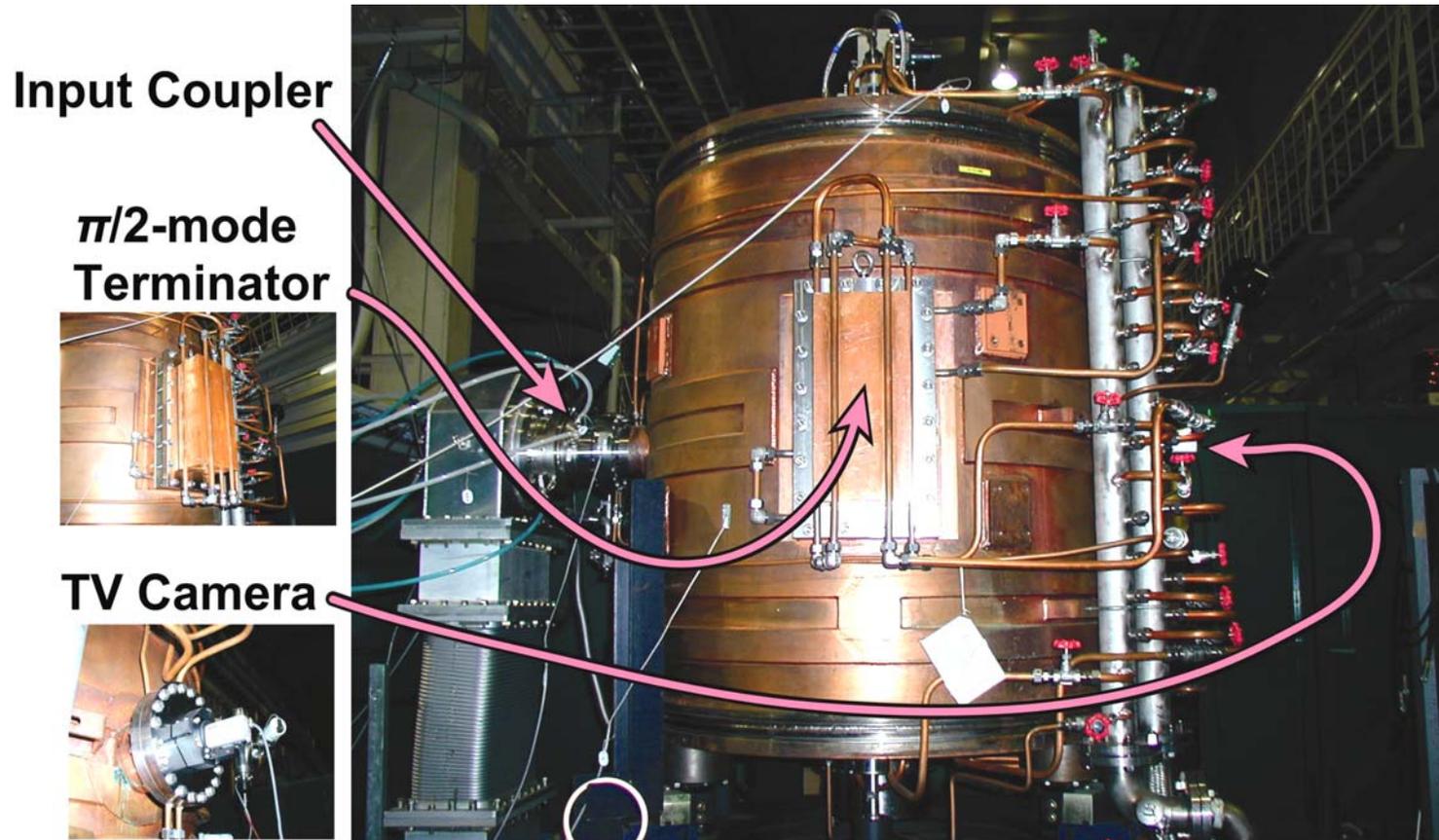


# Leak test



➔ Tested in the upgrade coupler test stand

# Old Setup of the Coupler Test Stand



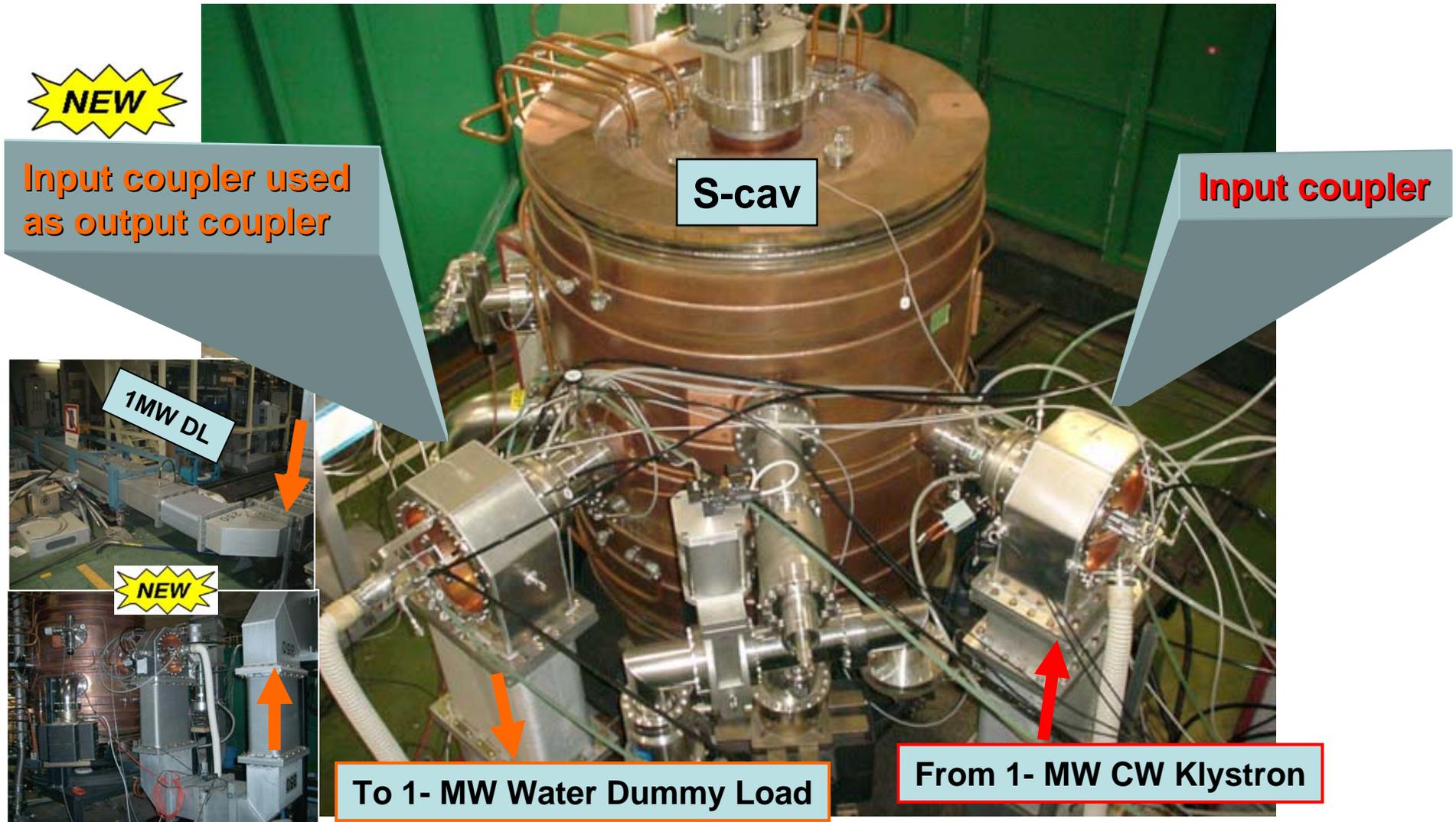
- **No RF output**

→ S-cav works as a dummy load.

→ Input powers are limited: <400kW.

