

Belle 衝突点領域に於ける 放射光ワット量分布の計算法の開発

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KCG Seminar

Feb. 7, 2002

Introduction

⇒ Motivation

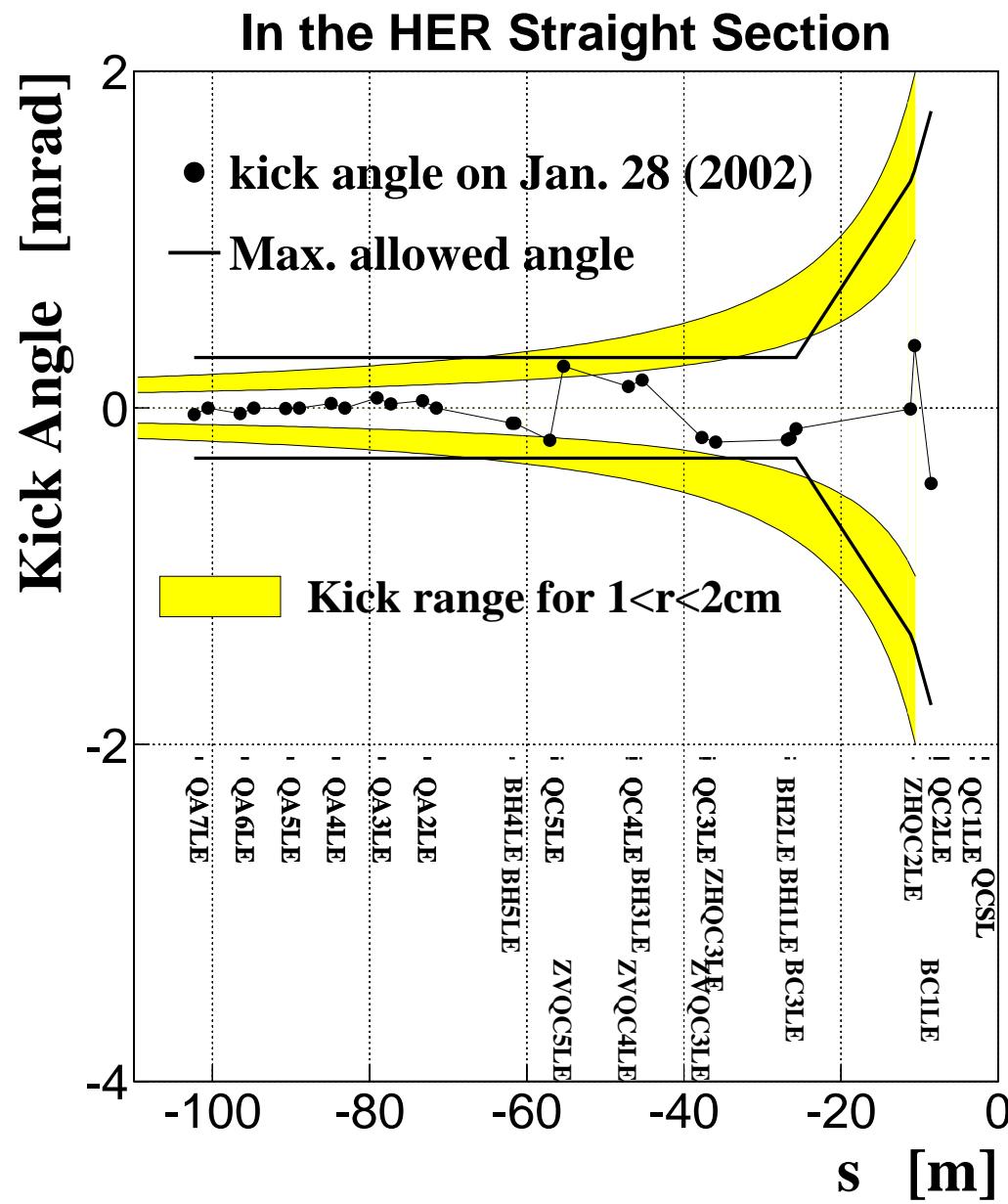
- ⇒ SVD1.0 was killed by the synchrotron radiation (SR) from HER.
 - Limitation for the HER steering magnets
 - Some current values are close to the limits. (→ figure)
- ⇒ Smaller-radius IR beampipe ($r = 2.0\text{ cm} \rightarrow 1.5\text{ cm} \rightarrow 1.0\text{ cm ?}$)
- ⇒ Larger beam currents for higher luminosities → more SR



⇒ A new idea has been proposed by Hitoshi Yamamoto:

Fitting **BPM**-measured values → **Real** beam orbit
→ **Wattage distribution** in the IR → Online alarm for SR

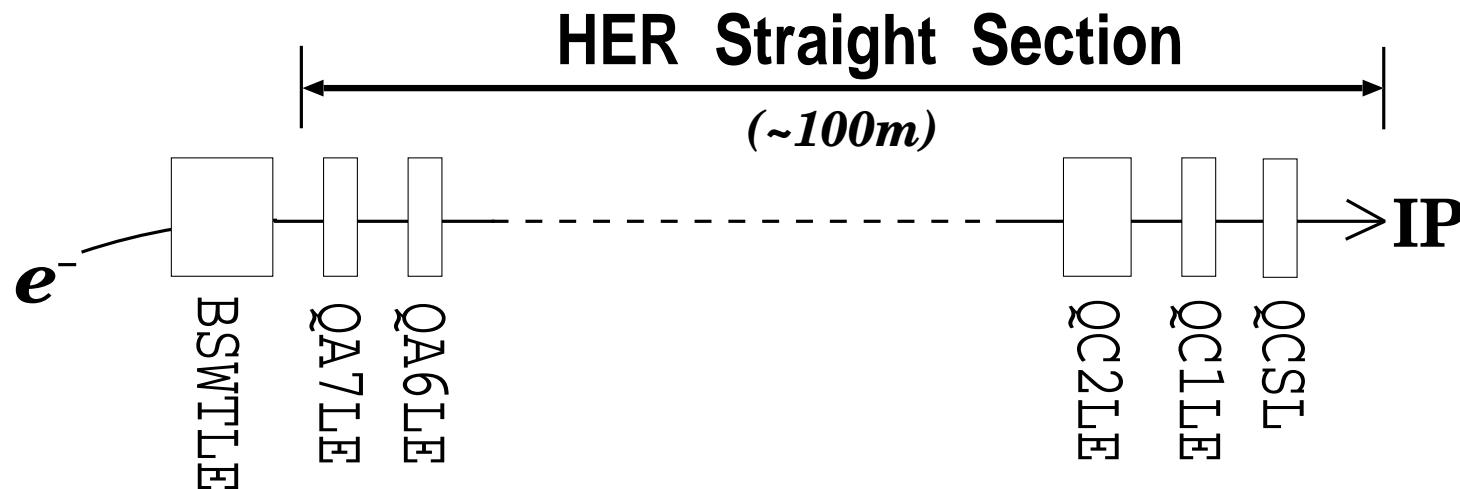
- ⇒ LOOSER LIMITATION for the HER steering magnets
- ⇒ PRIOR NOTICE for detector damages



Calculation Method

[I] Orbit Calculation

- In the HER straight section (see ↓)
- Using a linear approximation → **transfer matrices**
- Implemented in my own program



≪ Transfer Matrices ≫

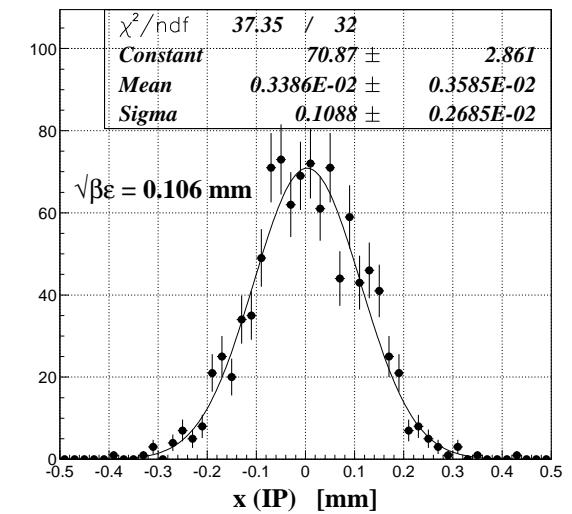
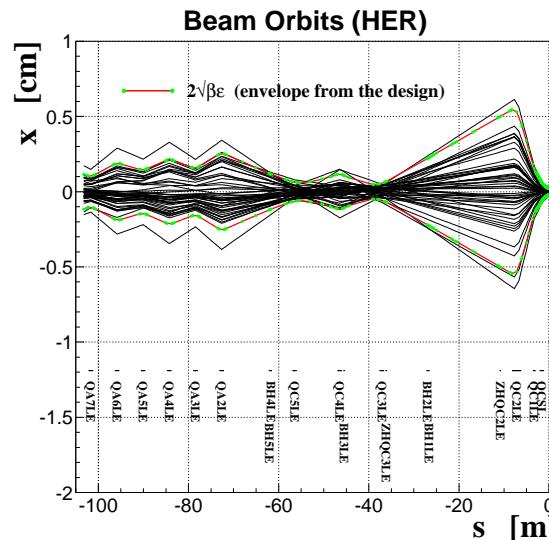
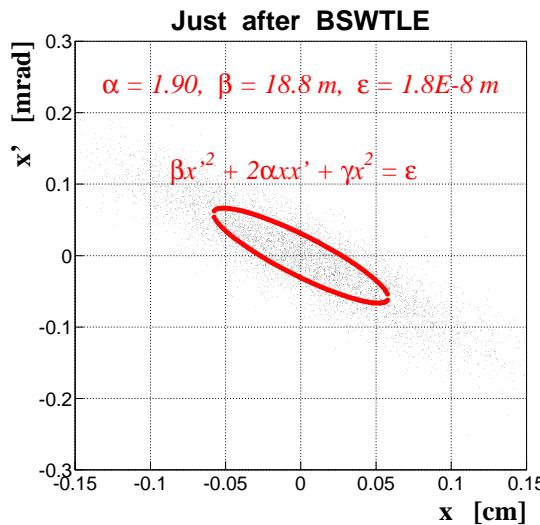
$$\text{Orbit : } \mathbf{X}(s) = \begin{pmatrix} x(s) \\ x'(s) \\ y(s) \\ y'(s) \\ \hline \mathbf{1} \end{pmatrix} \quad \text{Drift space : } \mathbf{R}_{\text{drift}}(L) = \left(\begin{array}{cc|c} 1 & L & \\ & 1 & \\ & & 1 & L \\ & & & 1 \end{array} \right)$$

$$\text{QUAD : } \mathbf{R}_{\text{quad}} = \left(\begin{array}{cc|c} \cos(kL) & k^{-1} \sin(kL) & \\ -k \sin(kL) & \cos(kL) & \\ \hline & & \cosh(kL) & k^{-1} \sinh(kL) \\ & & k \sinh(kL) & \cosh(kL) \end{array} \right) \quad \boxed{1}$$

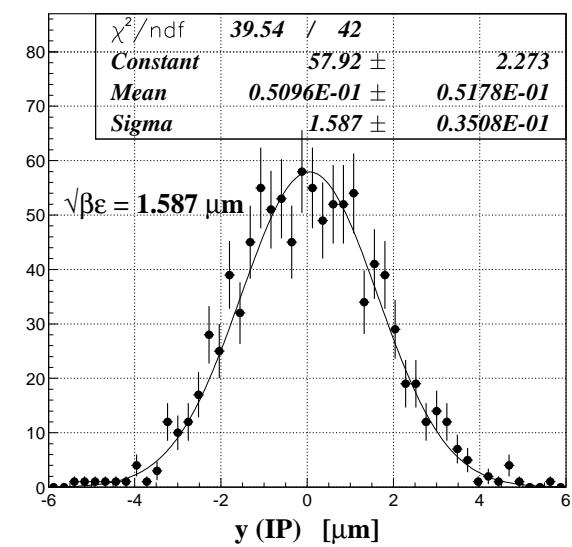
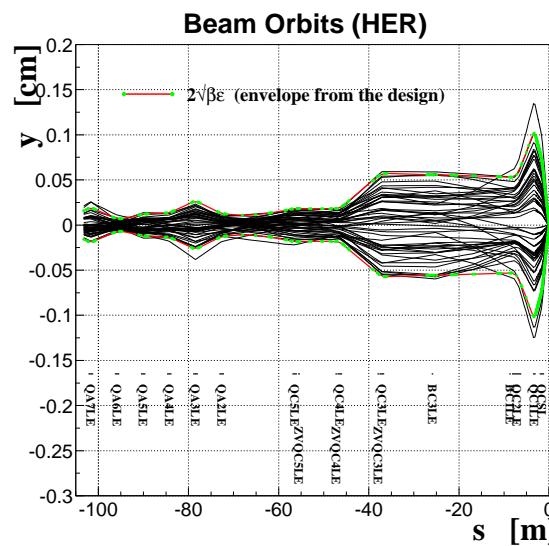
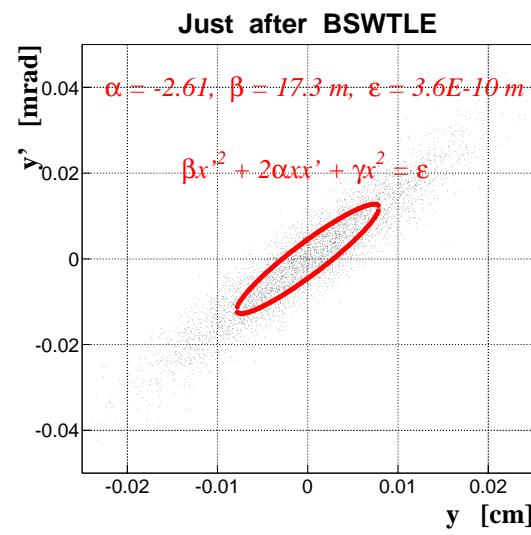
$$\text{BEND : } \mathbf{R}_{\text{bend}} = \mathbf{R}_{\text{drift}}(L/2) \times \left(\begin{array}{cc|c} 1 & & \theta_x \\ & 1 & \\ & & 1 \end{array} \right) \times \mathbf{R}_{\text{drift}}(L/2)$$

$$\text{Skew QUAD : } \mathbf{R}_{\text{skewQ}} = \mathbf{R}_{\text{rot}}(-45^\circ) \times \mathbf{R}_{\text{quad}} \times \mathbf{R}_{\text{rot}}(+45^\circ)$$

Check of the Transfer-Matrix Implementation [1]



BSWTLE $e^- \longrightarrow \text{IP}$



Check of the Transfer-Matrix Implementation [2]

Numerical comparison with SAD on QC3LE

```
In[61]:= TransferMatrix["QC3LE", "LX086E.1"]
Out[61]:= {1.0415110062367, 1.094542869142296, 0, 4.440892098501E-16}
           {.077425177671287, 1.0415110062367, 3.469446951954E-18, 0}
           {3.382710778155E-17, -3.53883589099E-16, .959055549847622, 1.065412001995326}
           {-2.60208521397E-18, 2.775557561563E-17, -.075287731090181, .959055549847622}
```

$$\frac{R_{ij} - R_{ij}^{(SAD)}}{|R_{ij}^{(SAD)}|} = \begin{pmatrix} 0 & +4 \times 10^{-15} & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & -2 \times 10^{-15} & -3 \times 10^{-14} \\ 0 & 0 & 0 & -2 \times 10^{-15} \end{pmatrix}$$

Check of the Transfer-Matrix Implementation [3]

Numerical comparison with SAD on QKELE

```
In[62]:= TransferMatrix["QKELE", "LC51LAE"]
```

```
Out[62]:=
```

```
{1.000001092692837,.372300042338456,-.00256049953636,-2.68166492929E-4}
{1.3572130039052E-5,1.000001092692837,-.013755037460226,-.00256049953636}
{-0.00256049953636,-2.68166492929E-4,1.000001092692837,.37230004233846}
{-0.013755037460226,-.00256049953636,1.3572130039019E-5,1.000001092692837}
```

