Chromatic aberrations and Coherent Synchrotron Radiation in the KEKB and SuperKEKB

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Acknowledgements: G. Stupakov, K. Oide, Y. Cai, K. Ohmi, T. Agoh, K. Yokoya, Y. Funakoshi, Y. Ohnishi, Y. Seimiya and all KEKB group members

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Outline - Chromatic aberrations

1. Introduction 2. Chromatic aberrations (momentum-dependent nonlinearities) 2.1 Theory (Y. Seimiya, K. Ohmi, et al.) 2.2 Measurements (Y. Ohnishi, K. Ohmi, et al.) 2.3 Simulations (D. Zhou, K.Ohmi, et al.)

- 2.4 Observed luminosity performance
- **3. Summary**

KEKB B-Factory

Milestones since 2007

2007 Jan. Crab cavities installed
2007 Mar. Crab tuning started
2009 Apr. Skew-sext. installed
2009 Jun. Lum. → 2.11×10³⁴cm⁻²s⁻¹
2009 Nov. ∫Lum. → 1000 fb⁻¹
2010 Jun. KEKB shut down
2010 Jun. SuperKEKB officially approved











Ref. Y. Funakoshi, IPAC10 K. Hosoyama, EPAC08

Skew-sextupole





Ref. Y. Funakoshi, IPAC10



Machine parameters

Date	Nov.15 2006 before crab		Jun. 17 2009 with crab		
	LER	HER	LER	HER	
Current	1.65	1.33	1.64	1.19	А
Bunches	1389		1584		
Bunch current	1.19	0.96	1.03	0.750	mA
spacing	2.10		1.84		mA
emittance ϵ_x	18	24	18	24	nm
βx [*]	59	56	120	120	cm
β _y *	6.5	5.9	5.9	5.9	mm
σ _x @IP	103	107	147	170	μm
σ _y @IP	1.8	1.8	0.94	0.94	μm
Vx	45.505	43.534	45.506	44.511	
Vy	44.509	41.565	43.561	41.585	
Vs	-0.0246	-0.0226	-0.0246	-0.0209	
beam-beam ξ_x	0.117	0.070	0.127	0.102	
beam-beam ξ_y	0.108	0.058	0.129	0.090	
Luminosity	17.6		21.08		10 ³³ cm ⁻² s ⁻¹

NOTE: With crab cavities installed, β_x^* could not be small enough due to poor beam lifetime.

Ref. Y. Funakoshi, IPAC10

Chromatic aberration - Theory

The ideas:

All machine parameters depend on momentum deviation.
 Extend Courant-Snyder formalism to off-momentum particles.
 Re-construct the symplectic map in 6-D phase space to include the crosstalk between betatron and synchrotron motion.
 Implement the map for chromatic aberrations in beam-beam simulations.

Evaluate the luminosity loss using simulations.

Chromatic aberrations (definition):

$$\alpha_{u}(\delta) = \sum_{i=0}^{\infty} \alpha_{ui} \delta^{i} \qquad \beta_{u}(\delta) = \sum_{i=0}^{\infty} \beta_{ui} \delta^{i}$$
$$\nu_{u}(\delta) = \sum_{i=0}^{\infty} \nu_{ui} \delta^{i} \qquad r_{j}(\delta) = \sum_{i=0}^{\infty} r_{ji} \delta^{i}$$
$$u = x, y \quad \text{and} \quad j = 1, 2, 3, 4,$$
$$\delta = (p - p_{0})/p_{0}$$

NOTE:

Chromatic aberrations can be estimated using optics codes or measured using beam.

Y. Seimiya, et al., to be published. D. Zhou, et al., PRST-AB 13, 021001 (2010).

Chromatic aberration - Simulations

9

Luminosity loss due to all chromatic aberrations:



FIG. 5. (Color) Specific luminosity as a function of current product for KEKB. The natural chrom. and measured chrom. indicate natural chromaticity and measured chromaticity calculated from ideal optics and measurement data at KEKB HER, respectively. The WS and SS represent weak-strong and strongstrong simulations, respectively.

WS: weak-strong SS: strong-strong

$$\beta_x^* = 0.9m$$
 $\beta_y^* = 6mm$
 $\nu_x = 44.515$ $\nu_y = 41.606$
 $\kappa = 1\%$

NOTE: Luminosity loss: WS: ~5% SS: ~10%

Chromatic aberration - Simulations

Scan with first-order chromaticity of X-Y couplings (WS, Crab on):



NOTE: Simulations predicted significant luminosity loss. No particle loss was observed.