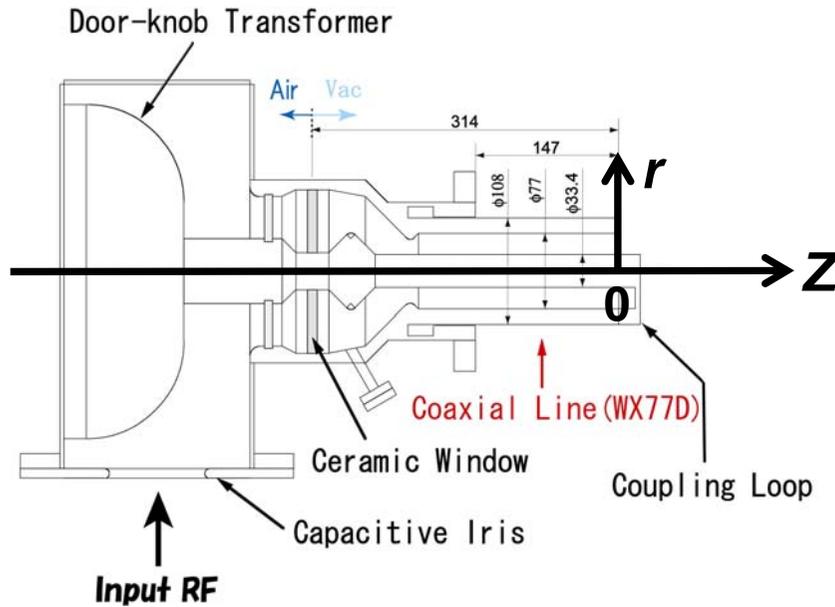
# Coupler Test Stand

## Upgraded for Higher Power Capability: 400→800kW



## Another characteristic:

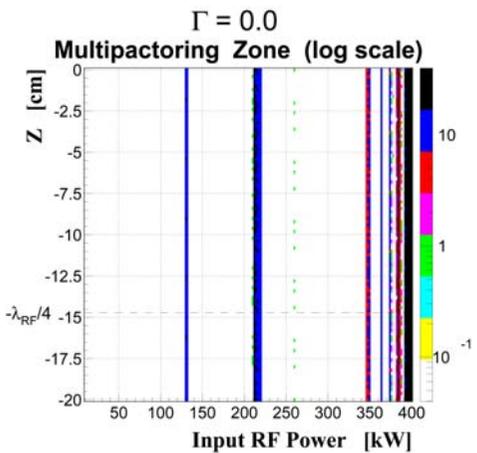
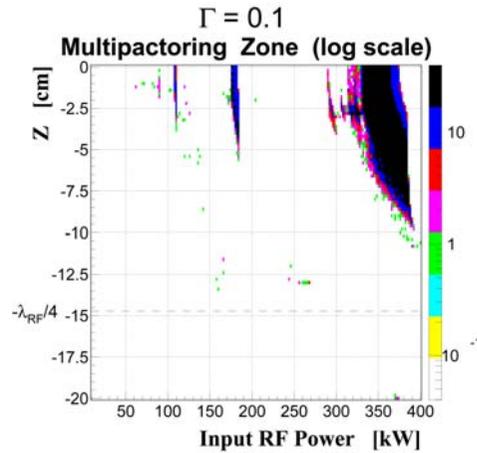
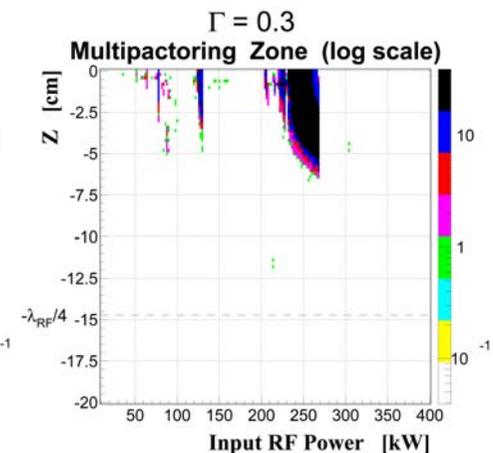
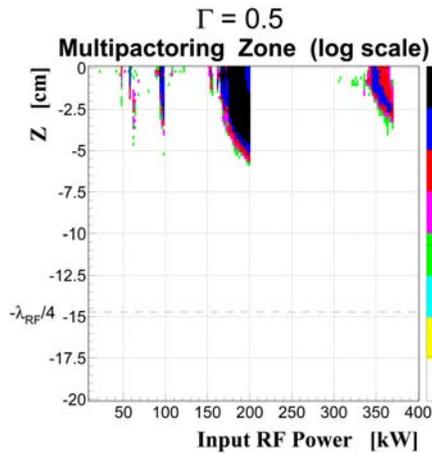
*The coupling-loop angles of the input and output couplers are set to be the same.*



→ No reflection ( $\Gamma \sim 0.0$ )

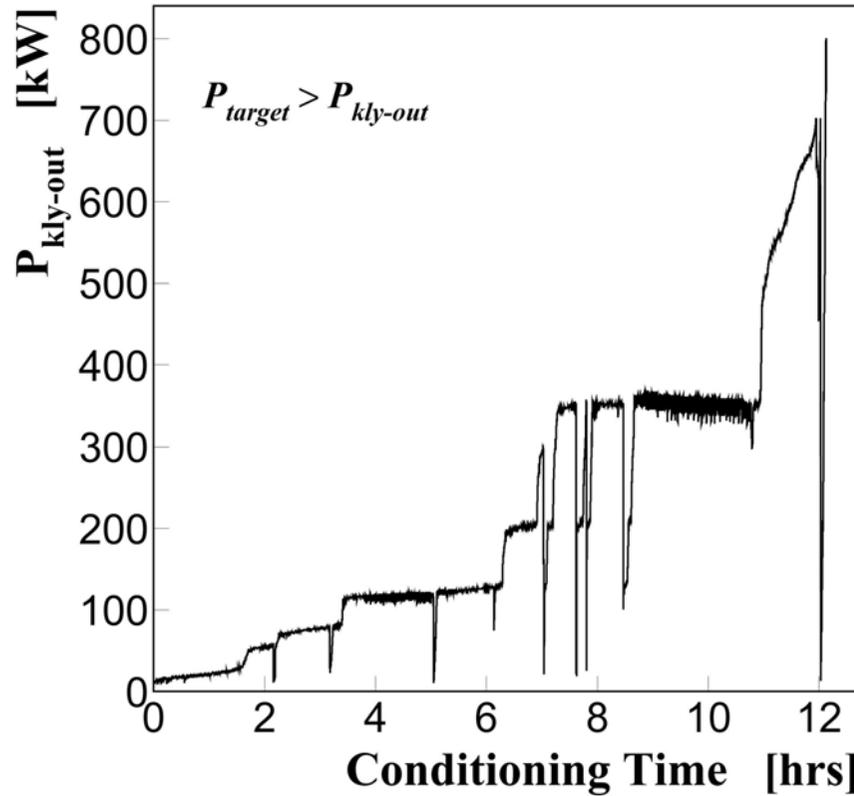
→ No Z-dependence

The hardest ordeal for couplers

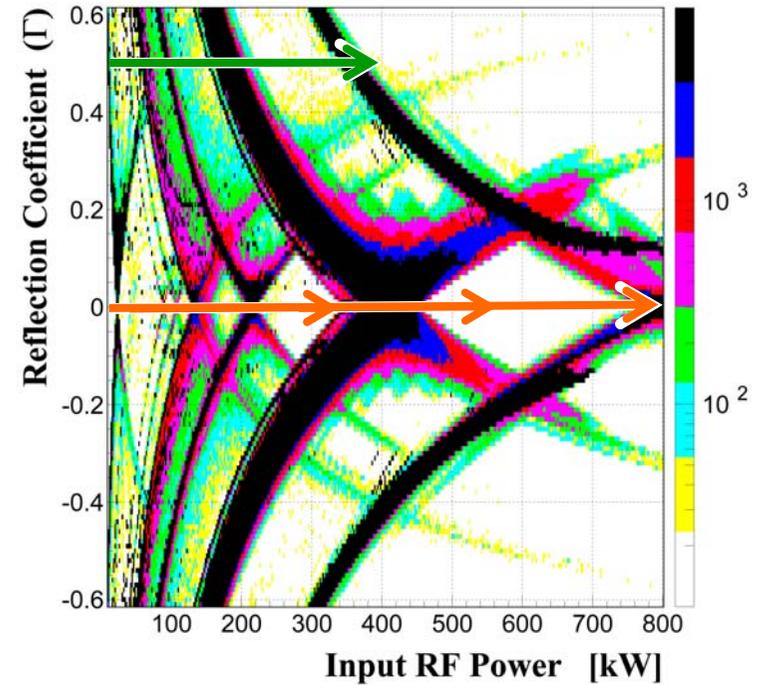


# Power History

(Data taken in 2005.02.01-10 @D01A/ARES TS)



Routes of the  $(\beta=3)$  **old** and  $(\beta=1)$  **upgraded** test stands



Any operating condition can be simulated in the test stand by changing the coupling-loop angles of the input and output couplers!

- To be compared with results on a coupler w/o TiN coating
- To be tested in the D04C station? (“genuine” test stand?)