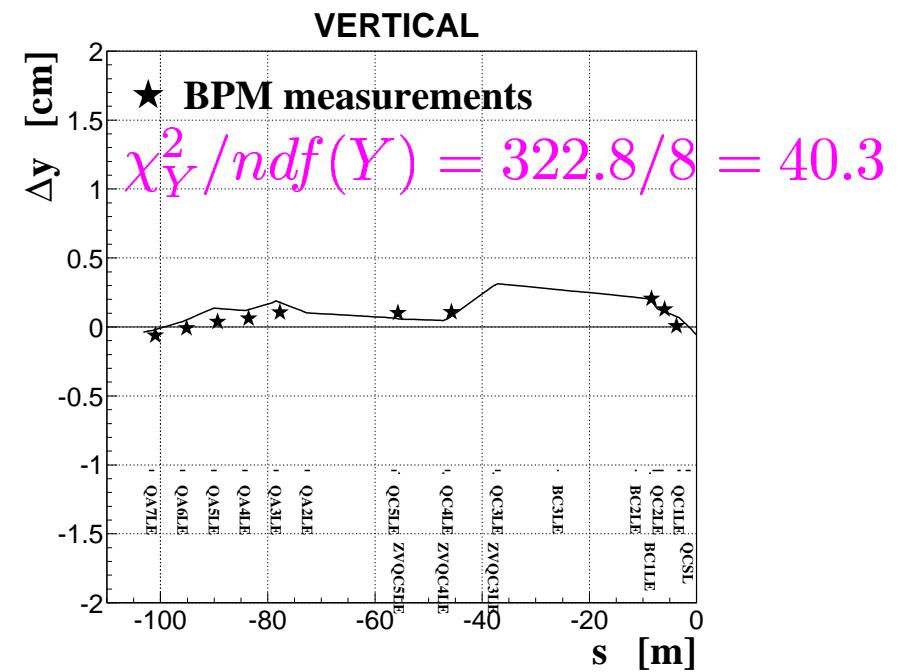
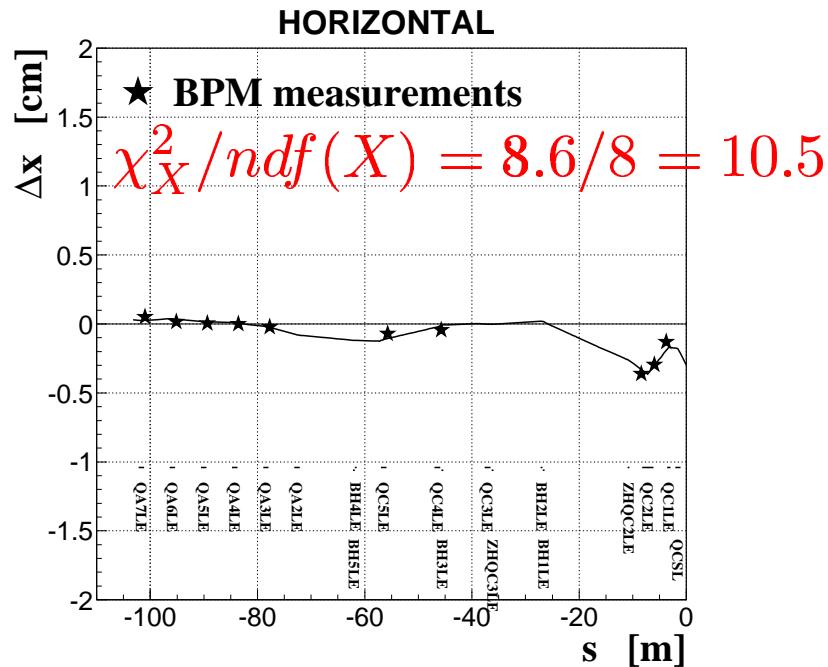
$$\frac{R_{ij} - R_{ij}^{(SAD)}}{|R_{ij}^{(SAD)}|} = \begin{pmatrix} -4 \times 10^{-14} & -2 \times 10^{-14} & -8 \times 10^{-14} & +6 \times 10^{-13} \\ -3 \times 10^{-11} & -4 \times 10^{-14} & 0 & -8 \times 10^{-14} \\ -8 \times 10^{-14} & +6 \times 10^{-13} & -4 \times 10^{-14} & -3 \times 10^{-14} \\ 0 & -8 \times 10^{-14} & +3 \times 10^{-11} & -4 \times 10^{-14} \end{pmatrix}$$

[II] Orbit Fitting

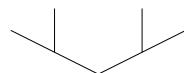
- Input parameters: $\begin{cases} \text{BR values from M002QC1} \sim \text{M013QA7} \\ k_0, k_1 \ (\rightarrow \text{optics}) \end{cases}$
- Floating parameters: $\begin{pmatrix} x_{\text{ini}} \\ y_{\text{ini}} \end{pmatrix}, \begin{pmatrix} x_{\text{IP}} \\ y_{\text{IP}} \end{pmatrix}$
- $\chi^2 \equiv \sum_{j:\text{BPM}} \left\{ \left(X_j^{(\text{BPM})} - X_j^{(\text{orbit})} \right)^2 + \left(Y_j^{(\text{BPM})} - Y_j^{(\text{orbit})} \right)^2 \right\} / \sigma^2$
- Minimization using MINUIT
- $\frac{\chi^2}{ndf} = \frac{\chi_X^2 + \chi_Y^2}{ndf(X) + ndf(Y)} = \frac{\frac{\chi_X^2}{ndf(X)} \frac{1}{ndf(Y)} + \frac{\chi_Y^2}{ndf(Y)} \frac{1}{ndf(X)}}{\frac{1}{ndf(X)} + \frac{1}{ndf(Y)}}$

Fitting Example

- BPM resolution: $100 \mu\text{m}$ (including offset uncertainties)
- Data on Nov. 7 (2001)

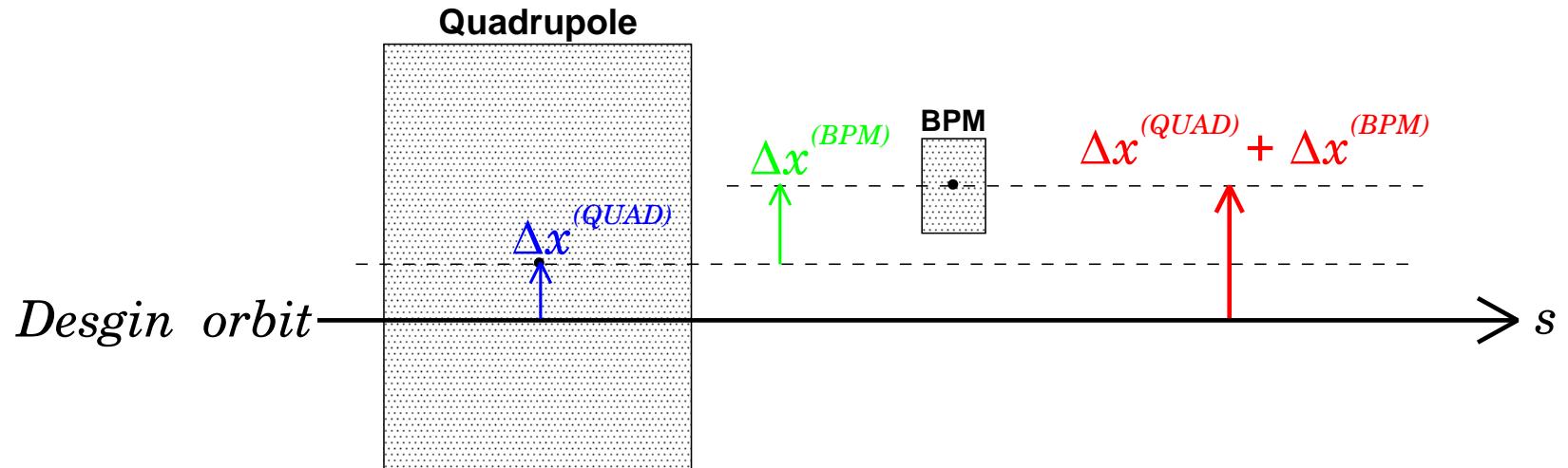


Failure with $X_{IP} \sim -3 \text{ mm}$ & $\chi^2/ndf \gg 1$



Need Some Offset Corrections!

Offset Definition



$$\chi^2 = \sum_{i: \text{orbits}} \sum_{j: \text{BPMs}} \left[\frac{\{(X_{j,i}^{(\text{BPM})} + \Delta X_j^{(\text{QUAD})} + \Delta X_j^{(\text{BPM})}) - X_{j,i}^{(\text{orbit})}\}^2}{+ \frac{\{(Y_{j,i}^{(\text{BPM})} + \Delta Y_j^{(\text{QUAD})} + \Delta Y_j^{(\text{BPM})}) - Y_{j,i}^{(\text{orbit})}\}^2}{\right] / (100 \mu m)^2$$

Offset Determination

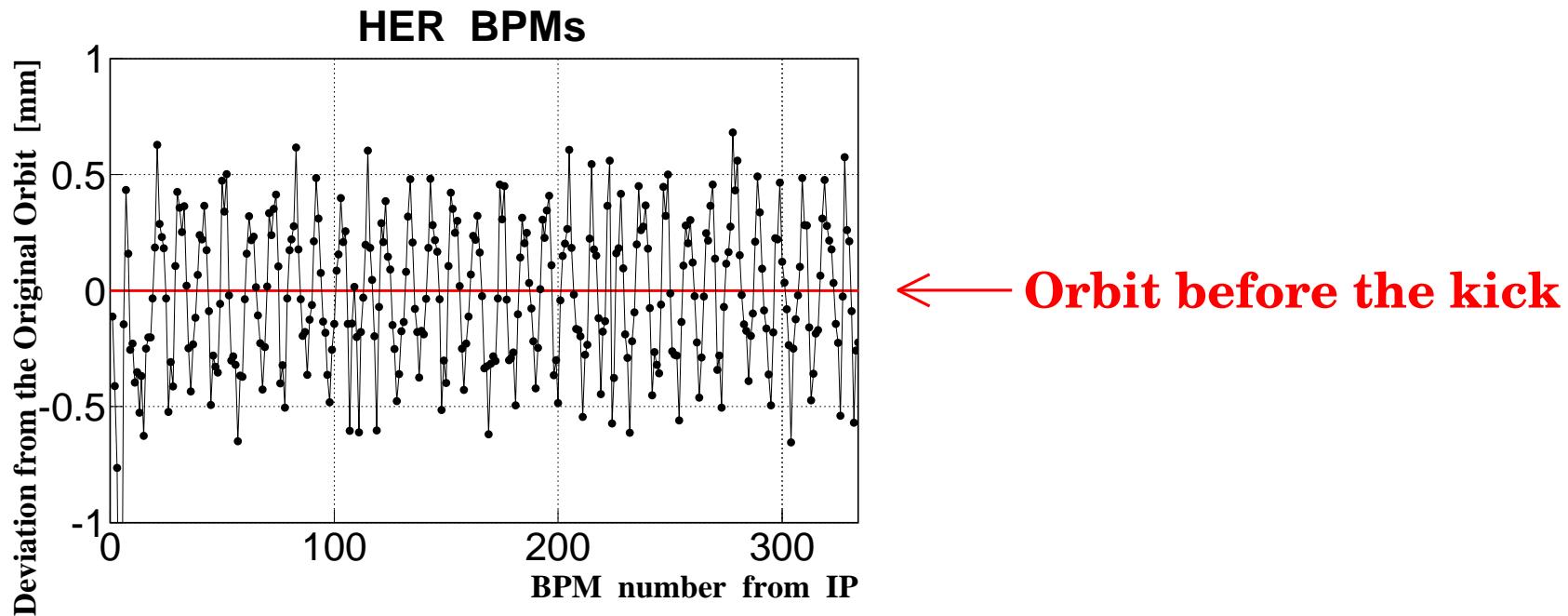
Using **BETARAW** sample: one of the following six sets of steering magnets ON

$$\left\{ \begin{array}{l} \text{ZHQFRNE1} \\ \text{ZVQDRNE1} \end{array} \right\} \left\{ \begin{array}{l} \text{ZHQFRNE2} \\ \text{ZVQDRNE2} \end{array} \right\} \left\{ \begin{array}{l} \text{ZHQFROE1} \\ \text{ZVQDROE1} \end{array} \right\} \left\{ \begin{array}{l} \text{ZHQFROE2} \\ \text{ZVQDROE2} \end{array} \right\} \left\{ \begin{array}{l} \text{ZHGX6E1} \\ \text{ZVQX5E1} \end{array} \right\} \left\{ \begin{array}{l} \text{ZHGX6E2} \\ \text{ZVQX5E2} \end{array} \right\}$$

$$s = \sim 710\text{m}, \sim 730\text{m}, \sim 2220\text{m}, \sim 2240\text{m}, \sim 1460\text{m}, \sim 1540\text{m}$$

→ An oscillation around the original orbit

→ Six different orbits are obtained.



« Floating Parameters »

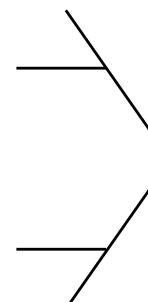
- Starting and ending points of orbits:

$$\left\{ \begin{pmatrix} X_{ini}^i \\ Y_{ini}^i \end{pmatrix}, \begin{pmatrix} X_{IP}^i \\ Y_{IP}^i \end{pmatrix} \right\}$$

$(i = 1, 2, 3, 4, 5, 6 : \text{orbits})$

- Offsets of BPMs and QUADs
- Scales of bendings:**

$$\theta_{kick}^{(NEW)} = (1 + a) \times \theta_{kick}^{(ORG)}$$



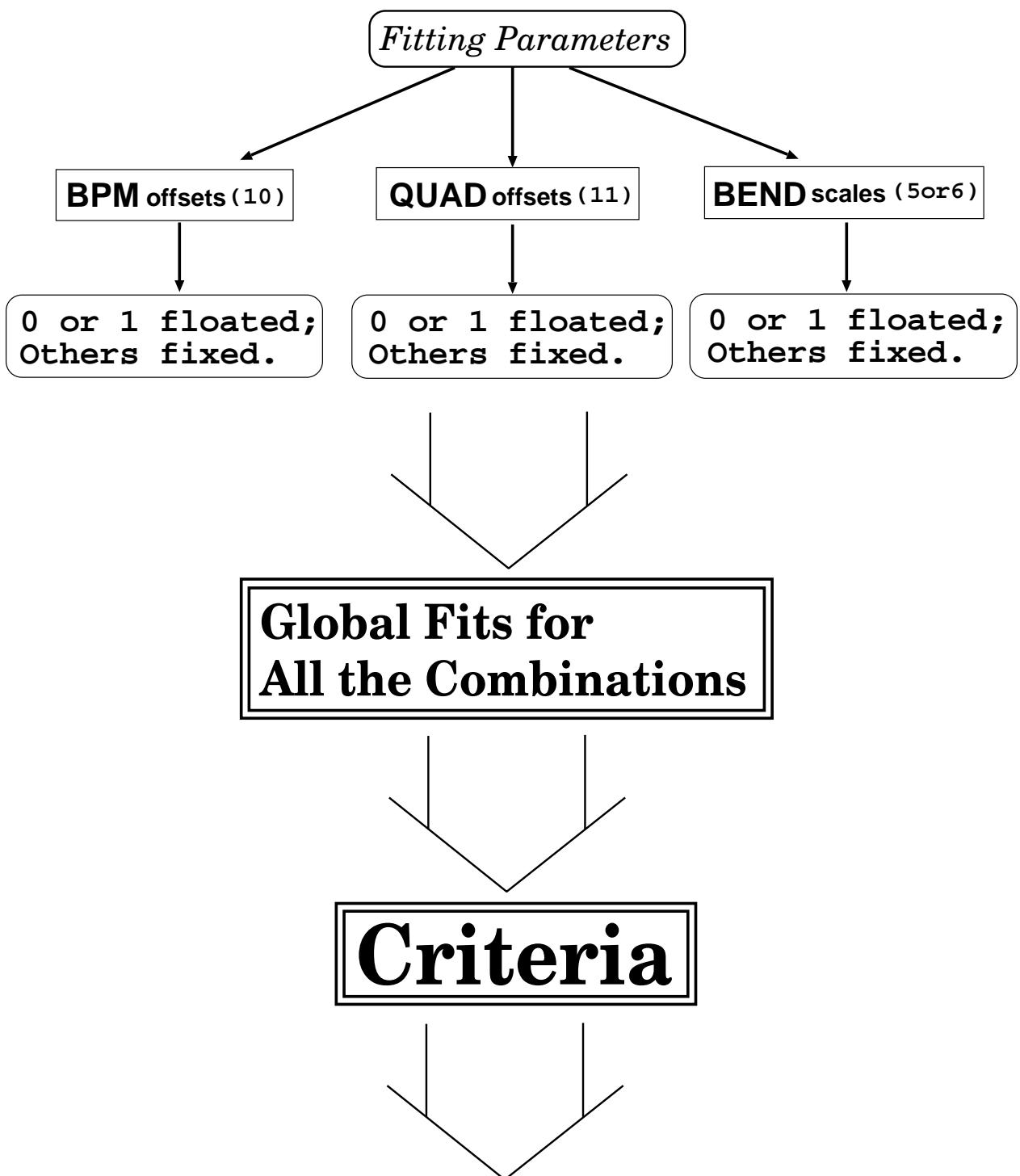
If we float all,

- > 100 floating parameters
- Large offsets (> 1 cm)
- Multi-solution
- Not positive-definite Hessian matrix

Common among all the orbits



Strategy



Criteria

- ⇒ MINUIT convergence with a positive-definite Hessian matrix
- ⇒ $| \text{BPM offsets} | < 1 \text{ cm}$
- ⇒ $| \text{QUAD offsets} | < 1 \text{ cm}$ (alignment)
- ⇒ $| \text{BEND rescaling factor} | < 20\%$ (kick angle)
- ⇒ $| X_{IP} | < 1 \text{ mm}$ & $| Y_{IP} | < 1 \text{ mm}$

