

Numerical simulations of CSR impedance

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and

Acknowledgements: K. Ohmi, T. Agoh, Y. Cai, K. Yokoya, M. Kikuchi, K. Shibata, H. Ikeda

CSR mini-workshop, KEK, Nov. 08, 2010

Outline

- 1. Introduction**
- 2. Algorithms**
- 3. Benchmark results**
 - 3.1 Single dipole
 - 3.2 Wiggler/undulator
- 4. CSR in wigglers**
 - 4.1 KEKB LER
 - 4.2 SuperKEKB LER
- 5. Fringe field and interference**
 - 5.1 KEKB LER
 - 5.2 SuperKEKB DR
- 6. Summary**

Introduction

Motivations:

1. To find out the unknown source of longitudinal impedance which drive the microwave instability (MWI) in the KEKB LER
2. To work out a reliable impedance model for SuperKEKB DR
3. CSR in wigglers, with interference, or with resistive wall

Existing publications on numerical calculations of CSR impedance:

1. T. Agoh and K. Yokoya, PRST-AB 7, 054403 (2004) and T. Agoh, PhD. Thesis (2004)
2. K. Oide, Presentation at KEKB ARC 2009 and PAC09
3. G. Stupakov and I. Kotelnikov, PRST-AB 12, 104401 (2009)

Algorithms - Fundamental equations

Parabolic equation in curvilinear coordinate system:

$$\frac{\partial \vec{E}_{\perp}}{\partial s} = \frac{i}{2k} (\nabla_{\perp}^2 \vec{E}_{\perp} - \mu_0 c^2 \nabla_{\perp} \rho_0 + \frac{2k^2 x}{\rho(s)} \vec{E}_{\perp})$$

$\beta=1$

Field separation:

$$\vec{E}_{\perp} = \vec{E}_{\perp}^r + \vec{E}_{\perp}^b$$

$$\frac{\partial \vec{E}_{\perp}^r}{\partial s} = \frac{i}{2k} [\nabla_{\perp}^2 \vec{E}_{\perp}^r + \frac{2k^2 x}{\rho} (\vec{E}_{\perp}^r + \vec{E}_{\perp}^b)]$$

Beam field in free space (independent of s):

$$\begin{aligned} \frac{\partial^2 E_x^b}{\partial x^2} + \frac{\partial^2 E_x^b}{\partial y^2} &= \mu_0 c^2 \frac{\partial \rho_0}{\partial x} \\ \frac{\partial^2 E_y^b}{\partial x^2} + \frac{\partial^2 E_y^b}{\partial y^2} &= \mu_0 c^2 \frac{\partial \rho_0}{\partial y} \end{aligned}$$

Ref. T. Agoh and K. Yokoya, PRST-AB 7, 054403 (2004)

Algorithms - Beam field

Beam field in free space with finite beam sizes

Typical beam size: $\sigma_x=0.5\text{mm}$, $\sigma_y=0.01\text{mm}$ (bi-gaussian)

$$E_x(x, y) = \frac{\lambda(k)}{2\epsilon_0 \sqrt{2\pi(\sigma_x^2 - \sigma_y^2)}} \text{Im}[F(x, y)]$$

$$E_y(x, y) = \frac{\lambda(k)}{2\epsilon_0 \sqrt{2\pi(\sigma_x^2 - \sigma_y^2)}} \text{Re}[F(x, y)]$$

$$F(x, y) = w\left(\frac{x + iy}{\sqrt{2(\sigma_x^2 - \sigma_y^2)}}\right) - e^{-\frac{x^2}{2\sigma_x^2} - \frac{y^2}{2\sigma_y^2}} w\left(\frac{\frac{\sigma_y}{\sigma_x}x + i\frac{\sigma_x}{\sigma_y}y}{\sqrt{2(\sigma_x^2 - \sigma_y^2)}}\right)$$