# [3] New Copper Electroplating for S-cav

**S-cav is made from Iron with copper electroplating.**

✎ Present S-cav ---- **electroplating in a pyrophosphate bath**

- With brightener → little defect on the surface
- The facility has been retired.

✎ S-cav for SuperKEKB ---- **new electroplating in an acid sulfate bath performed in the periodic reverse (PR) process**

( H. Ino, et. al, "Advanced copper lining for accelerator components",  
Proc. of LAC2000, Monterey, CALIFORNIA, 1015 (2000) )

- Without brightener → high purity, high electric conductivity (102%IACS),  
but possible defects on the surface
- Using the facility being used for J-PARC

Ex. DTL tank



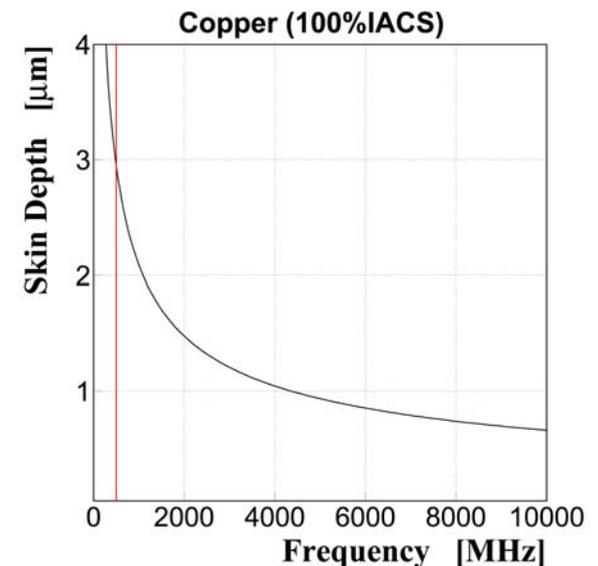
# Difference between J-PARC and SuperKEKB

- J-PARC case
  - Thickness: ~1mm → Mechanical polishing (-0.5mm) → Electrolytic Polishing (EP)
- SuperKEKB case
  - Thickness: ~0.2mm → Electrolytic Polishing (EP)



## Studies on

- **Thickness** (targets)
  - Ground(alkalinity): ~50 $\mu$ m
  - Main(acidity): ~150 $\mu$ m
  - Electrolytic Polishing: about -40 $\mu$ m
- **Less defect**
- **Electric performance**
  - Check  $Q_0$ .



# Pillbox Test Cavity

Diameter: 451.2mm  
Height: 260.0mm



(After copper electroplating)

Made from iron (SS400)



(Before copper electroplating)



# Theoretical Calculation of $Q_0$ (= $Q_0(\text{cal})$ )



## Analytical solution of the electromagnetic field in the pillbox cavity

TE<sub>mnp</sub> mode

$$\left\{ \begin{array}{l} E_r = A \frac{j\omega\mu_0}{k^2} \frac{m}{r} J_m \left( \frac{j'_{mn}}{b} r \right) \sin m\theta \sin \frac{p\pi z}{d} \\ E_\theta = A \frac{j\omega\mu_0}{k^2} \frac{j'_{mn}}{b} J'_m \left( \frac{j'_{mn}}{b} r \right) \cos m\theta \sin \frac{p\pi z}{d} \\ E_z = 0 \\ H_r = A \frac{1}{k^2} \frac{p\pi}{d} \frac{j'_{mn}}{b} J'_m \left( \frac{j'_{mn}}{b} r \right) \cos m\theta \cos \frac{p\pi z}{d} \\ H_\theta = -A \frac{1}{k^2} \frac{p\pi}{d} \frac{m}{r} J_m \left( \frac{j'_{mn}}{b} r \right) \sin m\theta \cos \frac{p\pi z}{d} \\ H_z = A J_m \left( \frac{j'_{mn}}{b} r \right) \cos m\theta \sin \frac{p\pi z}{d} \end{array} \right.$$

TM<sub>mnp</sub> mode

$$\left\{ \begin{array}{l} E_r = -A \frac{1}{k^2} \frac{p\pi}{d} \frac{j_{mn}}{b} J'_m \left( \frac{j_{mn}}{b} r \right) \cos m\theta \sin \frac{p\pi z}{d} \\ E_\theta = A \frac{1}{k^2} \frac{p\pi}{d} \frac{m}{r} J_m \left( \frac{j_{mn}}{b} r \right) \sin m\theta \sin \frac{p\pi z}{d} \\ E_z = A J_m \left( \frac{j_{mn}}{b} r \right) \cos m\theta \cos \frac{p\pi z}{d} \\ H_r = -A \frac{j\omega\varepsilon_0}{k^2} \frac{m}{r} J_m \left( \frac{j_{mn}}{b} r \right) \sin m\theta \cos \frac{p\pi z}{d} \\ H_\theta = -A \frac{j\omega\varepsilon_0}{k^2} \frac{j_{mn}}{b} J'_m \left( \frac{j_{mn}}{b} r \right) \cos m\theta \cos \frac{p\pi z}{d} \\ H_z = 0 \end{array} \right.$$



$Q_0(m,n,p)$

$$= \omega_{mnp} \frac{U}{P_{\text{wall}}}$$

$$\left\{ \begin{array}{l} U = \frac{\varepsilon_0}{2} \int_{\text{cavity}} dV |\vec{E}|^2 = \frac{\mu_0}{2} \int_{\text{cavity}} dV |\vec{H}|^2 \\ P_{\text{wall}} = \frac{1}{2} \sqrt{\frac{\omega\mu}{2\sigma}} \int_{\text{cavity}} dS |\vec{H}|^2 \end{array} \right.$$



Assuming

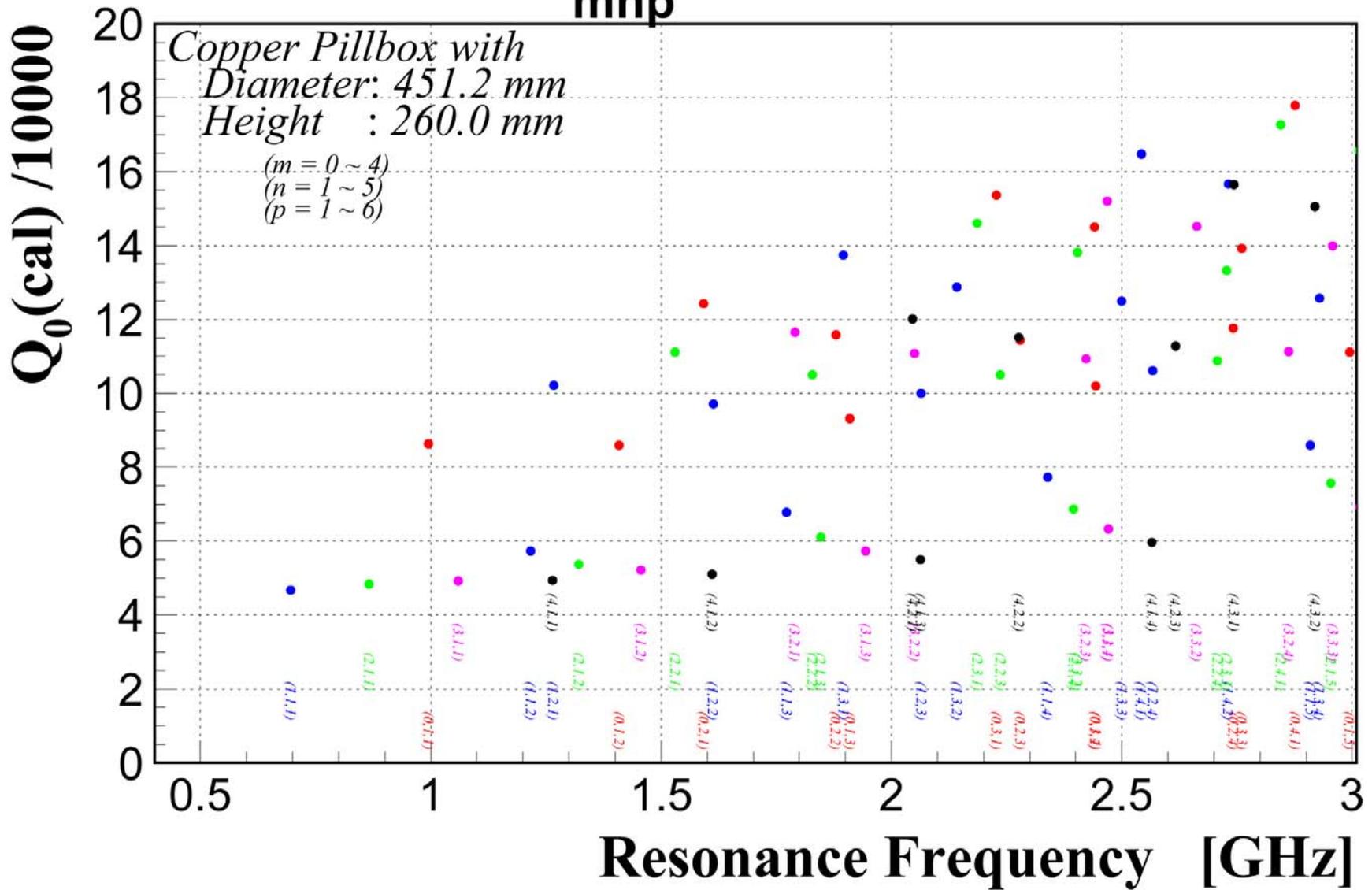
- **100% IACS** electric conductivity (=  $1/1.72\text{E-}8\Omega\text{m}$ )
- **flat surface** (i.e. no defect)