We find a solution

- With the smallest modification
- Within the scope of the numerical approach

BETARAW sample on Jun. 4, 2001

«Horizontal»

| | X_1 | X_2 | X_3 | X_4 |
|---------------------|---------------------|---------------------|---------------------|---------------------|
| floating BPM | M006QC4LE | M006QC4LE | M006QC4LE | M006QC4LE |
| floating QUAD | QC2LE | QC2LE | QC2LE | QC2LE |
| floating BEND | | BH12LE | BH45LE | ZHQC5LE |
| $\chi^2_X/ndf(X)$ | 3.5 | 3.4 | 3.4 | 3.5 |
| BPM offset [mm] | $+0.56 \pm 0.04$ | $+0.60 \pm 0.05$ | $+0.62 \pm 0.05$ | $+0.50 \pm 0.07$ |
| QUAD offset [mm] | $+0.62 \pm 0.04$ | $+0.61 \pm 0.04$ | $+0.61 \pm 0.04$ | $+0.62 \pm 0.04$ |
| BEND scale [%] | | $+3.5 \pm 3.2\%$ | $+4.2 \pm 2.1\%$ | $-6.3 \pm 4.9\%$ |
| IP offset [mm] | $\sim -0.7 \pm 0.1$ | $\sim -0.6 \pm 0.1$ | $\sim -0.7 \pm 0.1$ | $\sim -0.6 \pm 0.1$ |
| M005QC3 offset [mm] | -0.85 ± 0.04 | -0.88 ± 0.05 | -0.83 ± 0.04 | -0.88 ± 0.05 |
| M008QA2 offset [mm] | -0.85 ± 0.05 | -0.82 ± 0.06 | -0.94 ± 0.07 | -0.80 ± 0.06 |

BETARAW sample on Jun. 4, 2001

<<Vertical>>

| | Y1 | Y2 | Y3 |
|-----------------------|-----------------|-----------------|---------------|
| floating BPM | M002QC1LE | M002QC1LE | M003QC2LE |
| floating QUAD | QA2LE | QA2LE | QA2LE |
| floating BEND | ZVQC3LE | ZVQC5LE | ZVQC5LE |
| $\chi^2_Y / ndf(Y)$ | 0.7 | 0.7 | 1.1 |
| BPM offset [mm] | +0.64 ± 0.06 | +0.74 ± 0.06 | -0.52 ± 0.05 |
| QUAD offset [mm] | +0.85 ± 0.03 | +0.79 ± 0.03 | +0.77 ± 0.03 |
| BEND scale [%] | +17 ± 1% | -12 ± 1% | -16 ± 1% |
| IP offset [mm] | ~ -0.57 ± 0.003 | ~ -0.54 ± 0.001 | -0.54 ± 0.001 |
| M005QC3LE offset [mm] | -0.49 ± 0.09 | -1.12 ± 0.05 | -1.38 ± 0.05 |
| M008QA2LE offset [mm] | -0.56 ± 0.05 | -0.50 ± 0.05 | -0.48 ± 0.05 |

BETARAW sample on Oct. 24, 2001

«Horizontal»

| | X_1 | X_2 | X_3 | X_4 |
|-----------------------|---------------------|---------------------|---------------------|-------|
| floating BPM | M006QC4LE | M006QC4LE | M006QC4LE | |
| floating QUAD | QC2LE | QC2LE | QC2LE | |
| floating BEND | | BH12LE | BH45LE | |
| $\chi^2_X / ndf(X)$ | 3.4 | 2.8 | 3.4 | |
| BPM offset [mm] | $+0.63 \pm 0.04$ | $+0.78 \pm 0.05$ | $+0.59 \pm 0.05$ | |
| QUAD offset [mm] | $+0.58 \pm 0.04$ | $+0.52 \pm 0.04$ | $+0.58 \pm 0.04$ | |
| BEND scale [%] | | $+16 \pm 3\%$ | $-3.5 \pm 2.1\%$ | |
| IP offset [mm] | $\sim -0.8 \pm 0.1$ | $\sim -0.7 \pm 0.1$ | $\sim -0.8 \pm 0.1$ | |
| M005QC3LE offset [mm] | -0.74 ± 0.04 | -0.86 ± 0.05 | -0.76 ± 0.04 | |
| M008QA2LE offset [mm] | -1.01 ± 0.05 | -0.84 ± 0.06 | -0.93 ± 0.07 | |

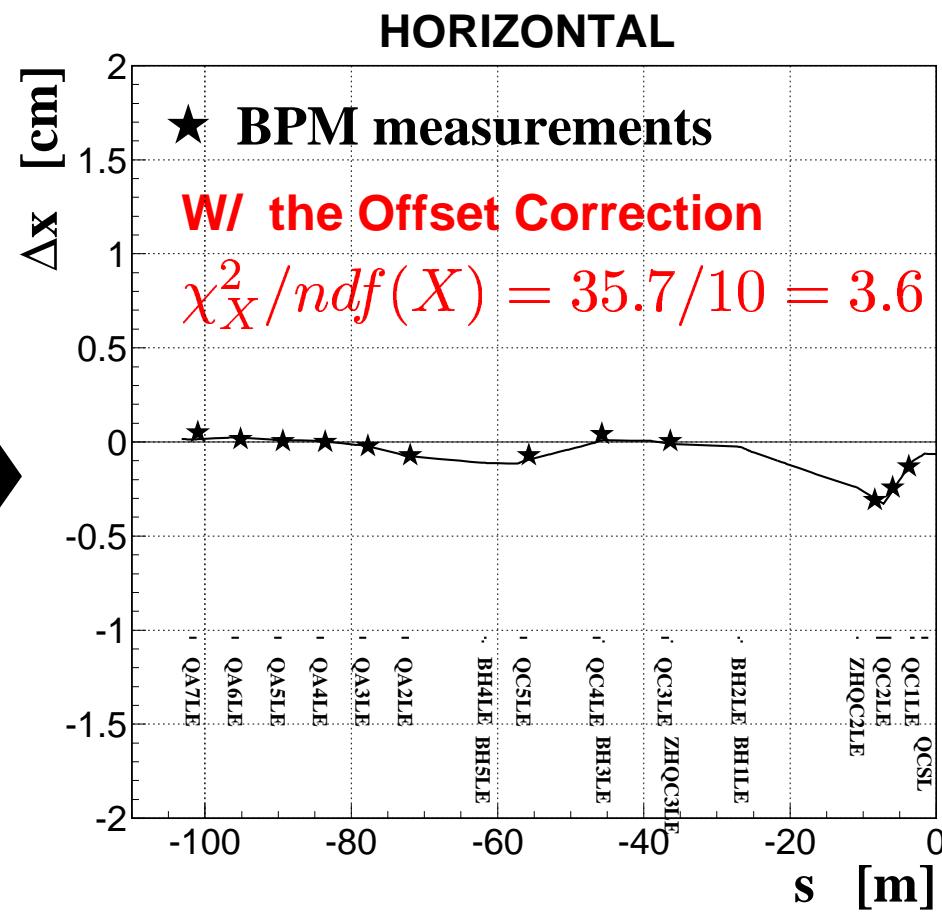
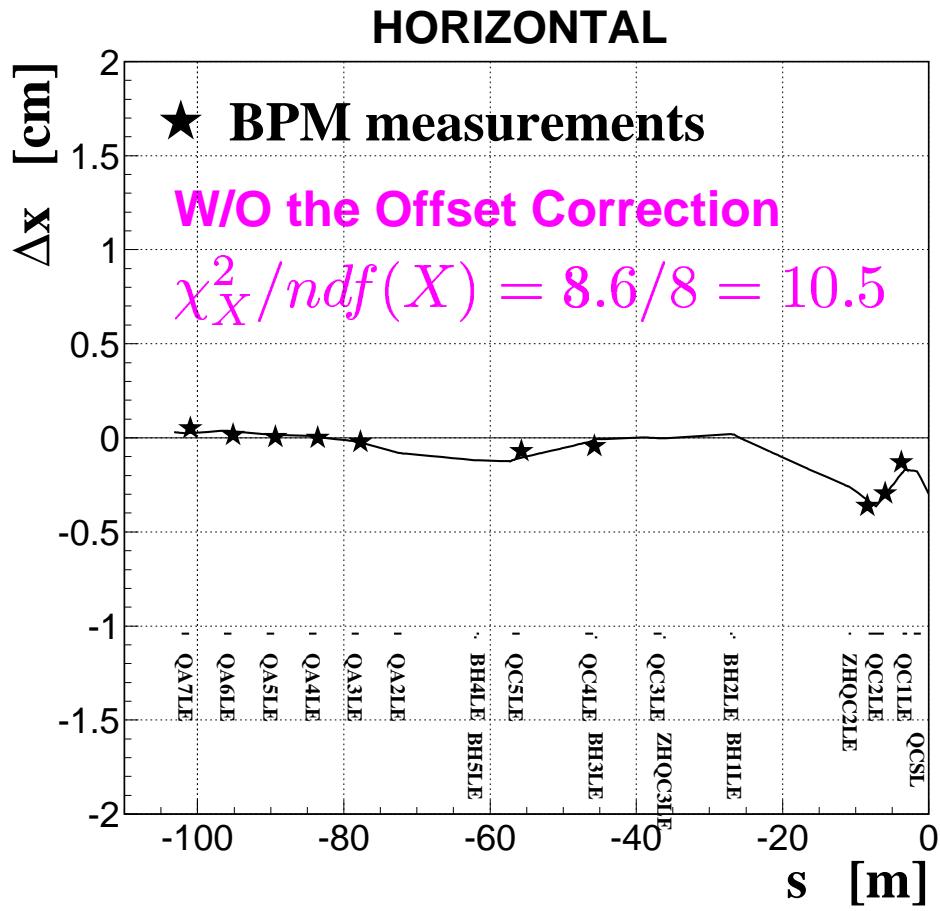
BETARAW sample on Oct. 24, 2001

<<Vertical>>

| | Y_1 | Y_2 | Y_3 |
|-----------------------|------------------------|------------------------|-------------------|
| floating BPM | M002QC1LE | M002QC1LE | M002QC1LE |
| floating QUAD | QA2LE | QA2LE | QA3LE |
| floating BEND | ZVQC3LE | ZVQC5LE | ZVQC5LE |
| χ^2_Y / ndf_Y | 0.4 | 0.5 | 0.7 |
| BPM offset [mm] | $+0.74 \pm 0.06$ | $+0.85 \pm 0.06$ | $+0.85 \pm 0.06$ |
| QUAD offset [mm] | $+0.66 \pm 0.03$ | $+0.60 \pm 0.03$ | -0.21 ± 0.01 |
| BEND scale [%] | $+15 \pm 1\%$ | $-12 \pm 1\%$ | $-19 \pm 1\%$ |
| IP offset [mm] | $\sim -0.63 \pm 0.003$ | $\sim -0.60 \pm 0.001$ | -0.60 ± 0.001 |
| M005QC3LE offset [mm] | -0.32 ± 0.09 | -1.02 ± 0.05 | -1.01 ± 0.05 |
| M008QA2LE offset [mm] | -0.51 ± 0.05 | -0.45 ± 0.05 | -0.10 ± 0.04 |

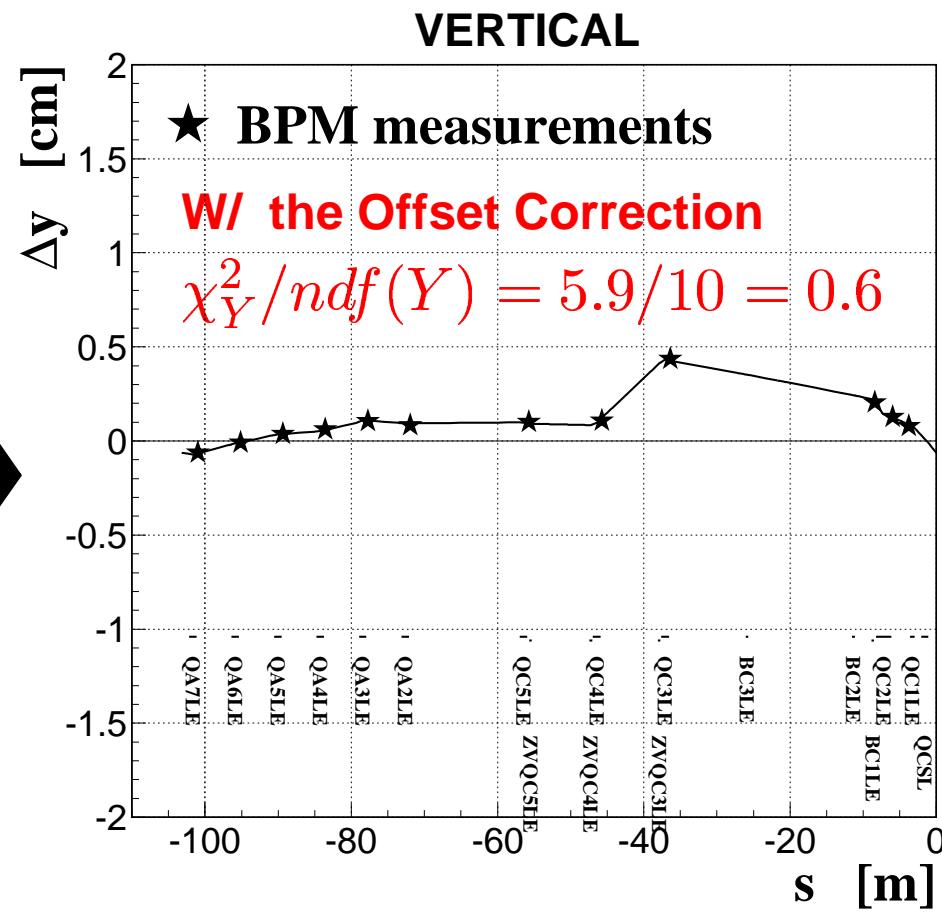
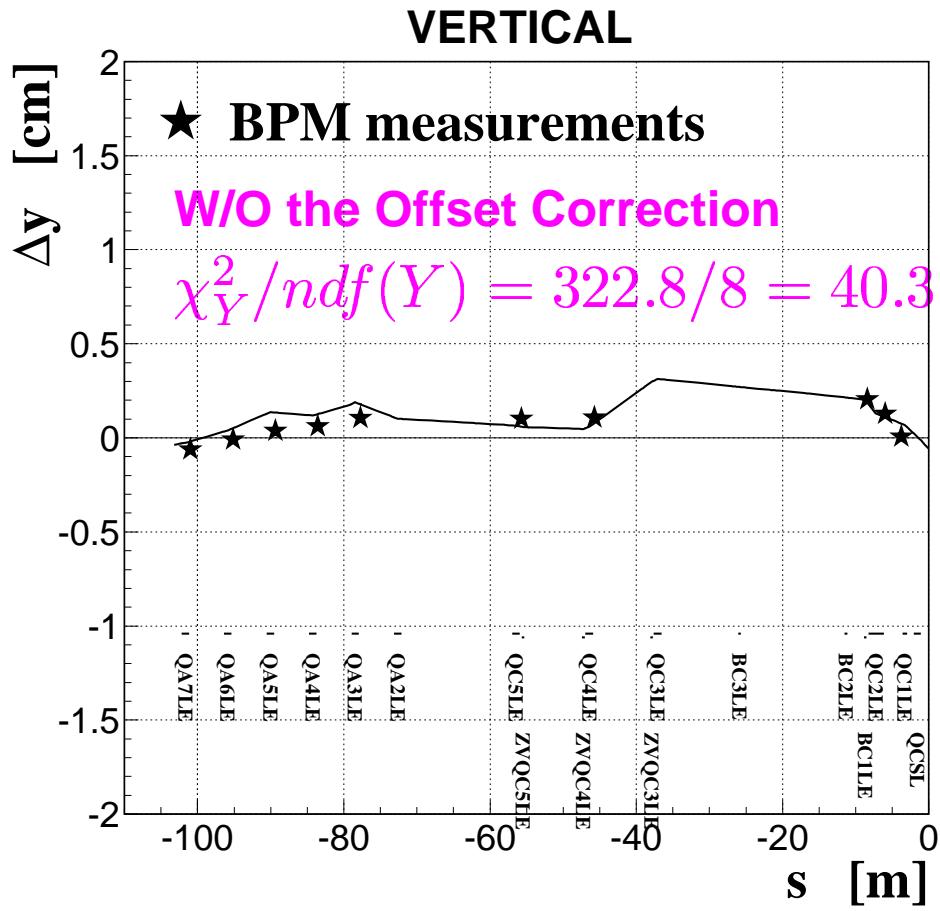
Results of the Offset Correction

(Horizontal case)



Results of the Offset Correction

(Vertical case)