D. Zhou, et al., PRST-AB 13, 021001 (2010).

Chromatic aberration - Simulations Linear and chromatic X-Y couplings at the SuperKEKB: Set the tolerances for the reference of optics design and optics corrections

II



Figure 1: Beam sizes and relative luminosity as function of the linear X-Y couplings at the IP with and without crab waist.



with 1000 error seeds for the SuperKEKB LER.



Figure 2: Beam sizes and relative luminosity as function of the chromatic X-Y couplings at the IP with and without crab waist.

Table 3: Tolerances for the linear and chromatic X-Y couplings at the IP of the SuperKEKB LER, assuming a rate of 20% luminosity degradation.

Parameter	w/ crab waist	w/o crab wais	st
r_1^* (mrad)	±5.3	±3.5	1
r_2^* (mm)	± 0.18	±0.13	
$r_3^{*}(m^{-1})$	±55	±15	Toloropoo
r_4^* (rad)	± 1.4	± 0.4	Tolerance
$r_{11}(rad)$	± 2.3	± 2.0	
$r_{21}(m)$	±0.09	± 0.07	
$r_{31}(m^{-1})$	± 11000	± 9400	
$r_{41}(rad)$	±430	± 280	

D. Zhou, et al., IPAC10



Typical examples of scanning chromatic X-Y couplings at IP during the KEKB operation:





Ref. Y. Funakoshi, IPAC10

Effectiveness of skew-sextupole magnets (crab on)



Ref. Y. Funakoshi, IPAC10

I4

Effectiveness of skew-sextupoles (Crab off)



Specific luminosity (crab on/off)



Luminosity improvement by crab cavities is about 20%. Geometrical loss due to the crossing angle is about 11%.

Beam-beam parameter (crab on/off)



Ref. Y. Funakoshi, IPAC10

Summary - Chromatic aberrations

The theory of chromatic aberrations looks pretty good.
The simulations were quite reliable and did lead to the remarkable achievements in KEKB.

The beam tuning in the KEKB revealed that chromatic X-Y couplings are very important in the KEKB.

- The crab cavities did contribute to luminosity gain (~20%).
- The skew-sextupoles contributed additional luminosity gain (~15%).

♦ But the strong-strong simulations predicted the luminosity gain in a factor of $2(@\beta_x^*=0.8m)$. There is still big discrepancy.

Outline - CSR

1. Introduction 2. Algorithms **3. Benchmark results** 3.1 Single dipole 3.2 Wiggler/undulator 4. CSR in wigglers 4.1 KEKB LER 4.2 SuperKEKB LER 5. Fringe field and interference 5.1 KEKB LER 5.2 SuperKEKB DR 6. Summary

Introduction

Motivations:

 To find out the unknown source of longitudinal impedance which drive the microwave instability (MWI) in the KEKB LER
 To work out a reliable impedance model for SuperKEKB DR
 CSR in wigglers, with interference, or with resistive wall

Existing publications on numerical calculations of CSR impedance:

1. T. Agoh and K. Yokoya, PRST-AB 7, 054403 (2004) and T. Agoh, PhD. Thesis (2004)

2. K. Oide, Presentation at KEKB ARC 2009 and PAC09

3. G. Stupakov and I. Kotelnikov, PRST-AB 12, 104401 (2009)

Algorithms - Fundamental equations

Parabolic equation in curvilinear coordinate system:

$$\frac{\partial \vec{E}_{\perp}}{\partial s} = \frac{i}{2k} (\nabla_{\perp}^2 \vec{E}_{\perp} - \mu_0 c^2 \nabla_{\perp} \rho_0 + \frac{2k^2 x}{\rho(s)} \vec{E}_{\perp})$$

Field separation:

$$\vec{E}_{\perp} = \vec{E}_{\perp}^r + \vec{E}_{\perp}^b$$

$$\frac{\partial \vec{E}_{\perp}^r}{\partial s} = \frac{i}{2k} [\nabla_{\perp}^2 \vec{E}_{\perp}^r + \frac{2k^2 x}{\rho} (\vec{E}_{\perp}^r + \vec{E}_{\perp}^b)]$$