# IACS

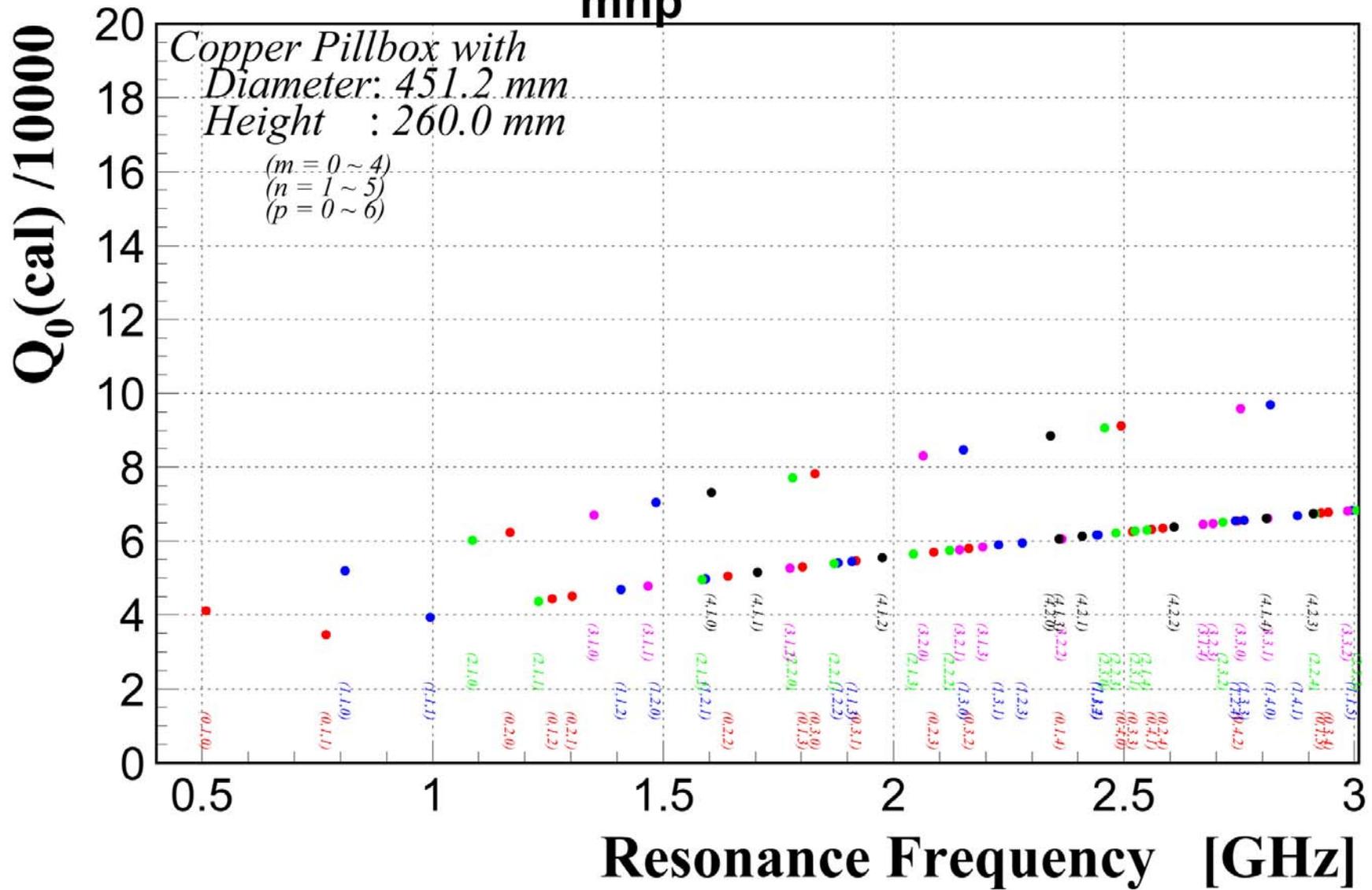
- International Annealed Copper Standard
- 100%IACS electric conductivity:  $1/1.72E-8\Omega m$
- The electric conductivity of the highest-class oxygen-free copper: 102%IACS