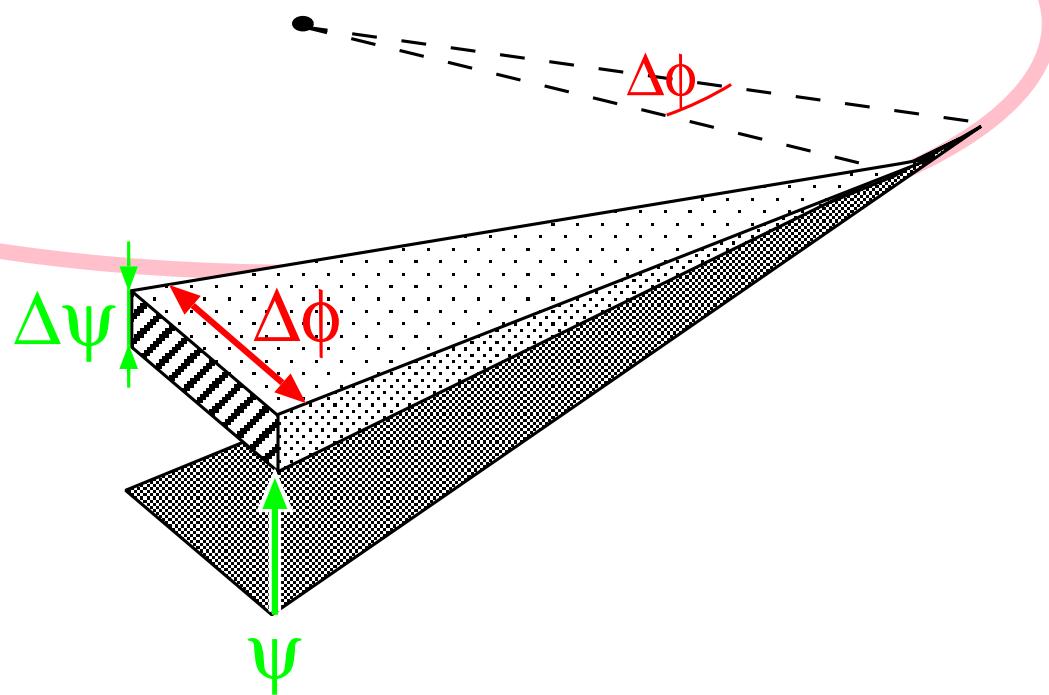


[III] Wattage Calculation

Using the following analytical formula (Phys. Rev. 75 (1949) 1912) :

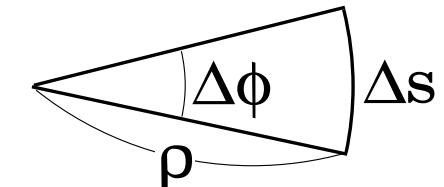
$$\Delta W = \frac{3\alpha}{4\pi^2} \frac{I}{e} \gamma^2 \times \Delta\omega \Delta\phi \Delta\psi \frac{1}{\omega} \left(\frac{\omega}{\omega_c} \right)^2 (1 + X^2)^2 \left\{ K_{\frac{2}{3}}^2(\eta) + \frac{X^2}{1 + X^2} K_{\frac{1}{3}}^2(\eta) \right\} \hbar\omega$$

$(\gamma : \text{Lorentz factor}, \omega : \text{frequency}, X \equiv \gamma\psi, \eta \equiv \frac{1}{2} \frac{\omega}{\omega_c} (1 + X^2)^{3/2})$



$$\Delta\phi \cong \frac{\Delta s}{\rho(s)}$$

$$\sum \Delta s \rightarrow \int ds \quad (\text{integration along the orbit})$$

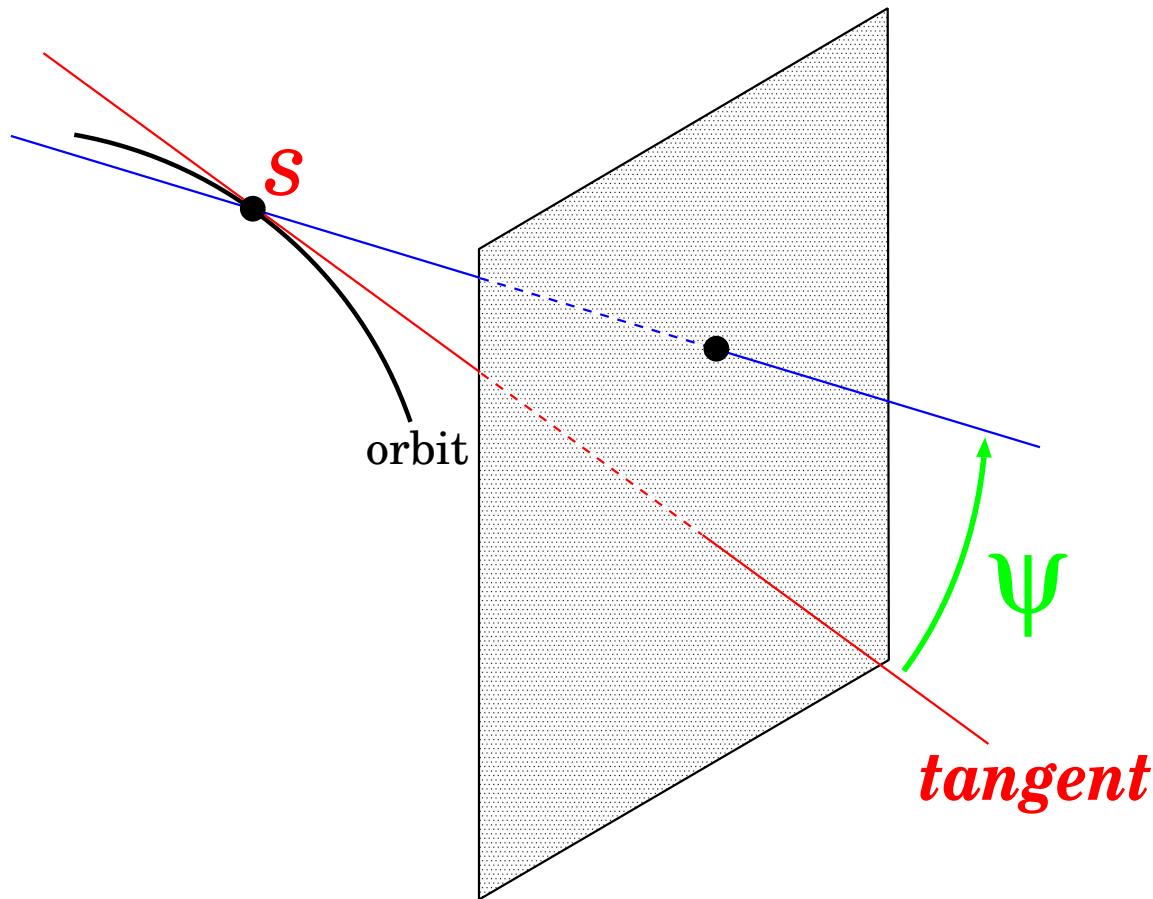


$$W = \frac{3\alpha}{4\pi^2} \frac{I}{e} \gamma^2 \iiint d\omega ds d\psi \frac{1}{\omega} \left(\frac{\omega}{\omega_c}\right)^2 (1 + X^2)^2 \left\{ K_{\frac{2}{3}}^2(\eta) + \frac{X^2}{1 + X^2} K_{\frac{1}{3}}^2(\eta) \right\} \frac{\hbar\omega}{\rho(s)}$$



3D-integration is performed using BASES. (MC integration)

Projection to a Plane

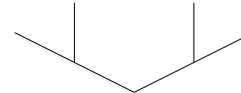


Mapping: $(s, \psi) \rightarrow$ point in the plane

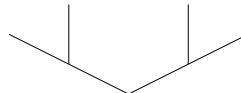
Check of the Wattage Calculation

by comparing with the SAD calculation

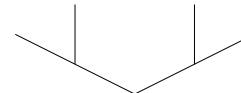
Start with the same lattice model file
(/ldata/KEKB/KCG/HER/herfq270.sad)



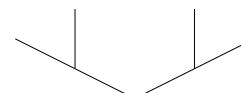
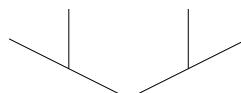
For a certain component (e.g. QC3LE)



My Calculation



SAD

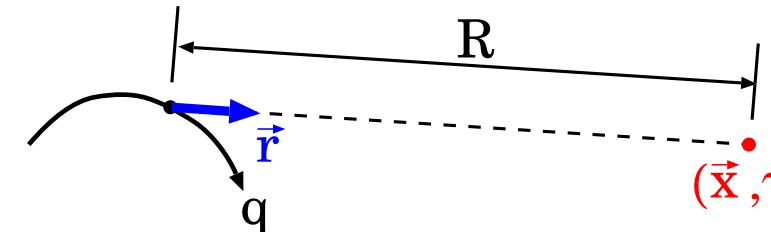


Wattage distribution in the XY plane at $Z = -8\text{ cm}$

Exact Calculation using SAD

starting with the **Feynman-Heaviside** formula

$$\vec{E}(\vec{x}, \tau) = \frac{q}{4\pi\epsilon_0} \left[\frac{\vec{r}}{R^2} + \frac{R}{c} \frac{d}{d\tau} \left(\frac{\vec{r}}{R^2} \right) + \frac{1}{c^2} \frac{d^2}{d\tau^2} \vec{r} \right]$$



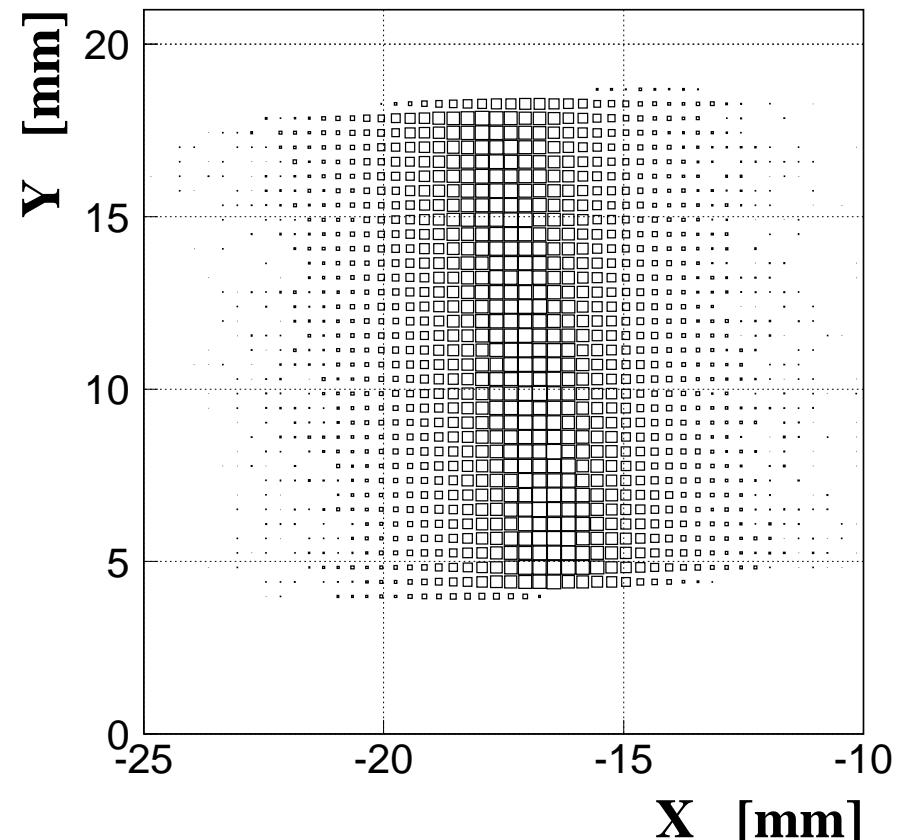
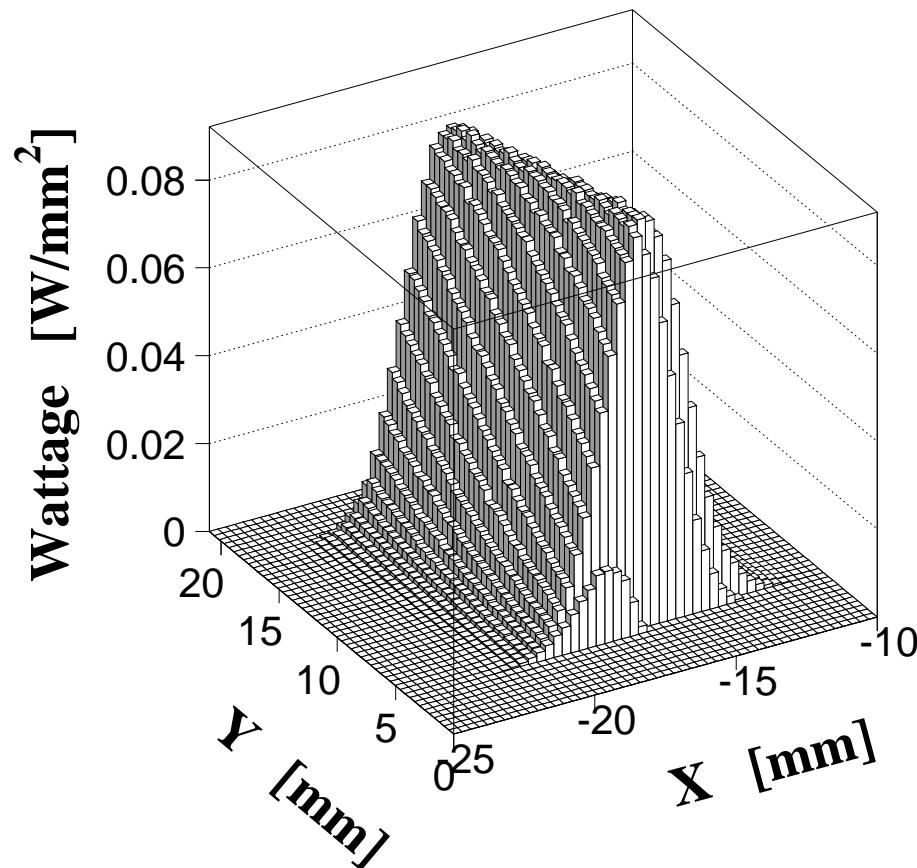
$$\vec{E}'(\vec{x}, \tau) = \frac{1}{2\pi} \int_{\omega_{min}}^{\omega_{max}} \hat{\vec{E}}(\vec{x}, \omega) e^{-i\omega\tau} d\omega, \quad \vec{H}' = \vec{r} \times \vec{E}'$$

Poynting vector: $\vec{S} = \vec{E}' \times \vec{H}'$

$$W = \int \left\{ \int_{-\infty}^{+\infty} \vec{S}(\vec{x}, \tau) d\tau \right\} \cdot \vec{n} d\Omega \times \frac{I_{beam}}{e}$$

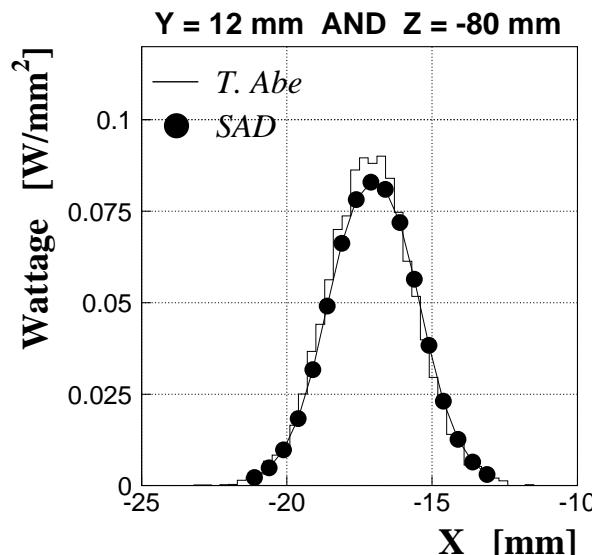
Example of My Calculation on QC3LE

at $Z = -8 \text{ cm}$



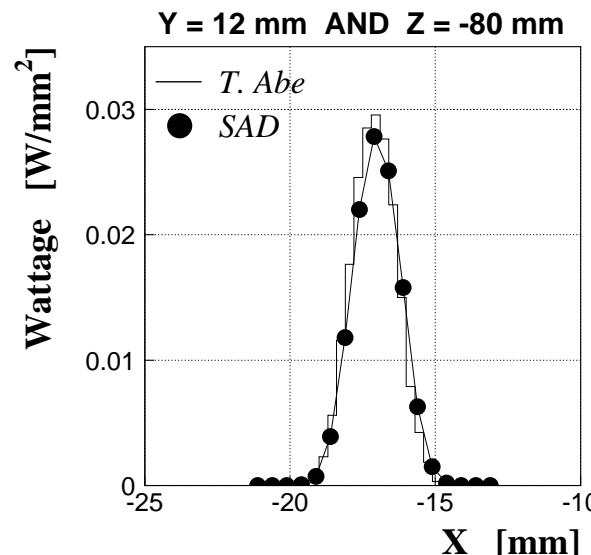
(X, Y, Z) : Belle coordinate system

$$I_{\text{HER}} = 780 \text{ mA}, \quad 0.1 < E_\gamma < 1 \text{ keV}$$

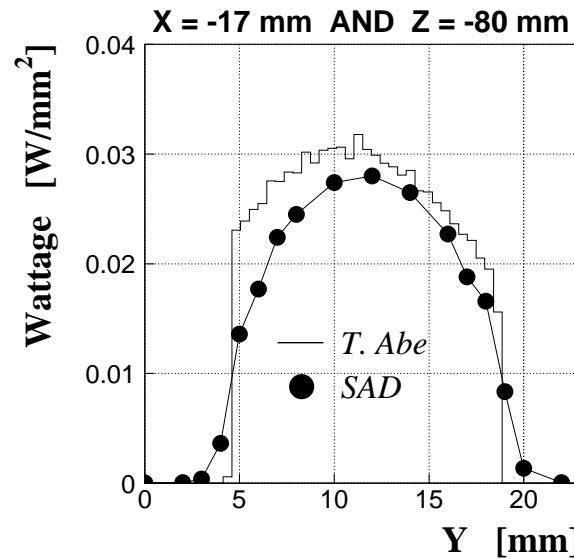
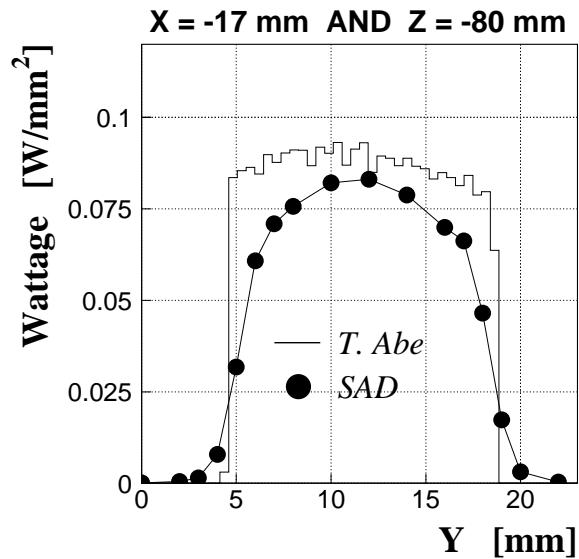