Beam field in free space (independent of s):

$$\frac{\partial^2 E_x^b}{\partial x^2} + \frac{\partial^2 E_x^b}{\partial y^2} = \mu_0 c^2 \frac{\partial \rho_0}{\partial x}$$
$$\frac{\partial^2 E_y^b}{\partial x^2} + \frac{\partial^2 E_y^b}{\partial y^2} = \mu_0 c^2 \frac{\partial \rho_0}{\partial y}$$

Ref. T. Agoh and K. Yokoya, PRST-AB 7, 054403 (2004)

β=1

Algorithms - Beam field

Beam field in free space with finite beam sizes Typical beam size: $\sigma_x=0.5$ mm, $\sigma_y=0.01$ mm (bi-gaussian)

$$\begin{split} E_x(x,y) &= \frac{\lambda(k)}{2\epsilon_0\sqrt{2\pi(\sigma_x^2 - \sigma_y^2)}} \mathrm{Im}[F(x,y)] \\ E_y(x,y) &= \frac{\lambda(k)}{2\epsilon_0\sqrt{2\pi(\sigma_x^2 - \sigma_y^2)}} \mathrm{Re}[F(x,y)] \\ F(x,y) &= w(\frac{x+iy}{\sqrt{2(\sigma_x^2 - \sigma_y^2)}}) - e^{-\frac{x^2}{2\sigma_x^2} - \frac{y^2}{2\sigma_y^2}} w(\frac{\frac{\sigma_y}{\sigma_x}x + i\frac{\sigma_x}{\sigma_y}y}{\sqrt{2(\sigma_x^2 - \sigma_y^2)}}) \\ w(z) &= e^{-z^2}(1 + \frac{2i}{\sqrt{\pi}}\int_0^z e^{t^2}dt) \end{split}$$

Ref. T. Agoh, Ph.D. Thesis (2004)

Algorithms - Beam pipe

Model of the beam pipe:

1. The bending radius can be arbitrarily s-dependent, which allows for treating fringe field, wigglers or a series of dipole magnets

2. Uniform rectangular cross section along the beam orbit (simply the calculation)

"Wiggling pipe"

Field integration along s:

Toroidal part: Numerical integration
 Straight pipe: mode expansion

Ref. T. Agoh, Ph.D. Thesis (2004) G. Stupakov and I. Kotelnikov, PRST-AB 12, 104401 (2009)

Algorithms - Mesh

Finite-difference discretization:1. Staggered grid: Central difference2. Ghost point: Boundary conditions with perfect wall



Benchmark results - Single dipole

25

Re.Z_L(k)

Im.Z_L(k)

Collaborate with K. Marit





Fluctuation in impedance is due to reflections of side walls (see Oide's talk)

ANKA w/h=70/32mm L_{bend}=2.183m p=5.559m L_{exit}=Infinity (pipe after exit) X_{offset}=0mm

Benchmark results - Single dipole

500

0

-500

0

Im[Z] (Ohm)

Re.Z_L(k)

Im.Z_L(k)

Oide's code Stupakov's code Zhou's code(TA)

Zhou's code(KO)

Parallel plates

2000







w/h=60/40mm L_{bend}=4m p=16.3m L_{exit}=Infinity (pipe after exit) X_{offset}=0mm

 $k(m^{-1})$

4000

6000

8000

TA: Agoh's algorithm

KO: Oide's algorithm

10000

Benchmark results - Single dipole

Re.Z_L(k)





TA: Agoh's algorithm KO: Oide's algorithm



w/h=60/40mm L_{bend}=4m p=16.3m L_{exit}=Infinity (pipe after exit) X_{offset}=-20mm (To inner wall)

Benchmark results - Wiggler

28

Re.Z_L(k)





 $Im.Z_{L}(k)$

 $W_L(s)$ with $\sigma_z=0.3$ mm 40 hou's code(TA) JRS theory 20 WL (V/pC) C -20-40 -60 0.004 0.006 0.008 0.010 0.012 $-0.002 \ 0.000 \ 0.002$

s (m)

JRS: Wu-Stupakov-Raubenheimer theory J. Wu et al., PRST-AB 6, 040701 (2003)

> N_{period}=10 w/h=94/94mm type $\lambda_w = 1.088 \text{m}$ ρ=15.483m L_{exit}=Infinity (pipe after exit) Xoffset=0mm

KEKB-LER

Benchmark results - Wiggler

Re.Z_L(k)