Cf. Electroplating in an acid sulfate bath w/o brightener: 102%IACS

# TE<sub>mnp</sub> Waves

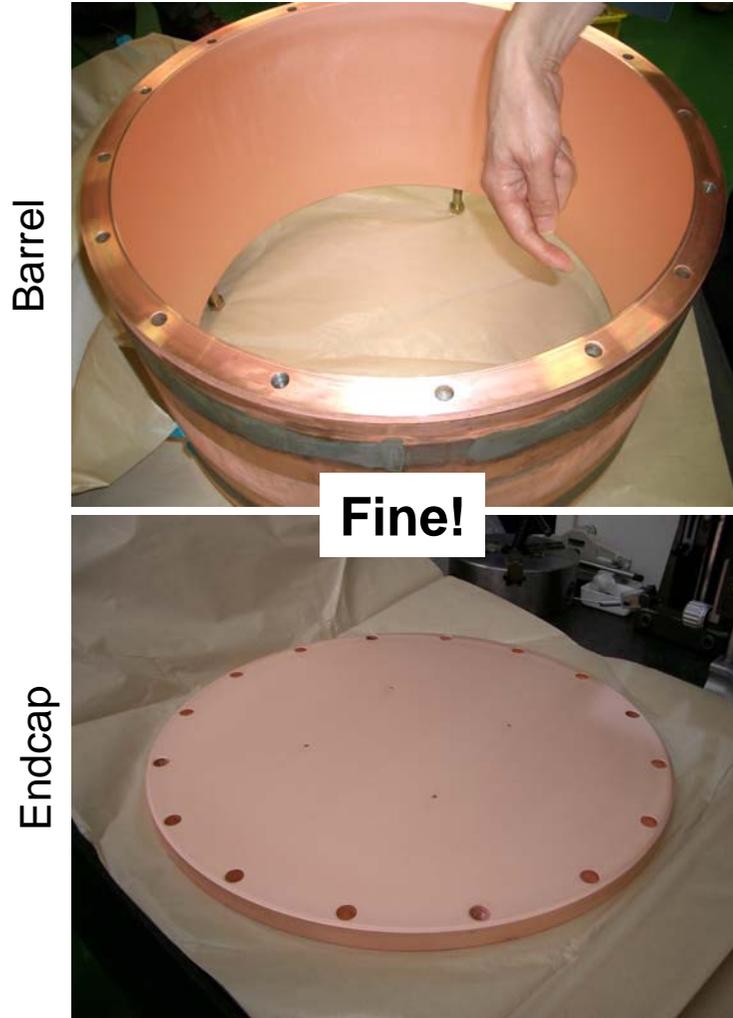


# TM<sub>mnp</sub> Waves



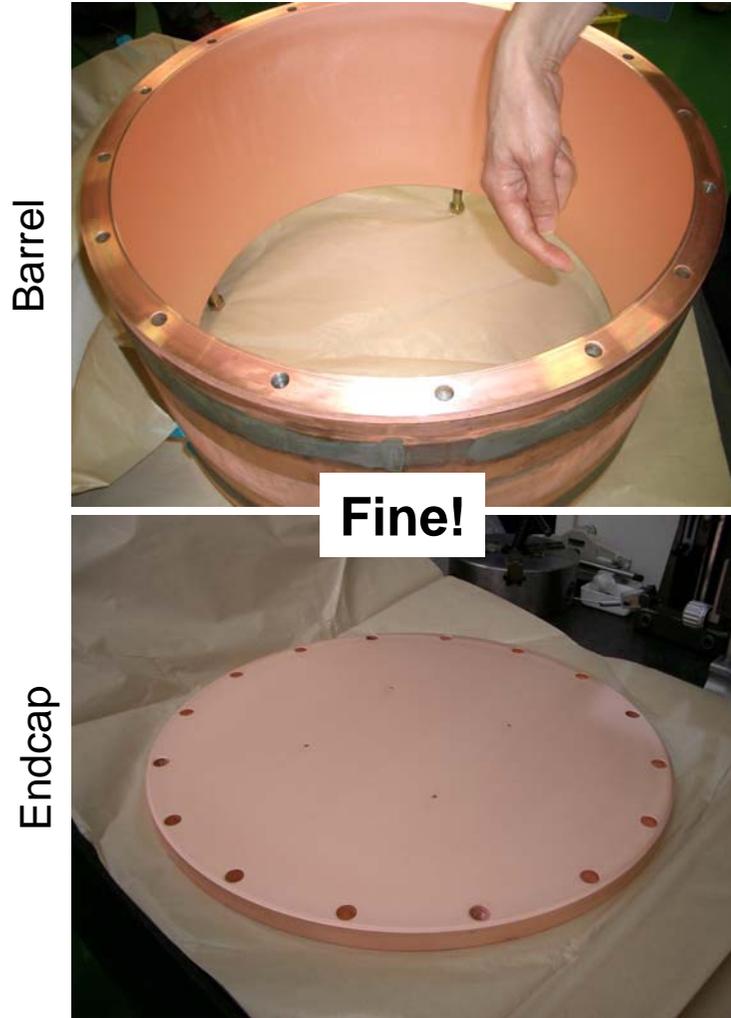
# After Trial and Error...

Copper Electroplating in an acid sulfate bath w/o brightener (PR process)



# After Trial and Error...

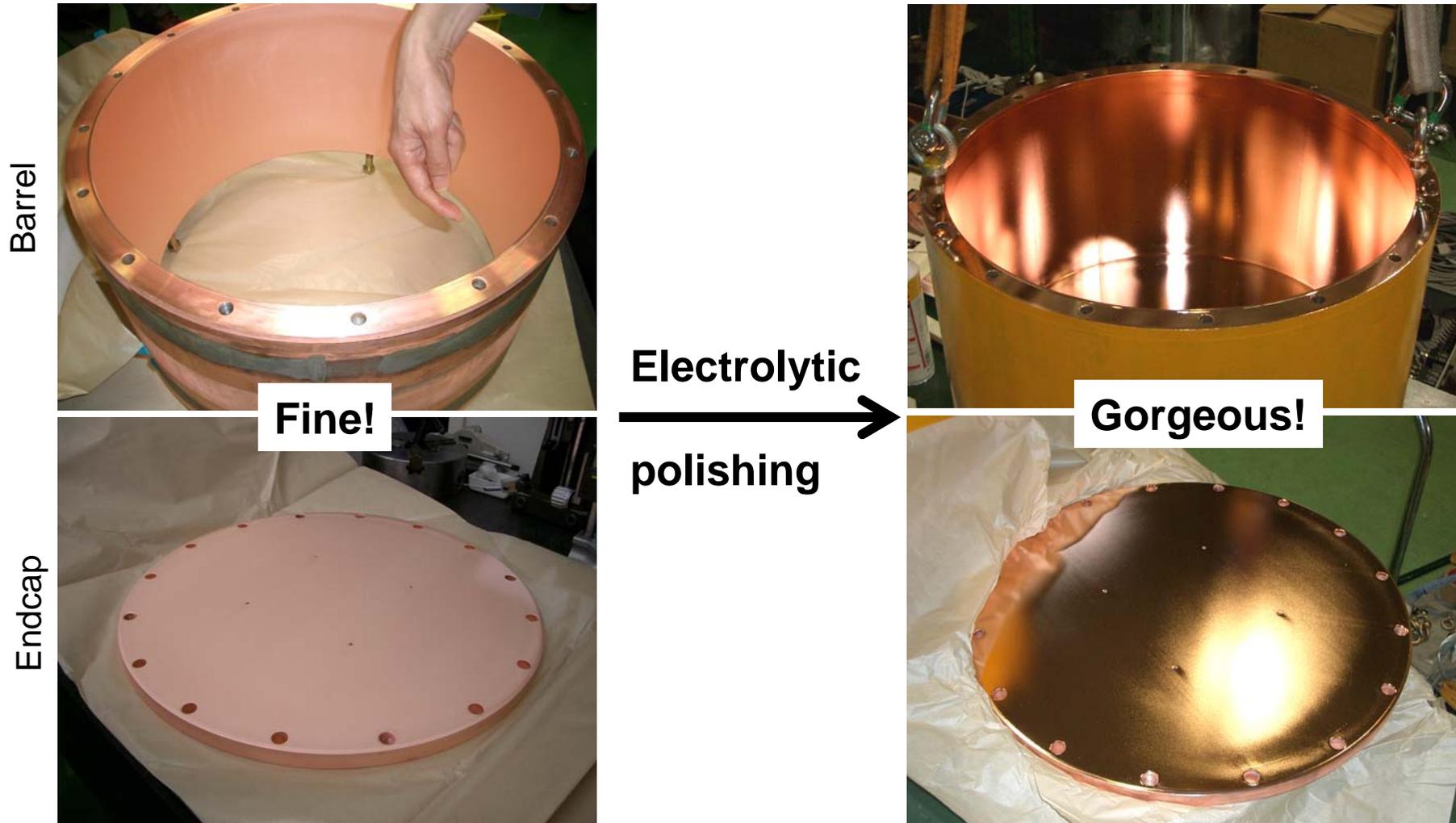
Copper Electroplating in an acid sulfate bath w/o brightener (PR process)