4.7 W
(T.Abe)
4.0 W (SAD)

$$I_{\text{HER}} = 780 \text{ mA}, \quad 1 < E_\gamma < 2 \text{ keV}$$

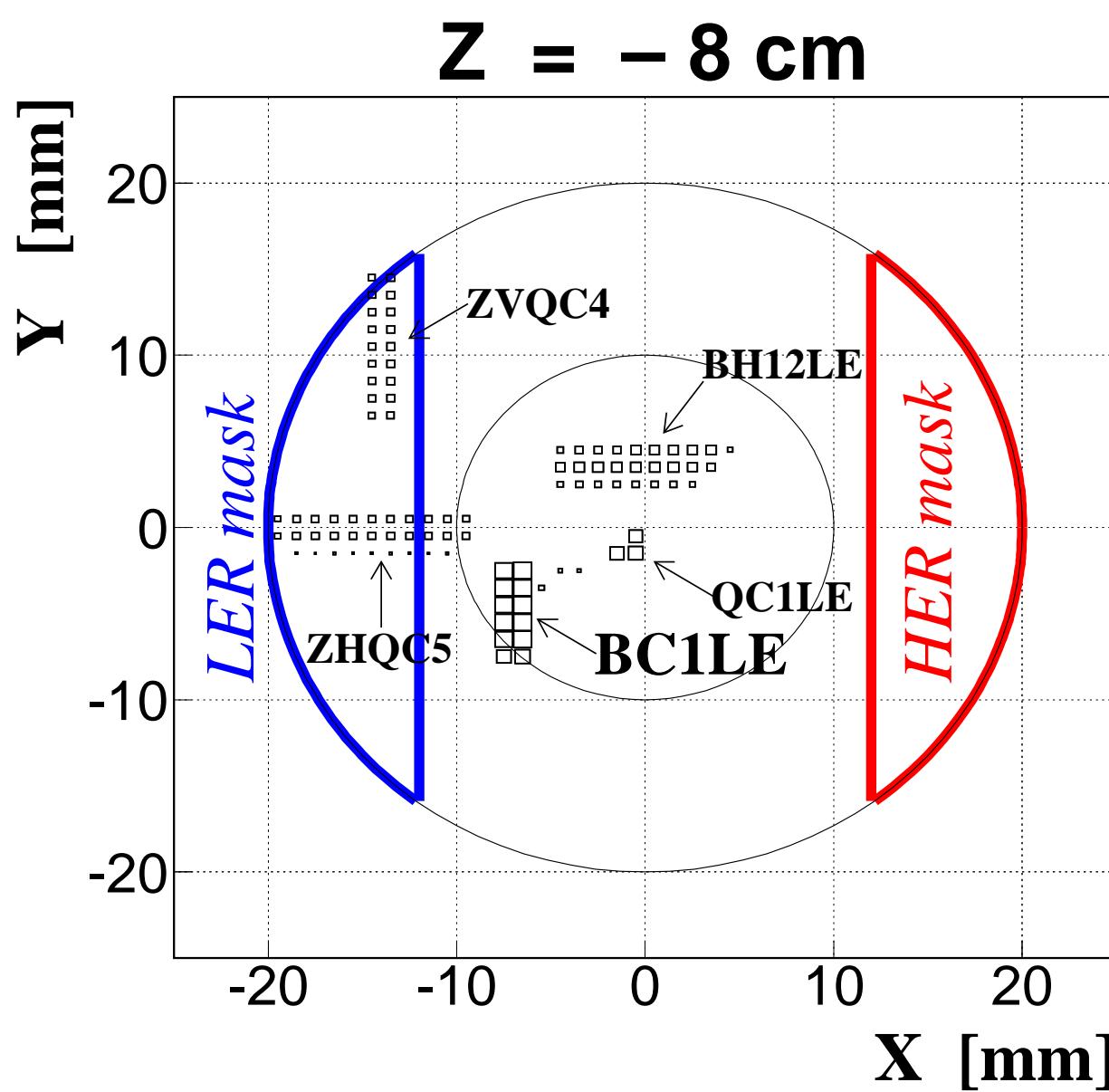


0.85 W (T.Abe)
0.75 W (SAD)



Conclusions on the Wattage Calculation

- ⇒ My geometry calculation is successful.
- ⇒ Good agreements on ψ distributions
- ⇒ Small differences on ϕ distributions:
→ $\sim 10\%$ higher than SAD results for $E_\gamma \sim 1 \text{ keV}$.



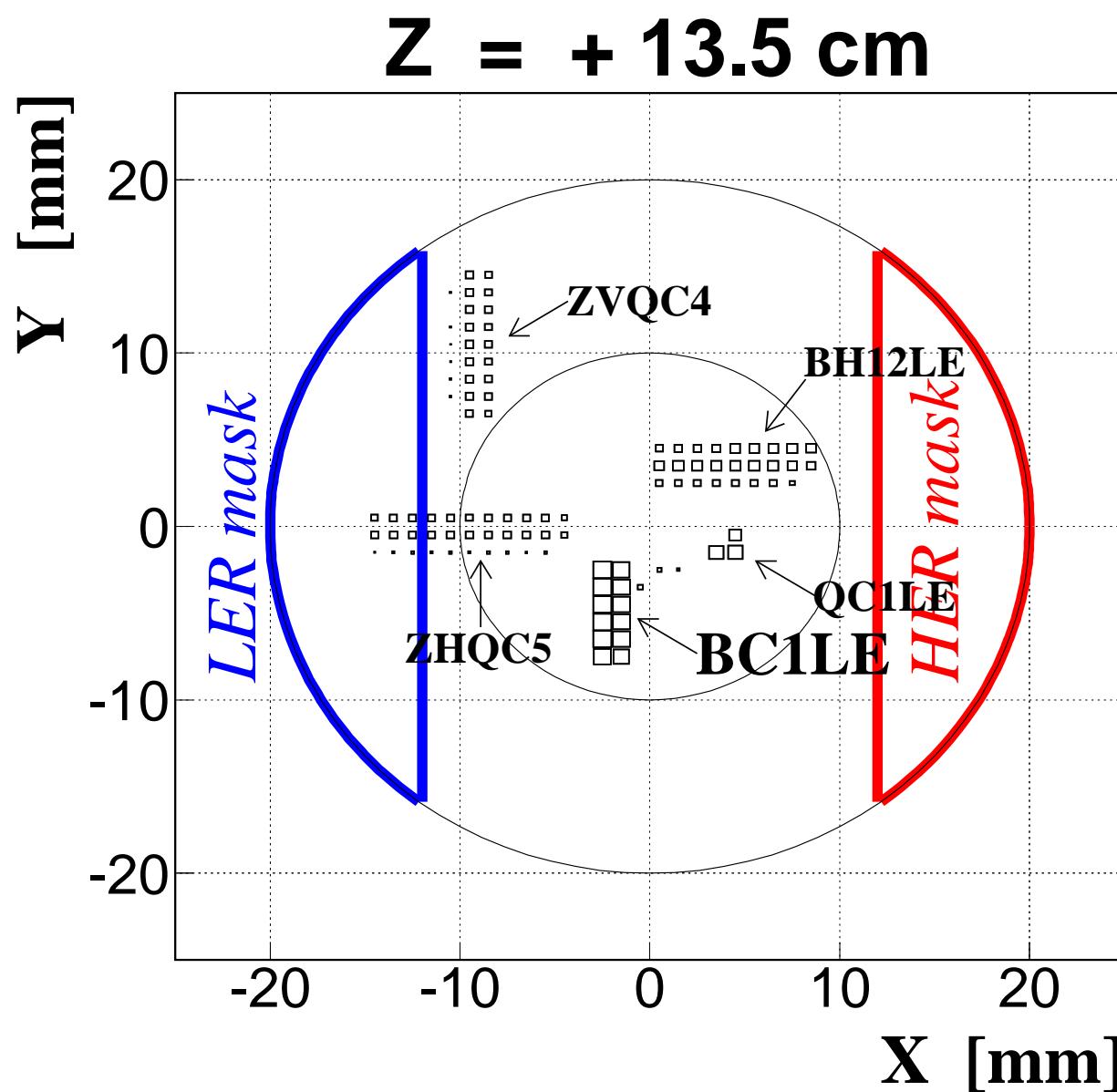
HER SR
(2001.11.07.13:00:00)

$$I_H^{ER} = 780 \text{ mA}$$

$$E_\gamma > 10 \text{ keV}$$

$$\Delta W_{MC}/W < 1\%$$

| Magnet | Wattage |
|--------|----------------------|
| BC1LE | 0.1 |
| BH1LE | 0.9×10^{-6} |
| BH2LE | 2.0×10^{-6} |
| ZVQC4 | 3.5×10^{-7} |
| ZHQC5 | 3.5×10^{-7} |
| QC1LE | 1.1×10^{-4} |
| QC2LE | 1.1×10^{-8} |



HER SR
(2001.11.07.13:00:00)

$$I_H^{ER} = 780 \text{ mA}$$

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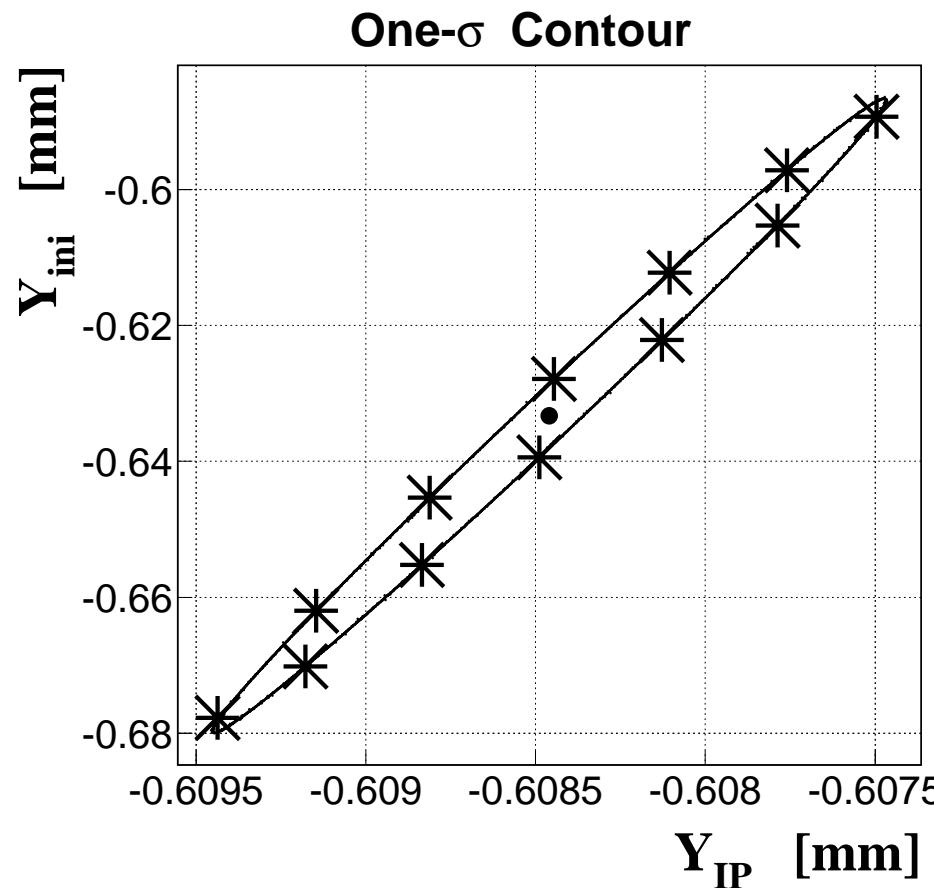
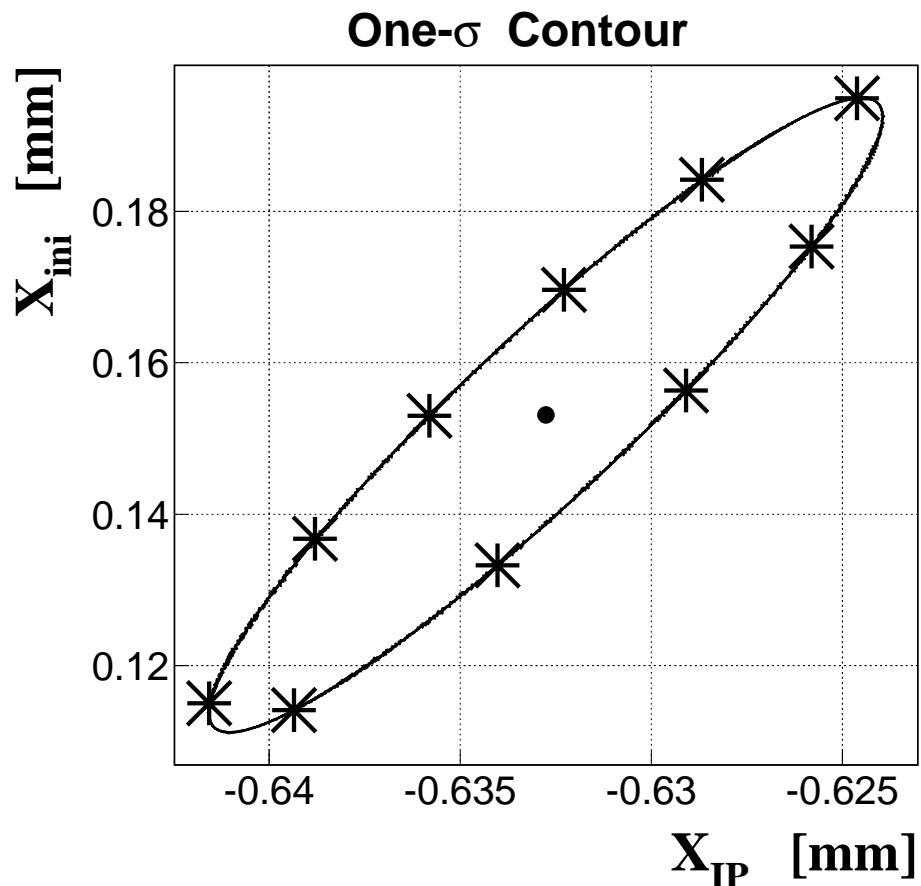
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Error Estimation

Errors on the BPM **resolutions** \oplus **offset** uncertainties are estimated.

- ⇒ Using the data on Nov. 7 (2001) at 1:00PM
- ⇒ If $\chi^2/ndf > 1 \Rightarrow \sigma_{BPM}^{(new)} \equiv \sigma_{BPM}^{(org)} \times \sqrt{\chi^2/ndf}$
so that $\chi^2(n^{ew})/ndf \equiv 1$.

The values at the asterisks are used.