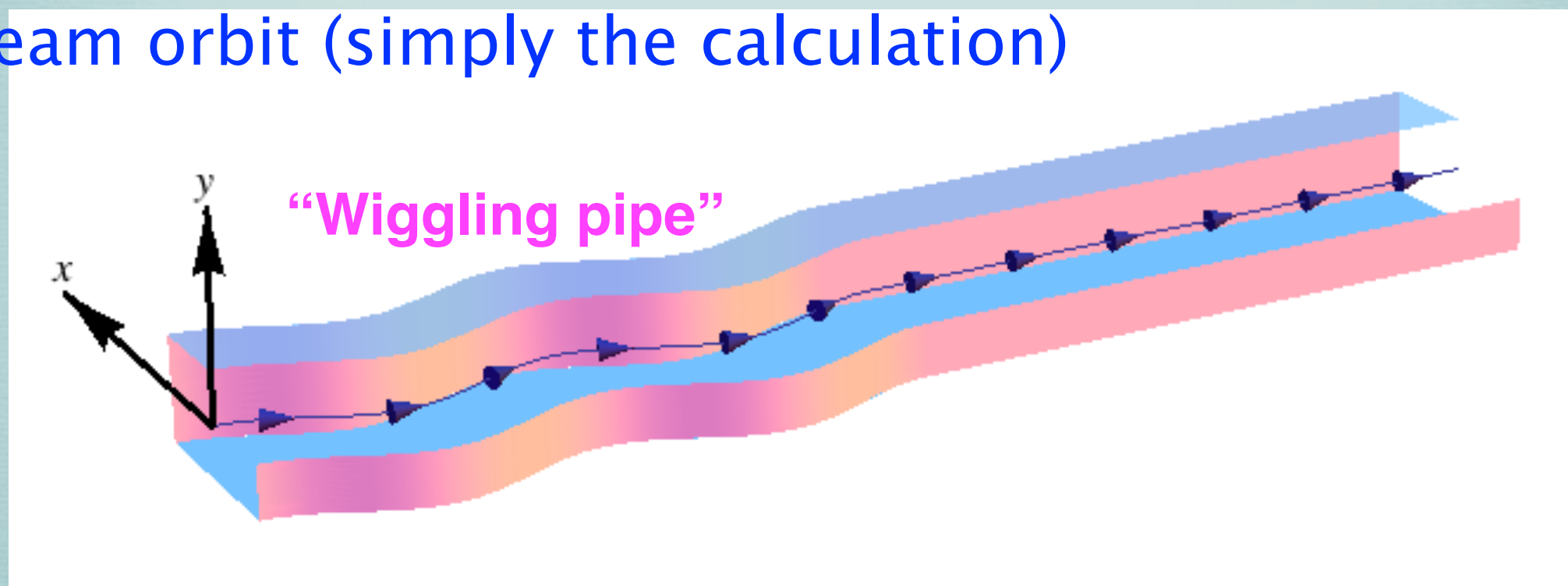
$$w(z) = e^{-z^2} \left(1 + \frac{2i}{\sqrt{\pi}} \int_0^z e^{t^2} dt\right)$$

Ref. T. Agoh, Ph.D. Thesis (2004)

Algorithms - Beam pipe

Model of the beam pipe:

1. The bending radius can be arbitrarily s -dependent, which allows for treating fringe field, wigglers or a series of dipole magnets
2. Uniform rectangular cross section along the beam orbit (simplify the calculation)



Field integration along s :