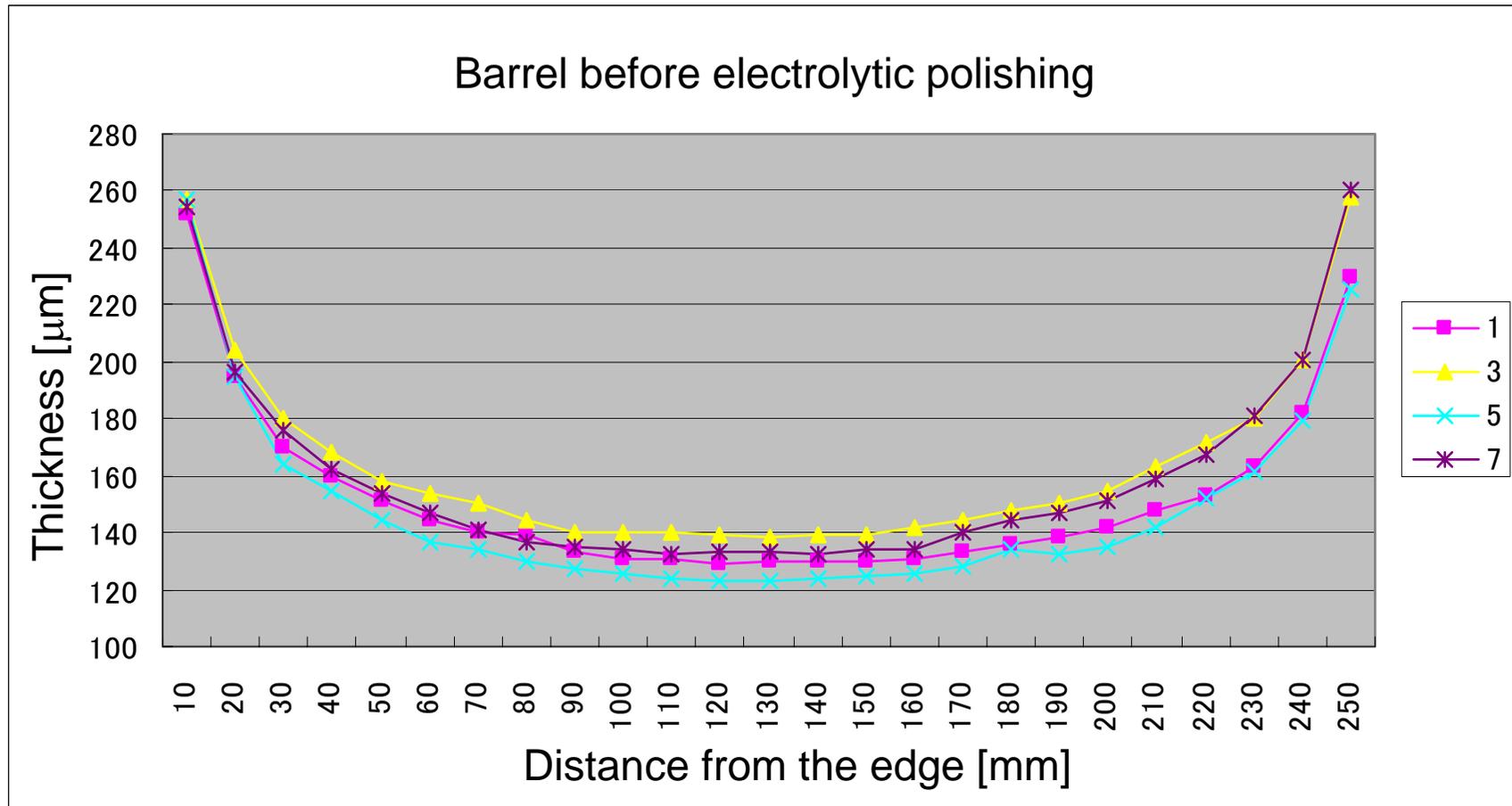
Electrolytic  
polishing

# After Trial and Error...

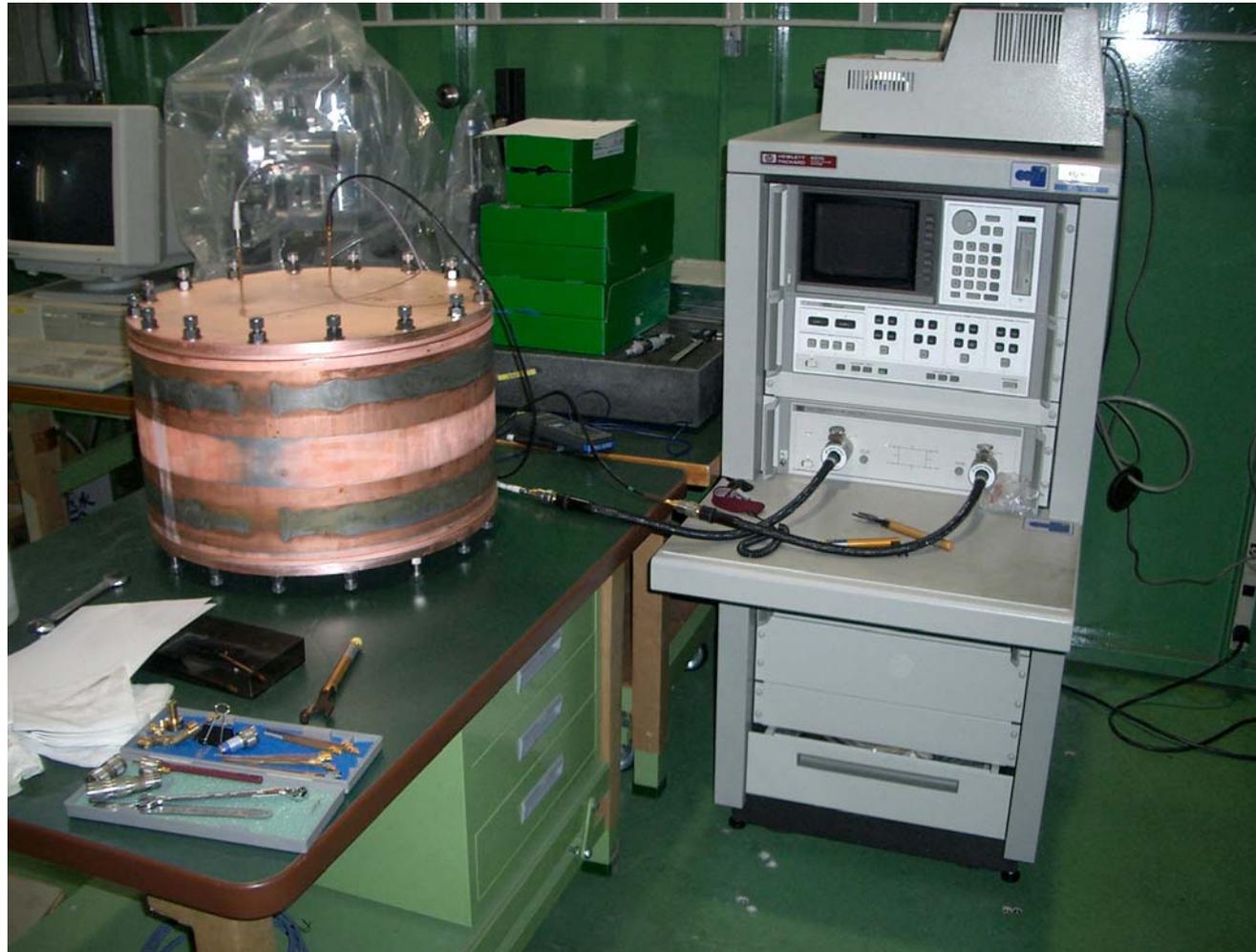
Copper Electroplating in an acid sulfate bath w/o brightener (PR process)