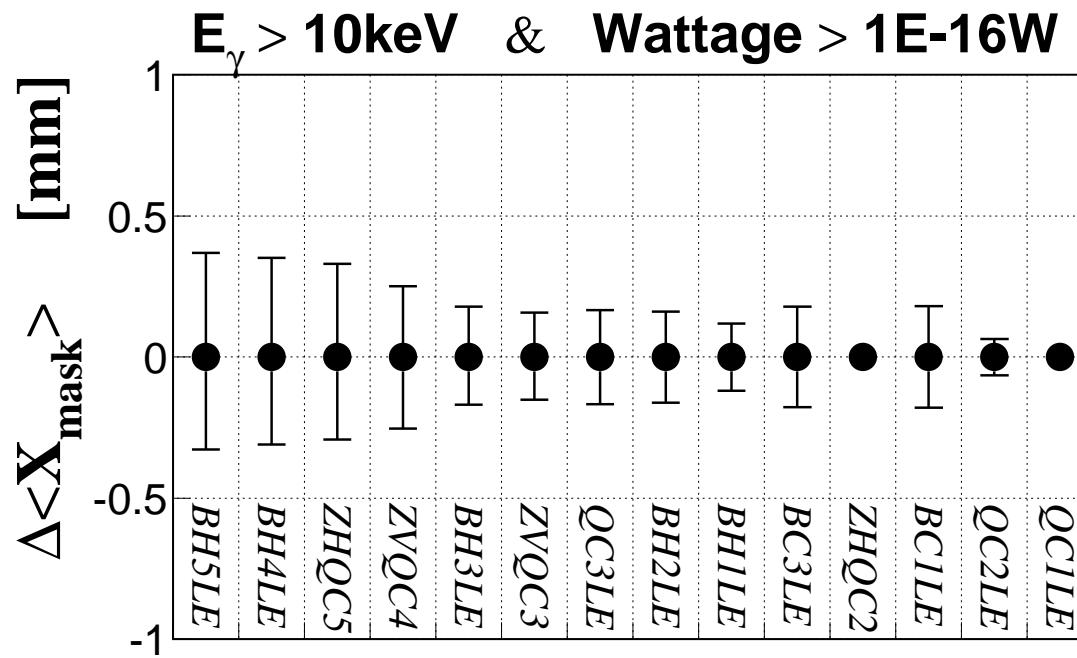


Position Errors

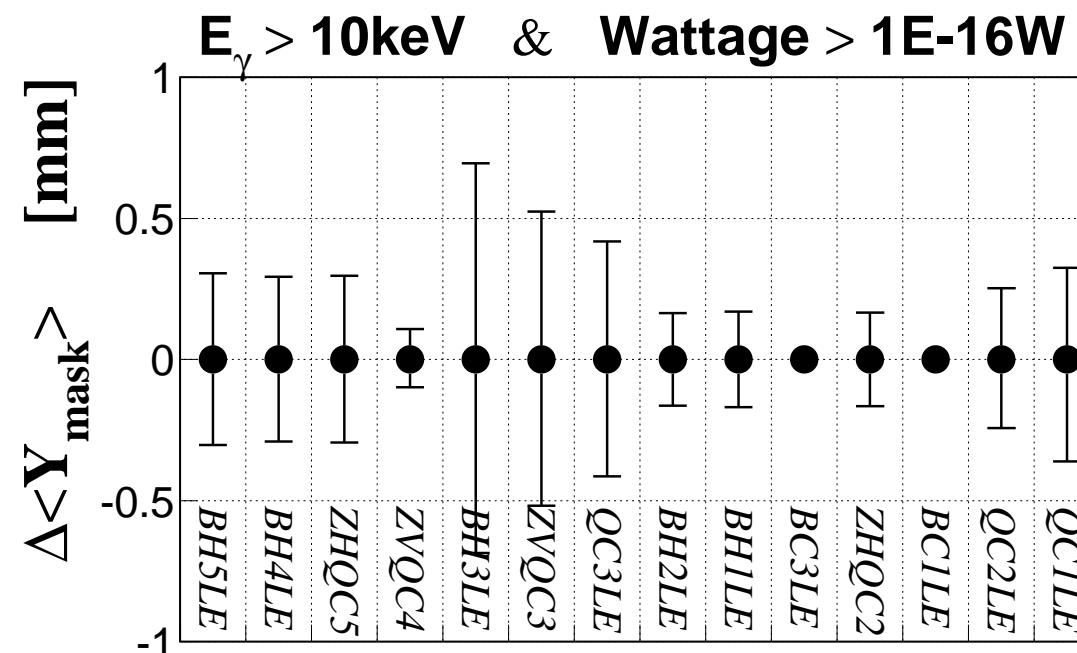
for

$$\langle X_{mask} \rangle \equiv \frac{\iint X \frac{d^2W(X,Y)}{dXdY} dXdY}{\iint \frac{d^2W(X,Y)}{dXdY} dXdY}$$

$$\langle Y_{mask} \rangle \equiv \frac{\iint Y \frac{d^2W(X,Y)}{dXdY} dXdY}{\iint \frac{d^2W(X,Y)}{dXdY} dXdY}$$

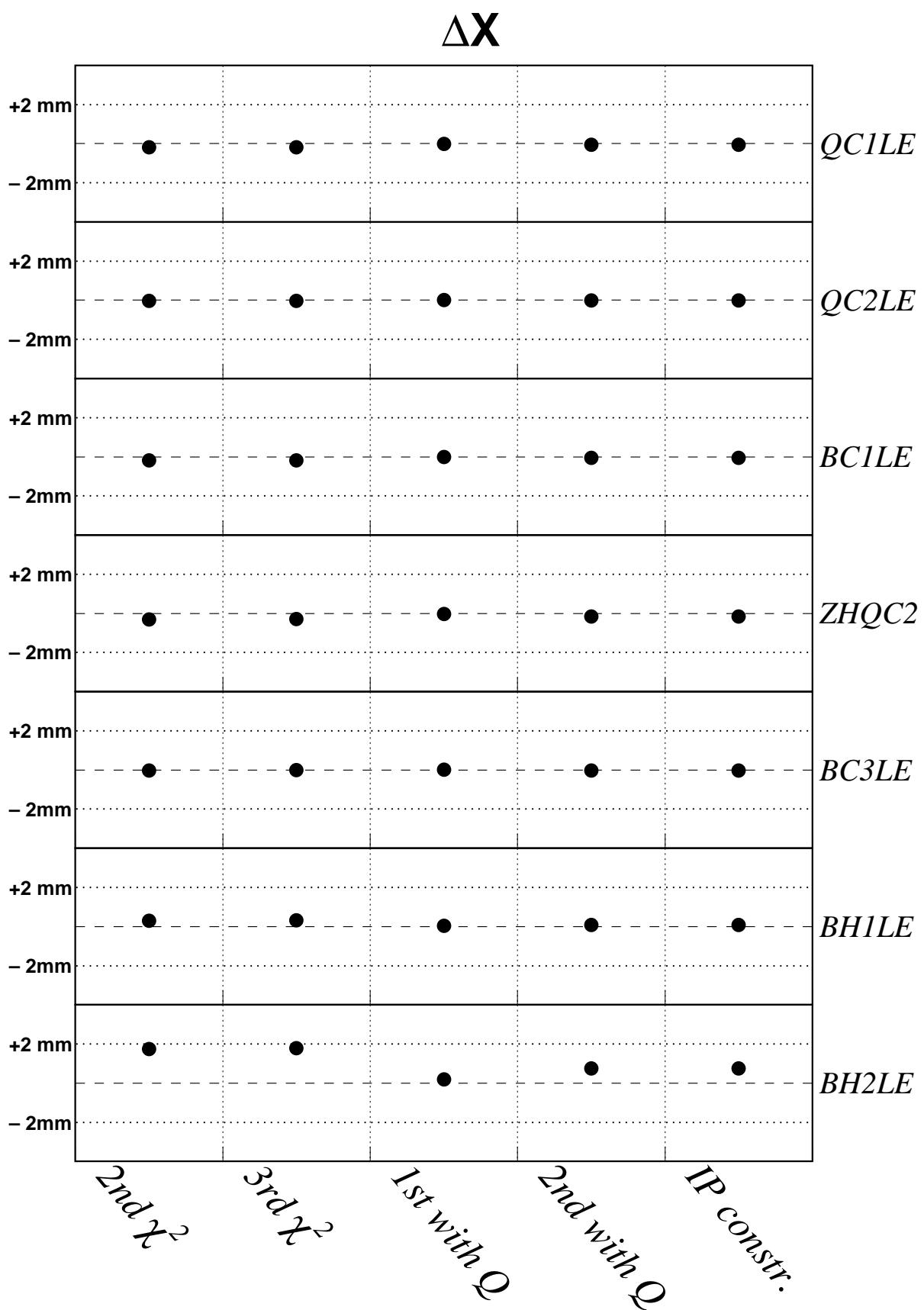


$$|\Delta X| \approx 0.2 \text{ mm}$$

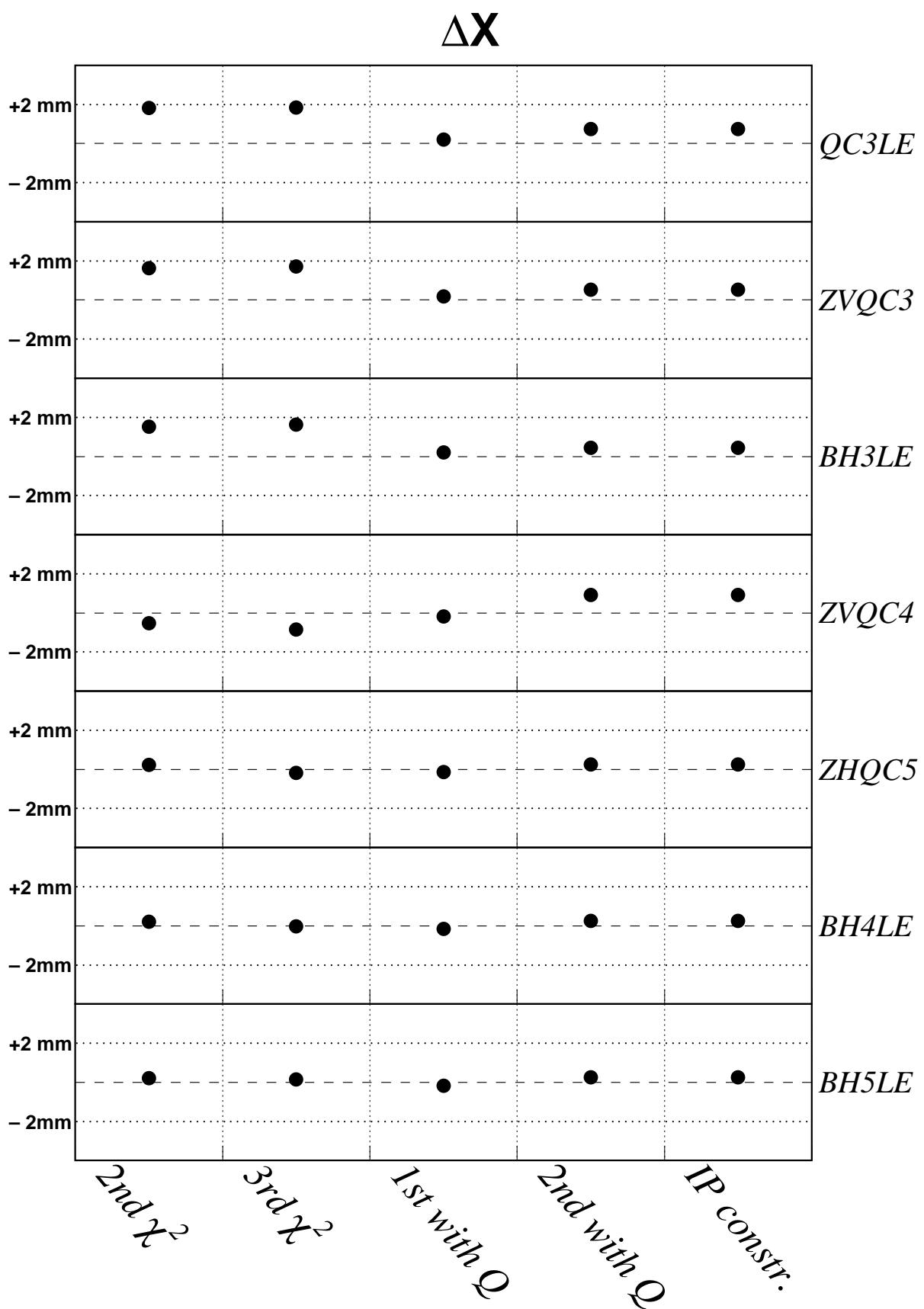


$$|\Delta Y| \approx 0.3 \text{ mm}$$

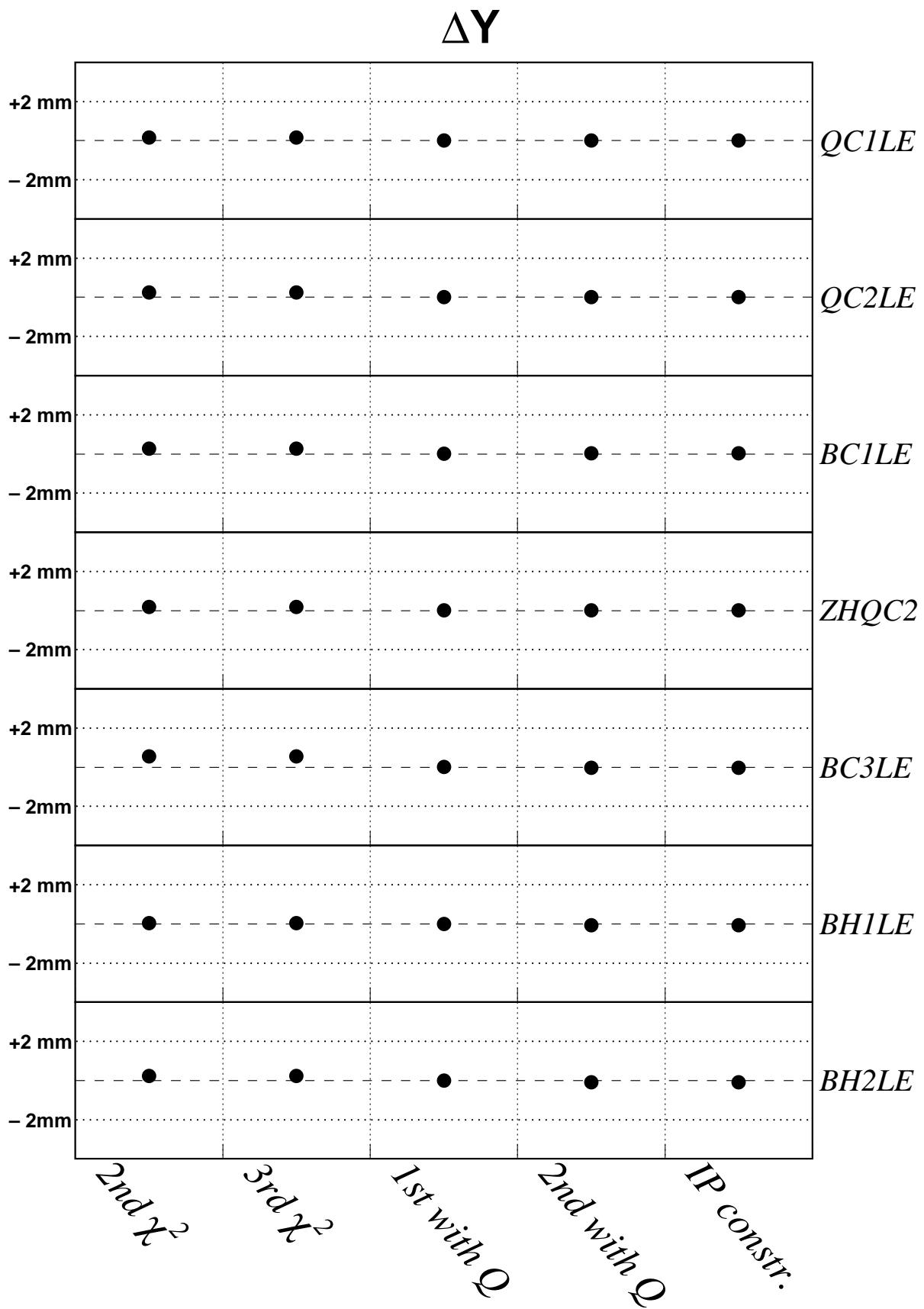
Horizontal Position Systematics (1)