Note: "Wiggling pipe" is not good enough! $N_{period}=10$ $\lambda_w=1.088m$ $\rho=154.83m$ $L_{exit}=Infinity (pipe after exit)$ Xoffset=0mm

CSR in wigglers - KEKB LER

Re.Z_L(k)





 $W_L(s)$ with $\sigma_z=0.3$ mm



 $N_{period} = \frac{1}{2}/\frac{3}{10}$ w/h=94/94mm $\lambda_w = 1.088m$ $\rho = 15.483m$ $L_{exit} = Infinity (pipe after exit)$ Xoffset=0mm Field distribution: Cosine

CSR in wigglers - Hard-edge approximation

Re.Z_L(k)



Field distribution





H.E. model looks to be good? $N_{period}=1/10$ w/h=94/94mm $\lambda_w=1.088m$ $\rho=15.483m$ $L_{exit}=Infinity$ (pipe after exit) Xoffset=0mm (To inner wall) Field distribution: Cosine/H.E.

CSR in wigglers - SuperKEKB LER

Z_L(k) ,1 Super-period







Field distribution



N_{super-period}=1/15w/h=90/90mm L_w=140m $\rho \approx 15m$ L_{exit}=Infinity (pipe after exit) Xoffset=0mm Field distribution: Hard-edge

Fringe field - KEKB LER

Re.Z_L(k)

Im.Z_L(k)



Interference - KEKB LER

Re.Z_L(k)



Single dipole 150 Two dipoles 100 Im[Z] (Ohm) 50 0 -50 -1002000 4000 6000 8000 10000 0 k (*m*⁻¹)

 $Im.Z_{L}(k)$



Two dipoles w/h=94/94mm $L_{bend}=0.89m$ $L_{drift}=5.65m$ $\rho=15.872m$ $L_{exit}=Infinity (pipe after exit)$ Xoffset=0mm

Interference - KEKB LER

Re.Z_L(k)







Two dipoles w/h=94/94mm $L_{bend}=0.89m$ $L_{drift}=20m$ $\rho=15.872m$ $L_{exit}=Infinity$ (pipe after exit) Xoffset=0mm



SuperKEKB DR parameters

parameter	Value	
Beam energy (GeV)	1.1	
Circumference (m)	135.502	
Bunch Length (mm)	11.1	
Rel. Energy spread (10-4)	5.53	
Beam pipe height in bends (mm)	34	
Beam pipe width in bends w/o antechamber (mm)	34	
Effective Length of bends (B1/B2/B3/B4)	0.74248/0.28654/0.39208/.47935	
Number of bends (B1/B2/B3/B4)	32/38/4/4	
Bending radius (m) (B1/B2/B3/B4)	2.68/2.96/3.15/3.15	



Re.Z_L(k)

 $Im.Z_{L}(k)$





 $W_L(s)$ with $\sigma_z=0.3$ mm



1 cell w/h=34/34mm B1+B2 L_{drift}=0.93m L_{exit}=Infinity (pipe after exit) Xoffset=0mm

Re.Z_L(k)

 $Im.Z_{L}(k)$





 $W_L(s)$ with $\sigma_z=0.3$ mm



2 cells w/h=34/34mm 2×(B1+B2) L_{drift}=0.93m L_{exit}=Infinity (pipe after exit) Xoffset=0mm

Re.Z_L(k)

Im.Z_L(k)





 $W_L(s)$ with $\sigma_z=0.3$ mm



16 cells w/h=34/34mm 16×(B1+B2) L_{drift}=0.93m L_{exit}=Infinity (pipe after exit) Xoffset=0mm

Summary - CSR

1. Features of the new CSR code (CSRZ):

1.1 Low noise level

1.2 Allow for s-dependent bending radius (fringe field, wigglers, interference between consecutive dipoles)

1.3 Allow for resistive wall (not discussed in this talk and to be benchmarked)

2. Achievements

2.1 Limitations in all three codes (GS, KO, DZ) improved after careful benchmark work

2.2 Narrow-band impedances (spikes) due to CSR of wigglers were observed which are unexpected according to traditional theories

2.3 Interference between consecutive dipoles can be significant and leads to narrow-band CSR impedances (with perfect wall)

2.4 CSR calculation for SuperKEKB project

3. Challenges

3.1 Computing time is not quite acceptable at high freq. or very long components which require refinements in meshes or huge integration steps
 3.2 "Wiggling pipe" is not good approximation

3.3 Treating pipe with arbitrary cross section is unavailable