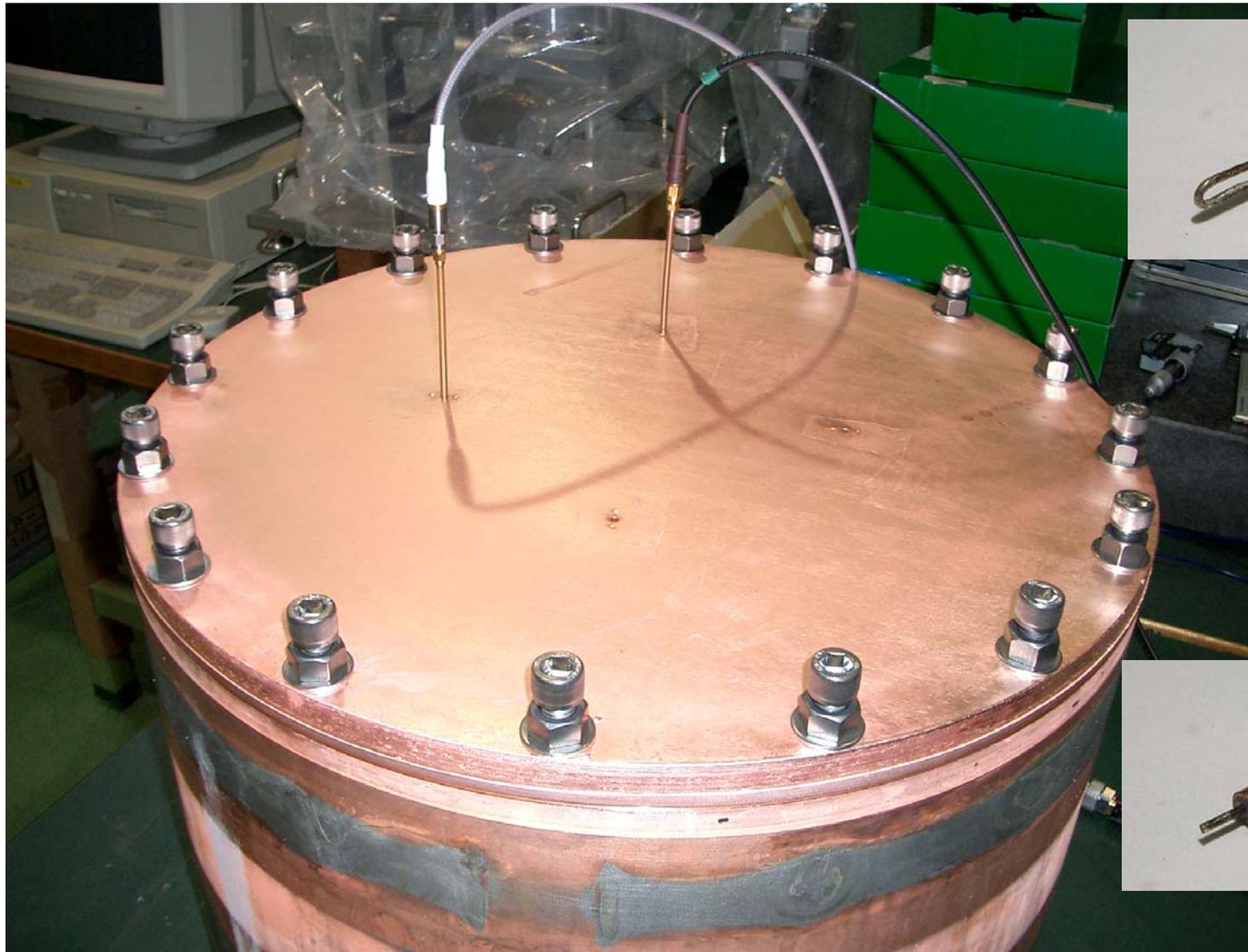
# Thickness Measurement



# Setup of the $Q_0$ Measurement



## Setup (close view)



Loop

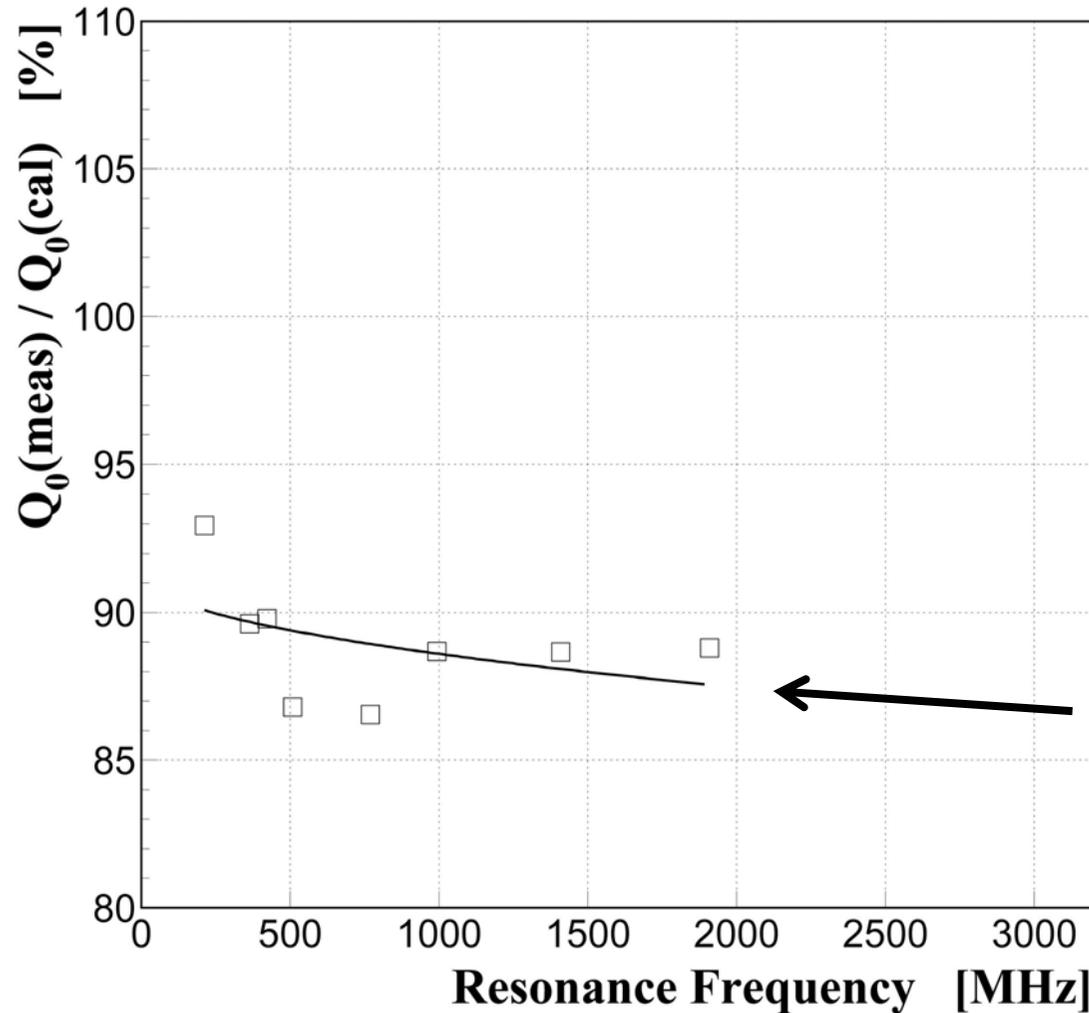
couples with magnetic field.



Antenna

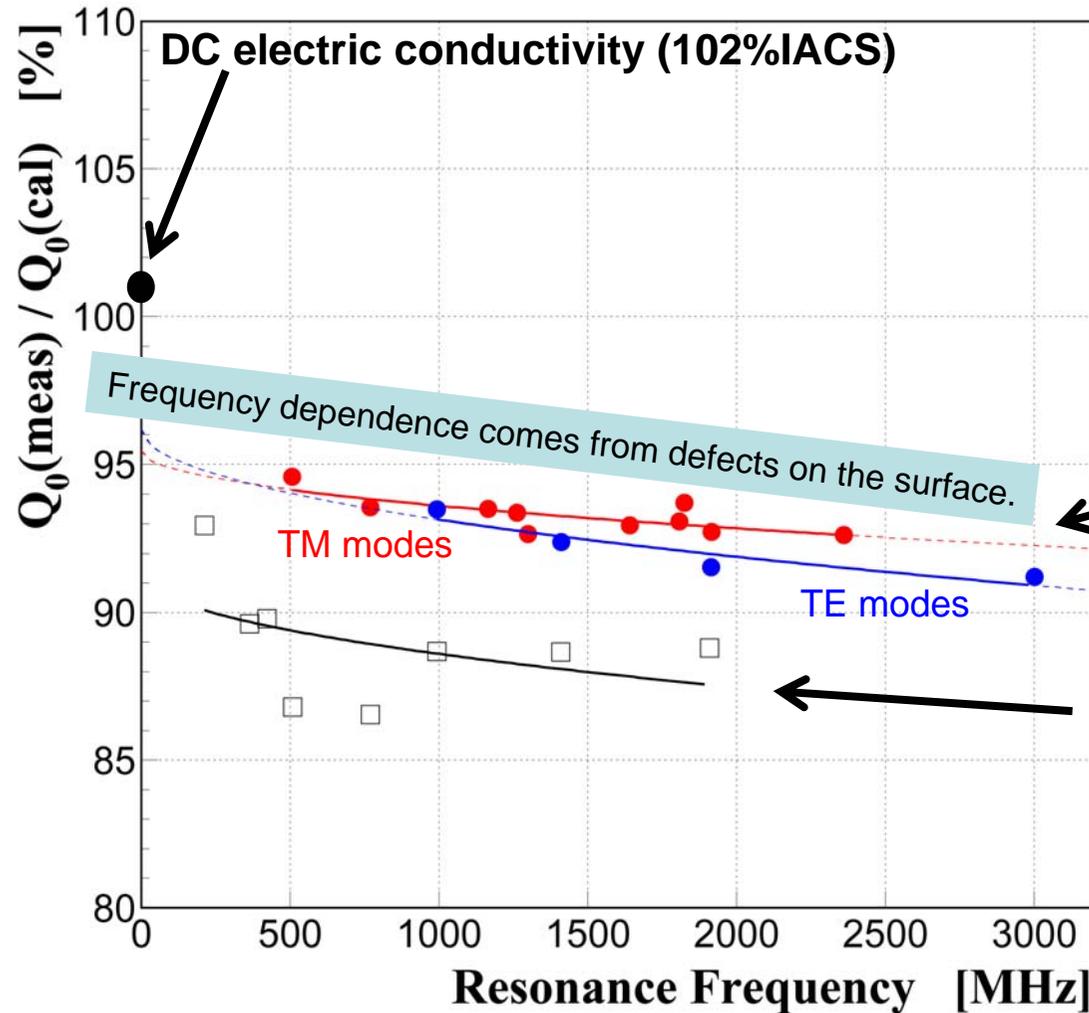
couples with electric field.