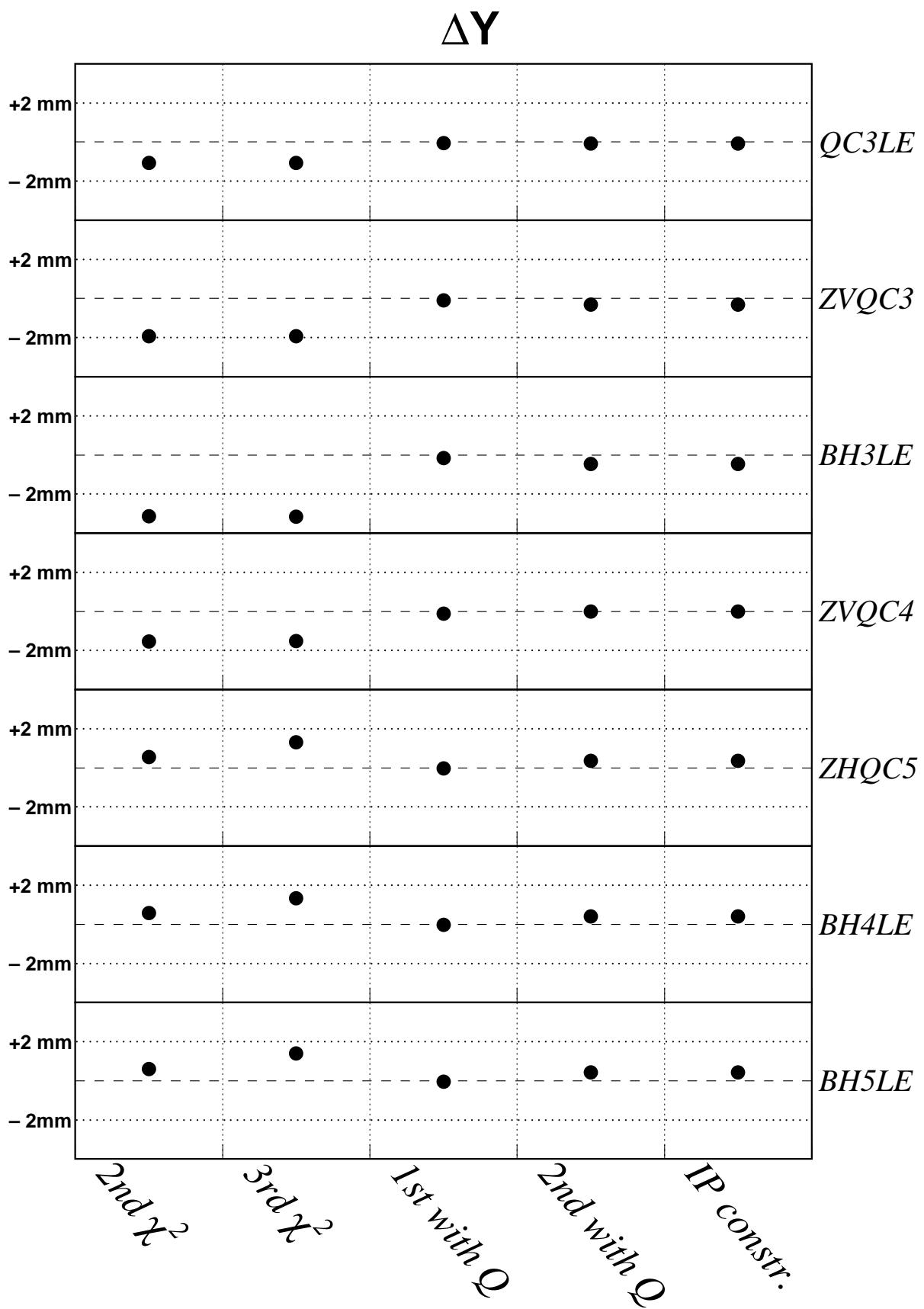
Horizontal Position Systematics (2)



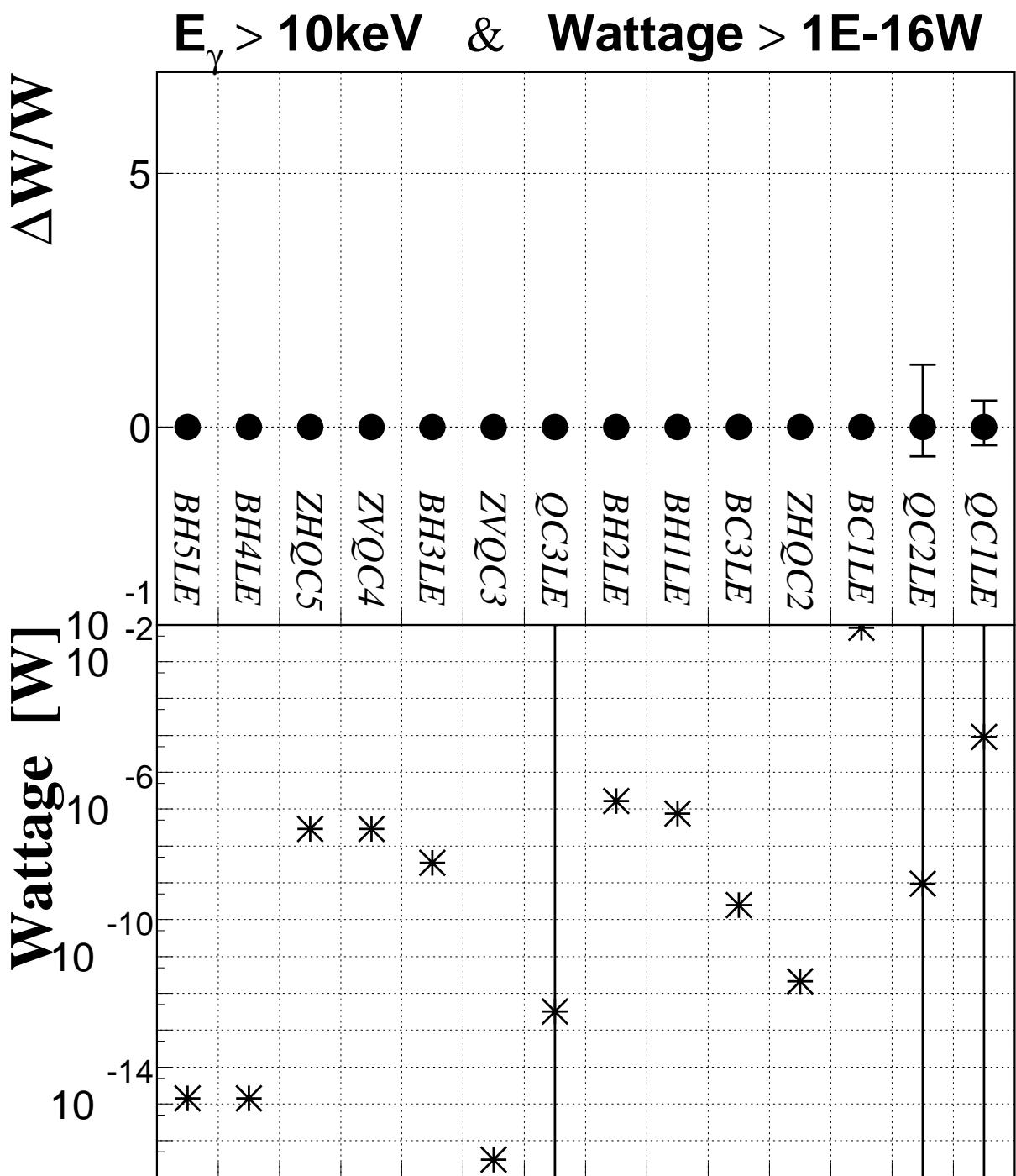
Vertical Position Systematics (1)



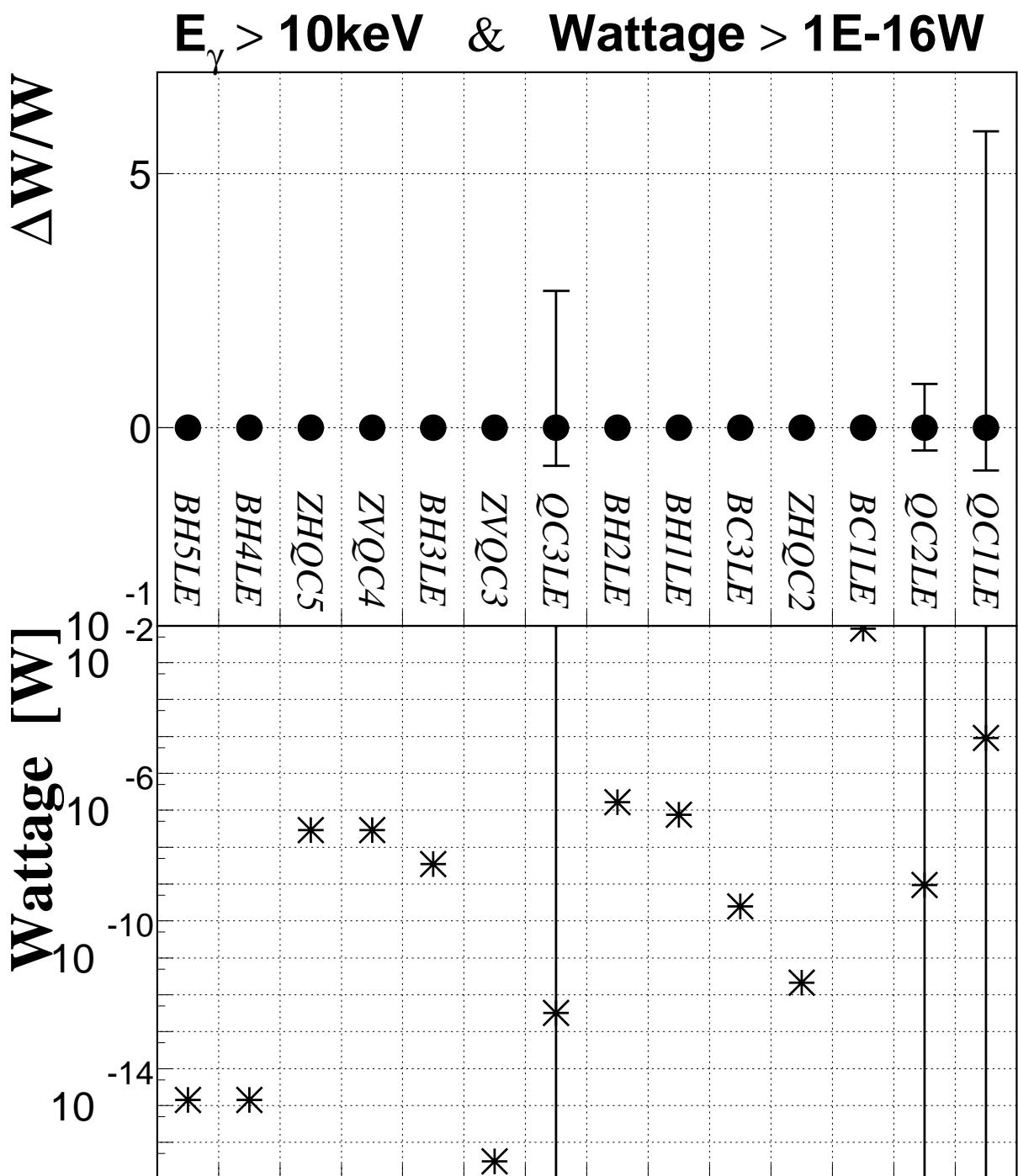
Vertical Position Systematics (2)



Wattage Errors on X

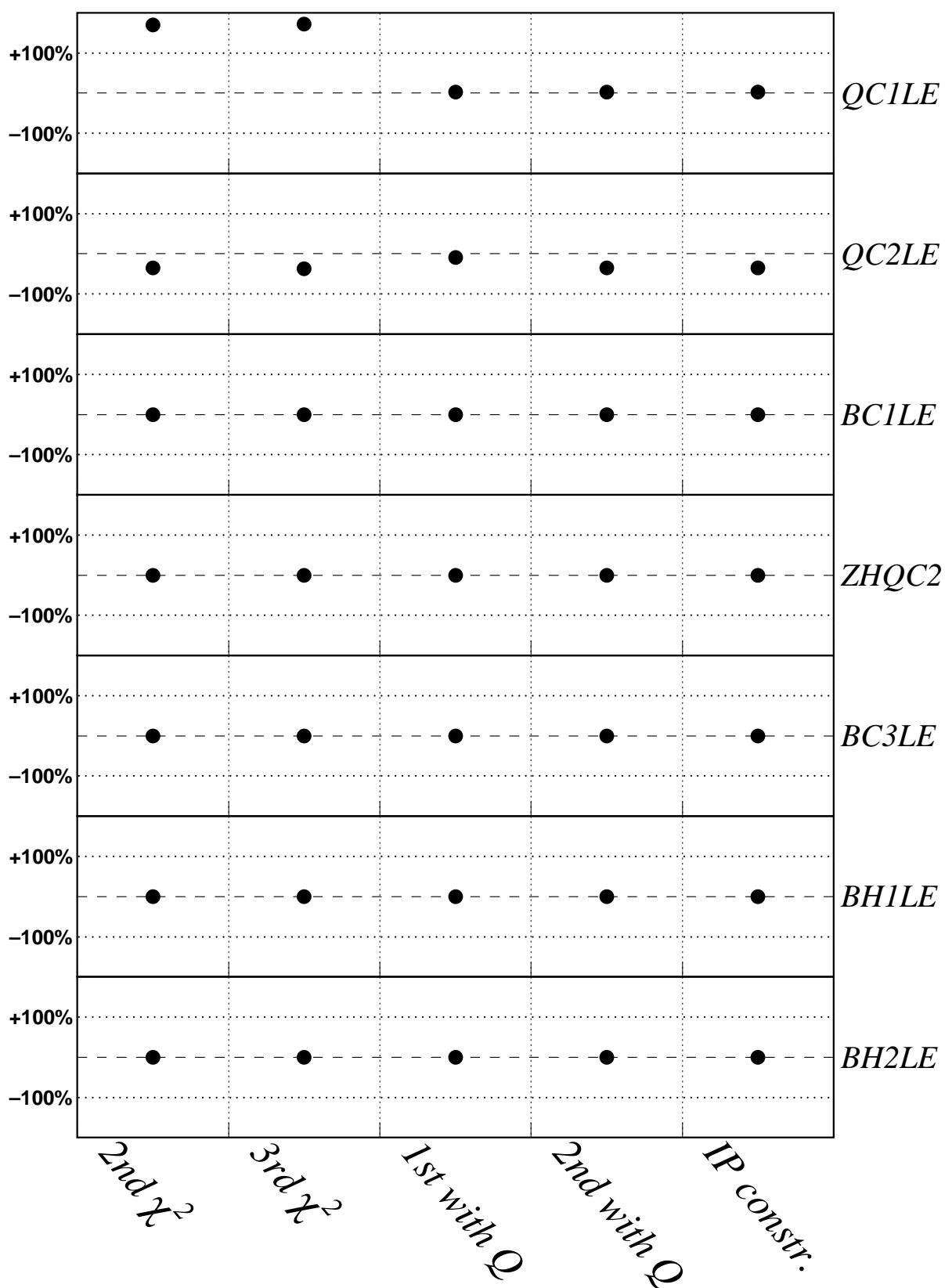


Wattage Errors on Y



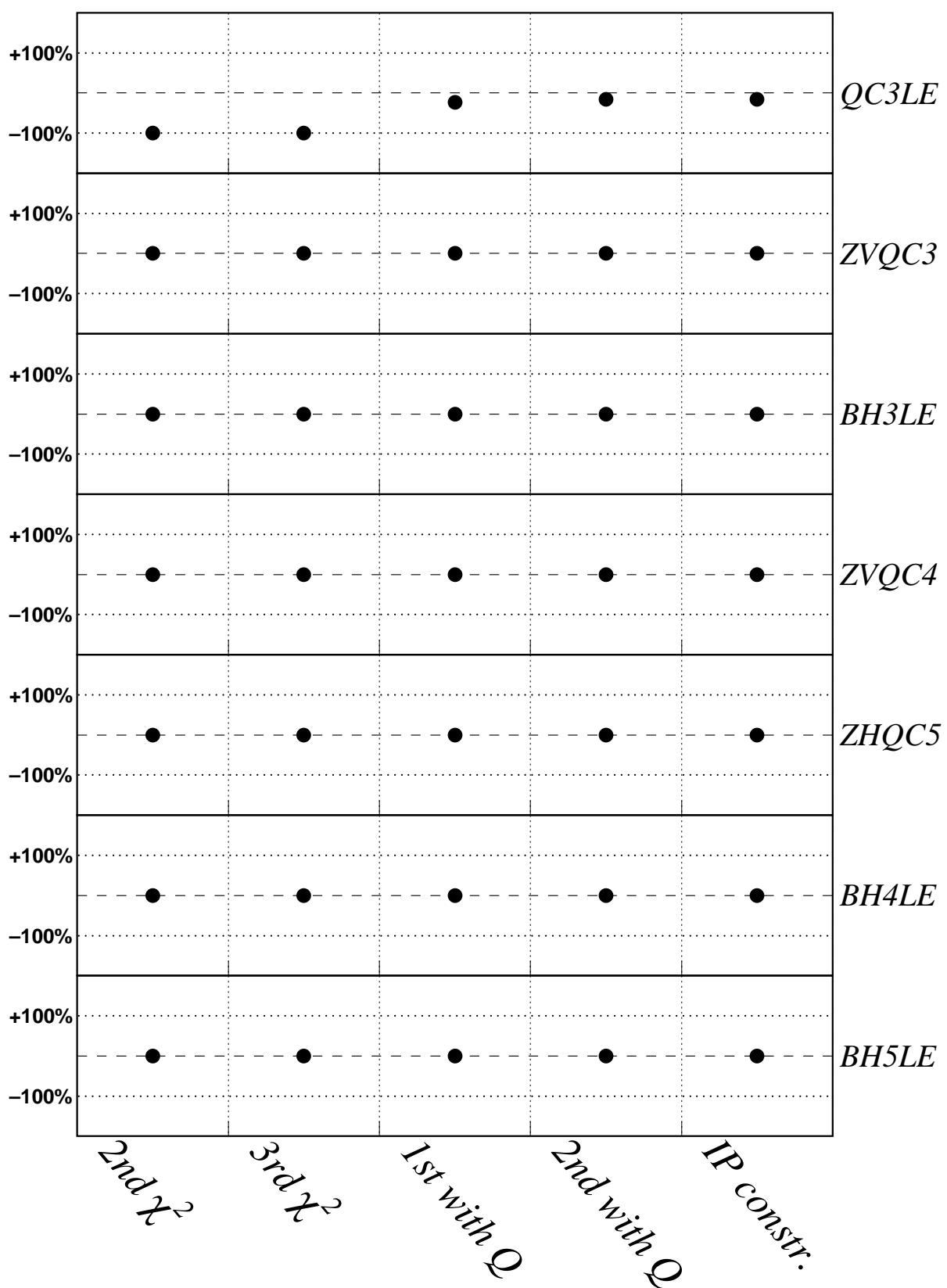
Wattage Systematics (1)

$\Delta W / W$

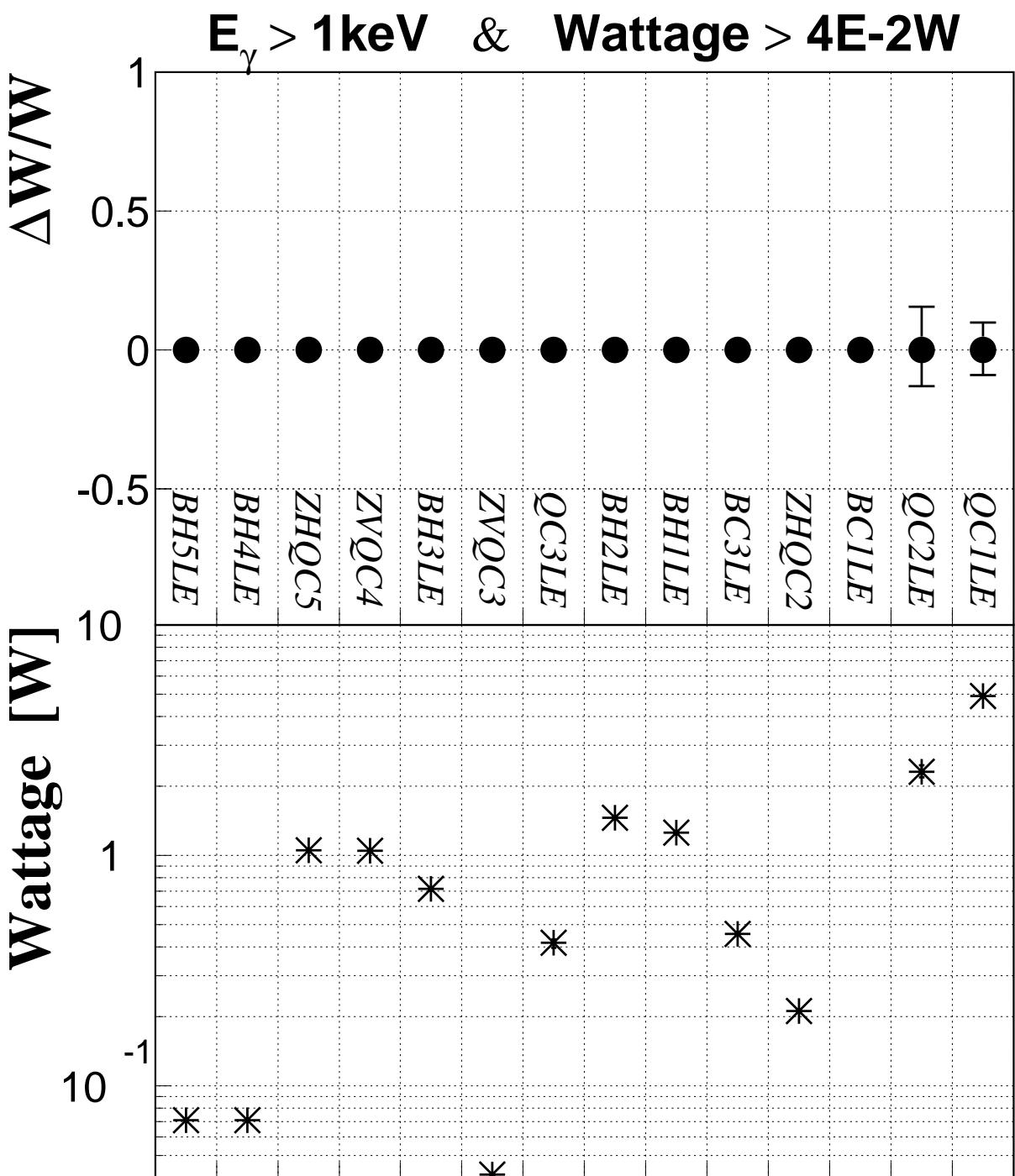


Wattage Systematics (2)

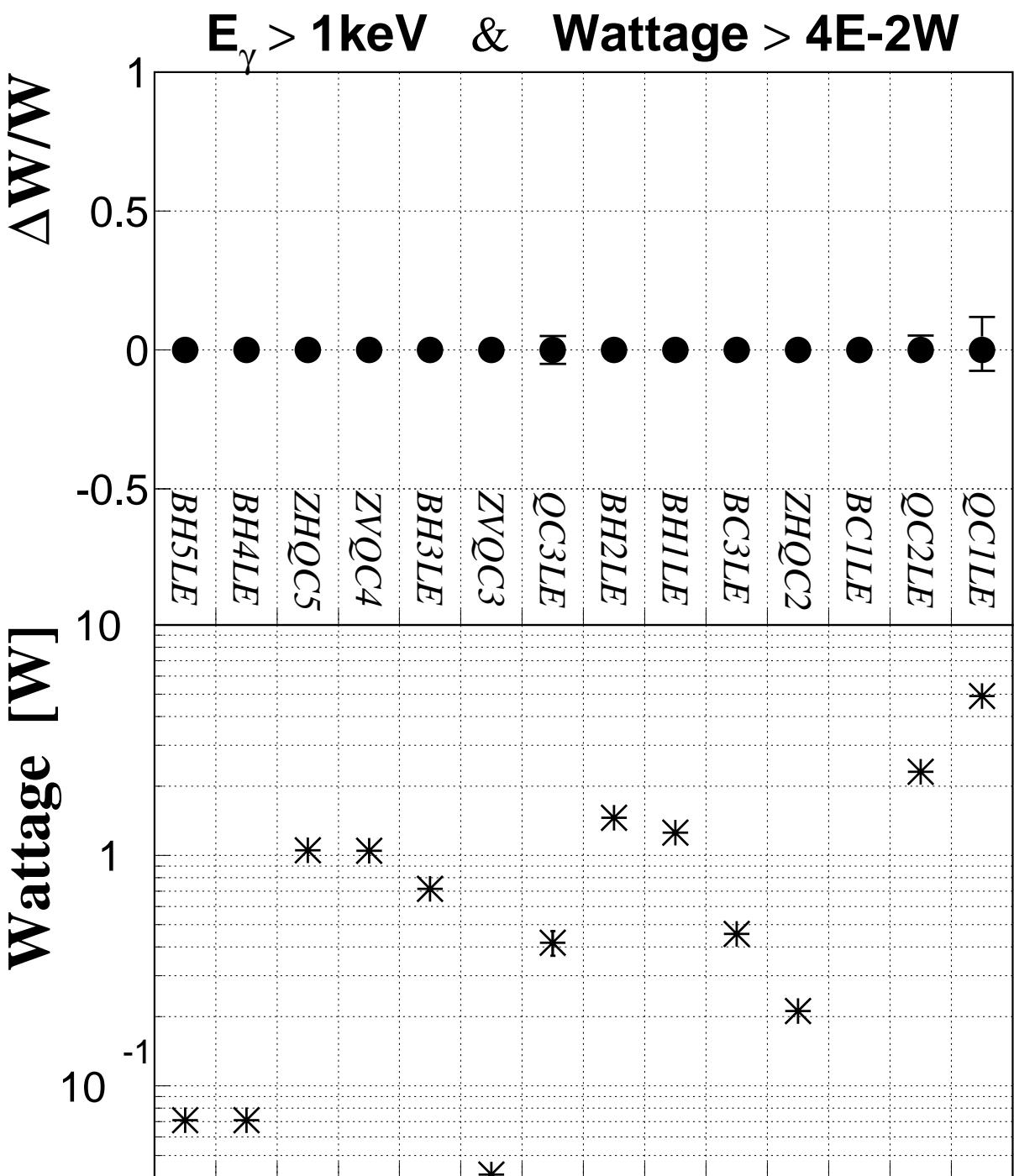
$\Delta W / W$



Wattage Errors on X

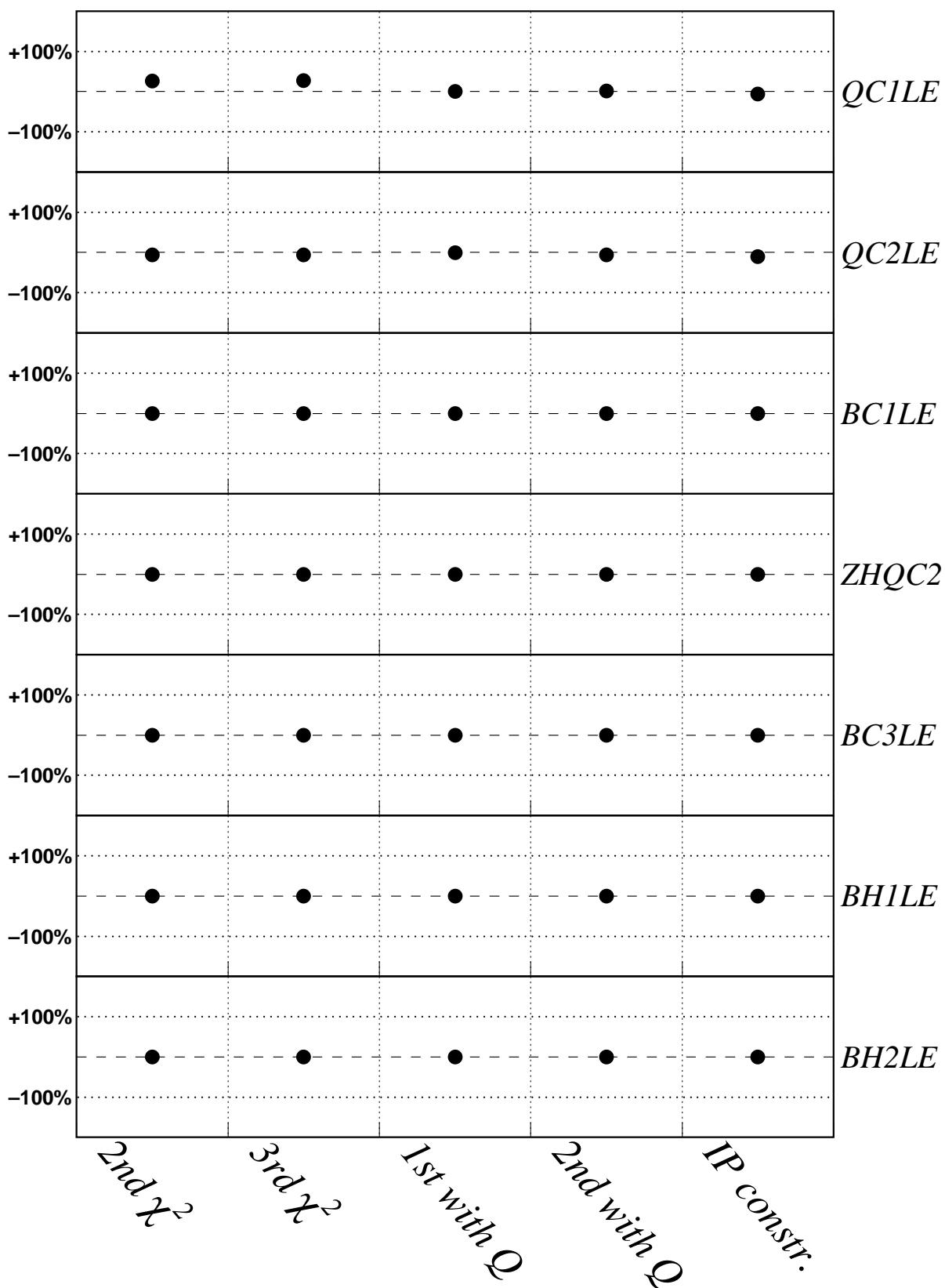


Wattage Errors on Y



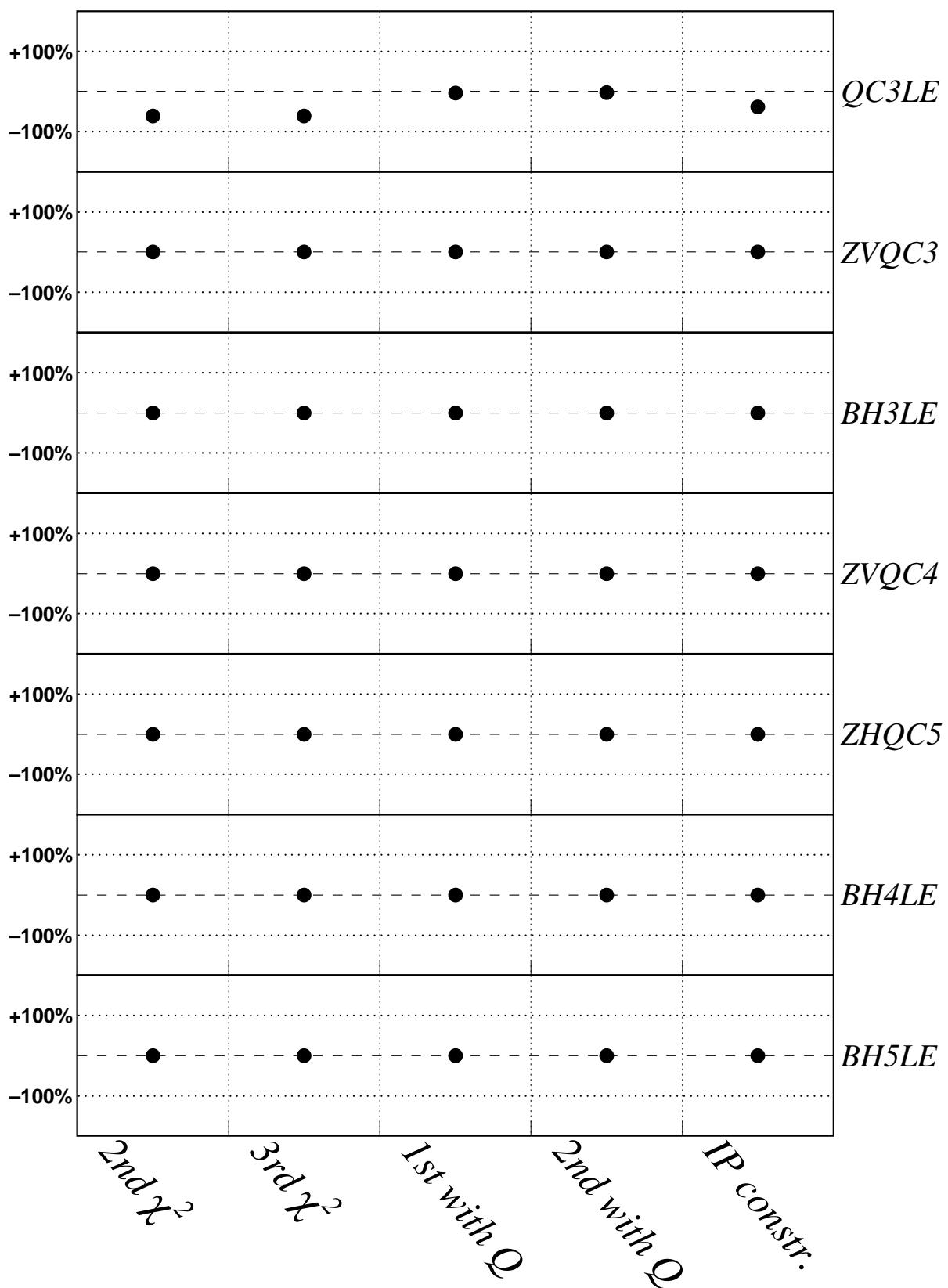
Wattage Systematics (1) ($E_\gamma > 1 \text{ keV}$)

$\Delta W / W$



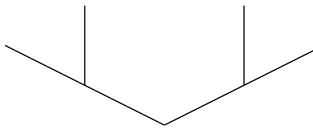
Wattage Systematics (2) ($E_\gamma > 1 \text{ keV}$)

$\Delta W / W$



Summary

**Methods of the real orbit and wattage calculations
have been established.**



Wattage distributions in the IR

- ⇒ My program has been checked comparing with the SAD results both on the orbit and wattage calculations.
- ⇒ Error estimations have been also done:
 - ⇒ $|\Delta < X >|, |\Delta < Y >| \sim 1 \text{ mm}$
 - ⇒ $\Delta W/W: 10 \sim 30\% \text{ for } E_\gamma > 1 \text{ keV},$
 $2 \sim 5 \quad \text{for } E_\gamma > 10 \text{ keV}$

Future Works

⇒ **For online monitoring**

- ⇒ Calculation speed: 3 ~ 4 sec / (fit & MC-integrations) → OK
- ⇒ Input parameters (BPM, k) are already available from the Belle NSM.

⇒ **Beam size**

→ to be implemented

⇒ **Transformation to the corresponding radiation dose**

→ not yet

- ⇒ Interface to EGS4

⇒ **Improvement of the offset determination algorithm**

- ⇒ Based on the current method
- ⇒ To reduce the wattage errors
- ⇒ More understanding on the real orbit calculation is needed.