# Results of the $Q_0$ Measurements



Electroplating in a **pyrophosphate** bath  
**with brightener** (applied to the present S-cav's)  
(no temperature correction)

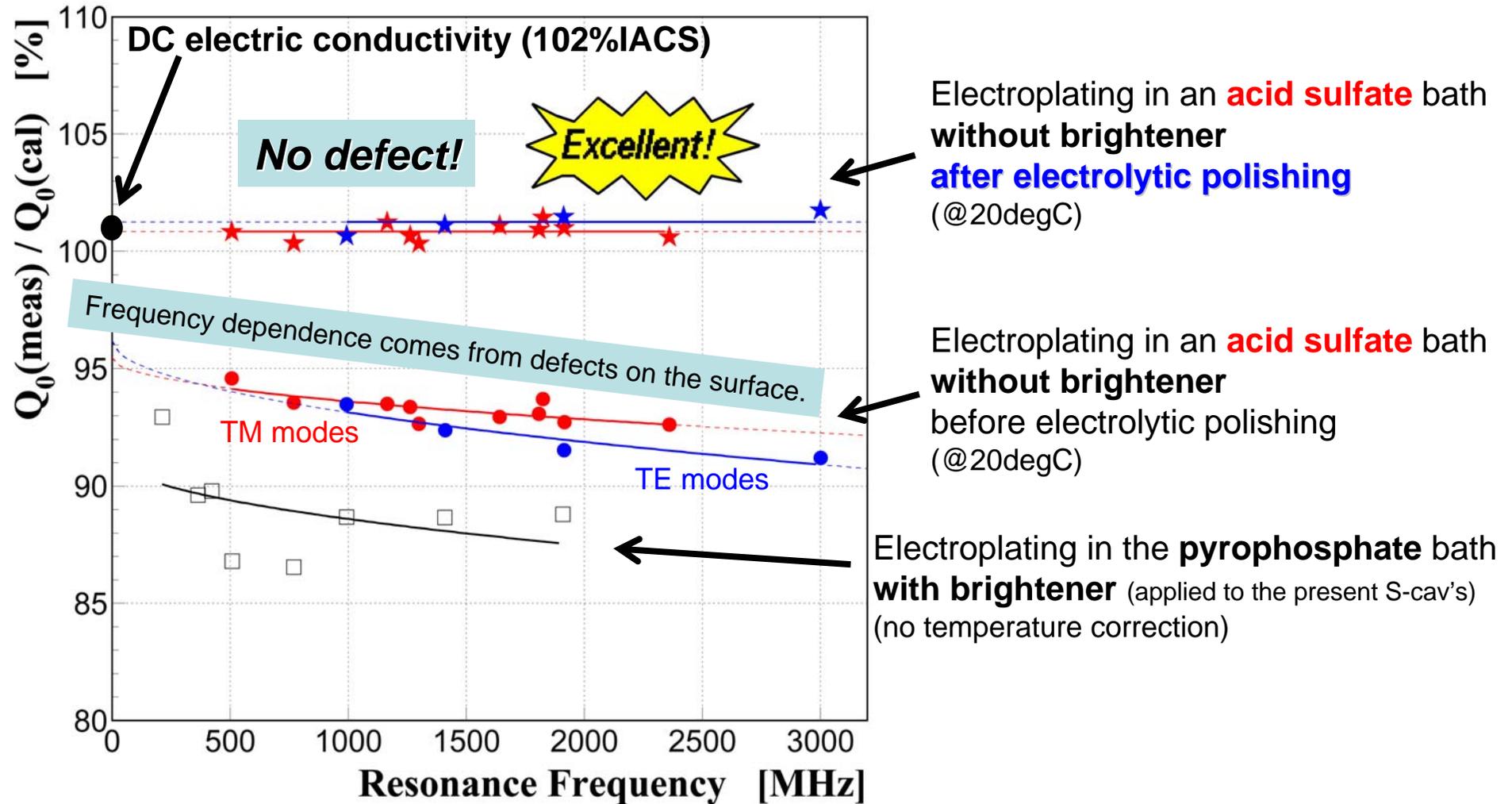
# Results of the $Q_0$ Measurements



Electroplating in an **acid sulfate** bath **without brightener** before electrolytic polishing (@20degC)

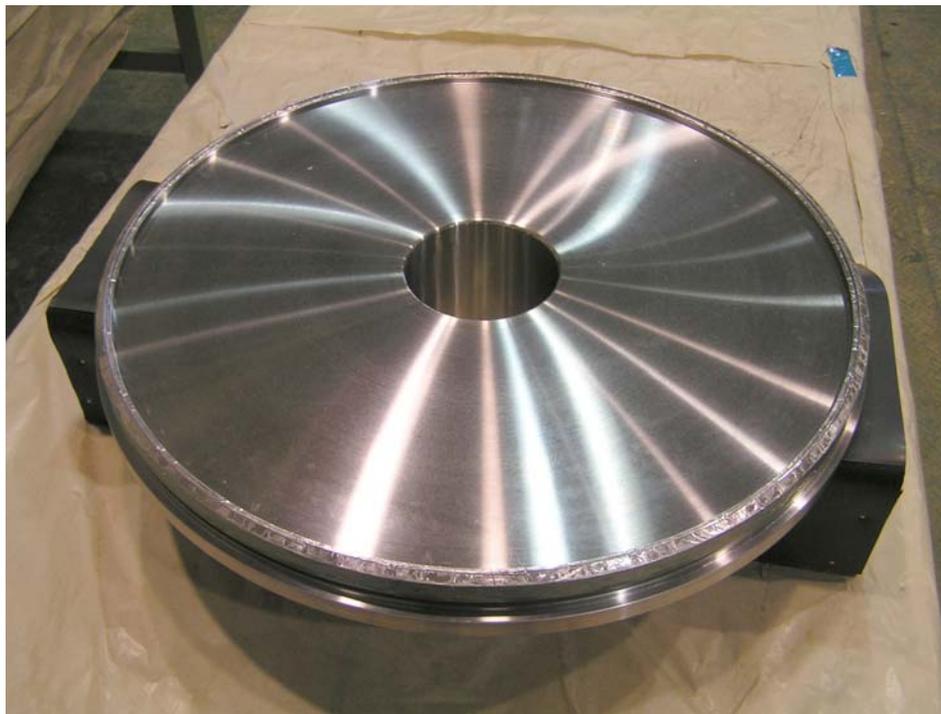
Electroplating in a **pyrophosphate** bath **with brightener** (applied to the present S-cav's) (no temperature correction)

# Results of the $Q_0$ Measurements

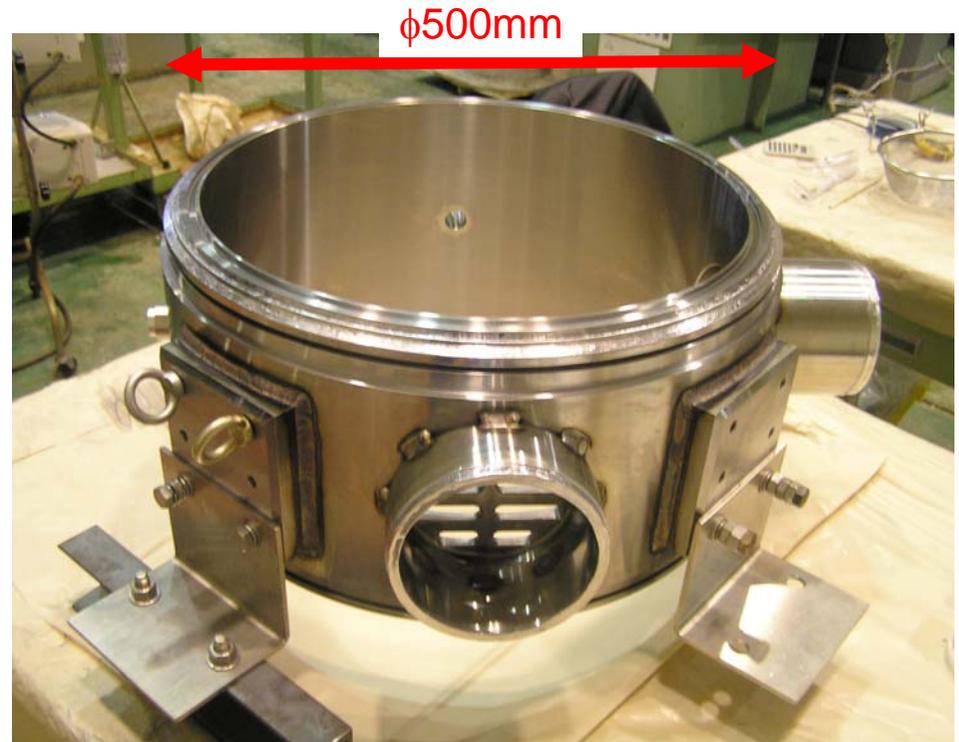


# Next Step: Vacuum Test

- *The test cavity has been fabricated.*
- *The electroplating is ongoing.*
- *A vacuum test will be done next month.*



Endcap



Barrel

# Summary

-  **ARES R&D programs are ongoing well.**
  
-  **A new L-band test stand has been constructed**
  - For the HOM-load upgrade.
  - The 1<sup>st</sup> stage has been finished.
  - To be tuned for supplying high powers.
  
-  **Input couplers with TiN coating**
  - Against multipactoring in the coaxial line.
  - Two TiN-coated couplers have been completed.
  - Being tested in the upgraded coupler test stand up to 800kW(CW).
  
-  **New highly-pure copper electroplating for S-cav**
  - On the slightly different condition from J-PARC.
  - The electric performance is estimated to be excellent.
  - A vacuum test to be done next month.