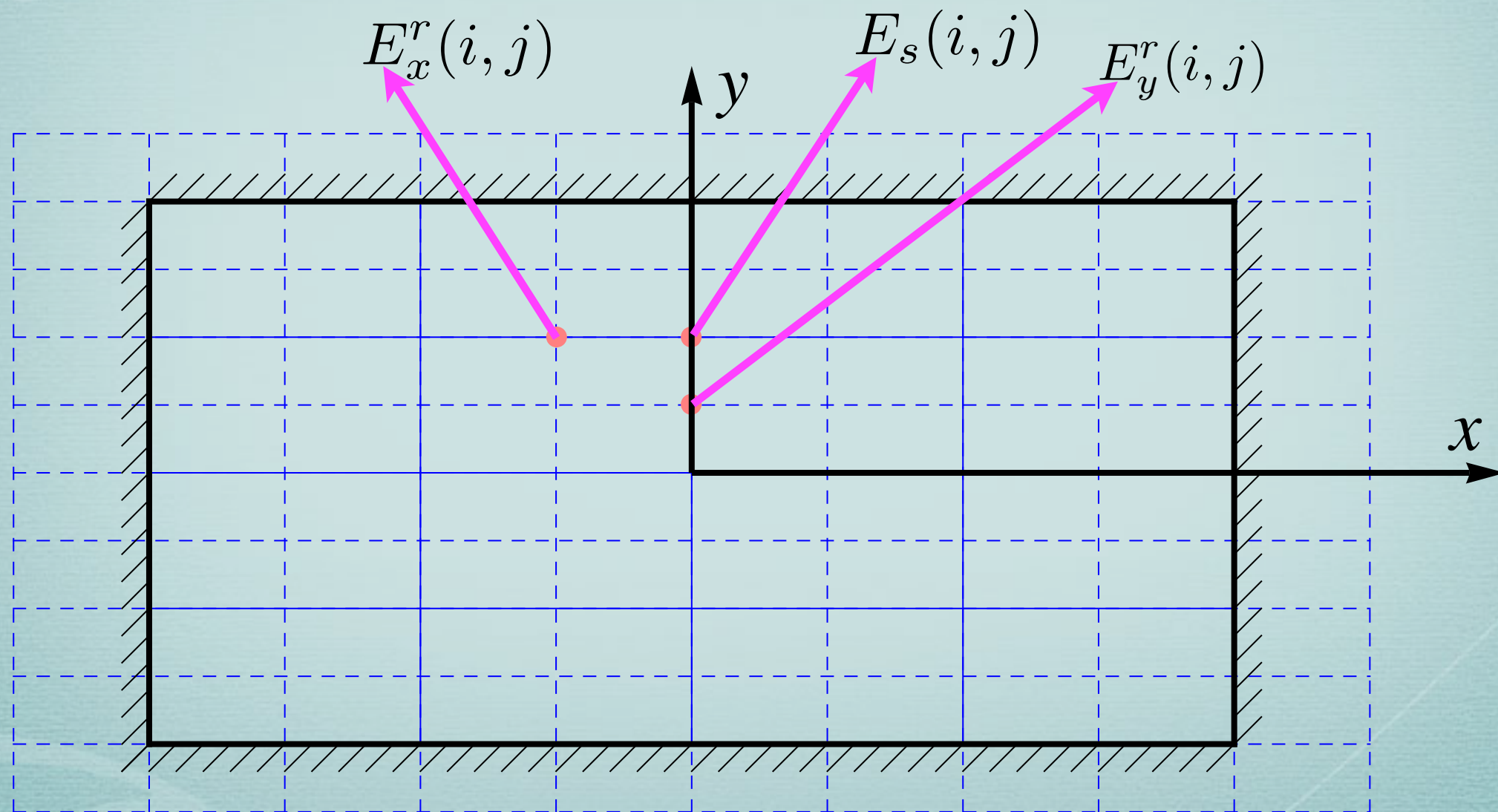
1. Toroidal part: Numerical integration
2. Straight pipe: mode expansion

Ref. T. Agoh, Ph.D. Thesis (2004)
G. Stupakov and I. Kotelnikov, PRST-
AB 12, 104401 (2009)

Algorithms - Mesh

Finite-difference discretization:

1. Staggered grid: Central difference
2. Ghost point: Boundary conditions with perfect wall

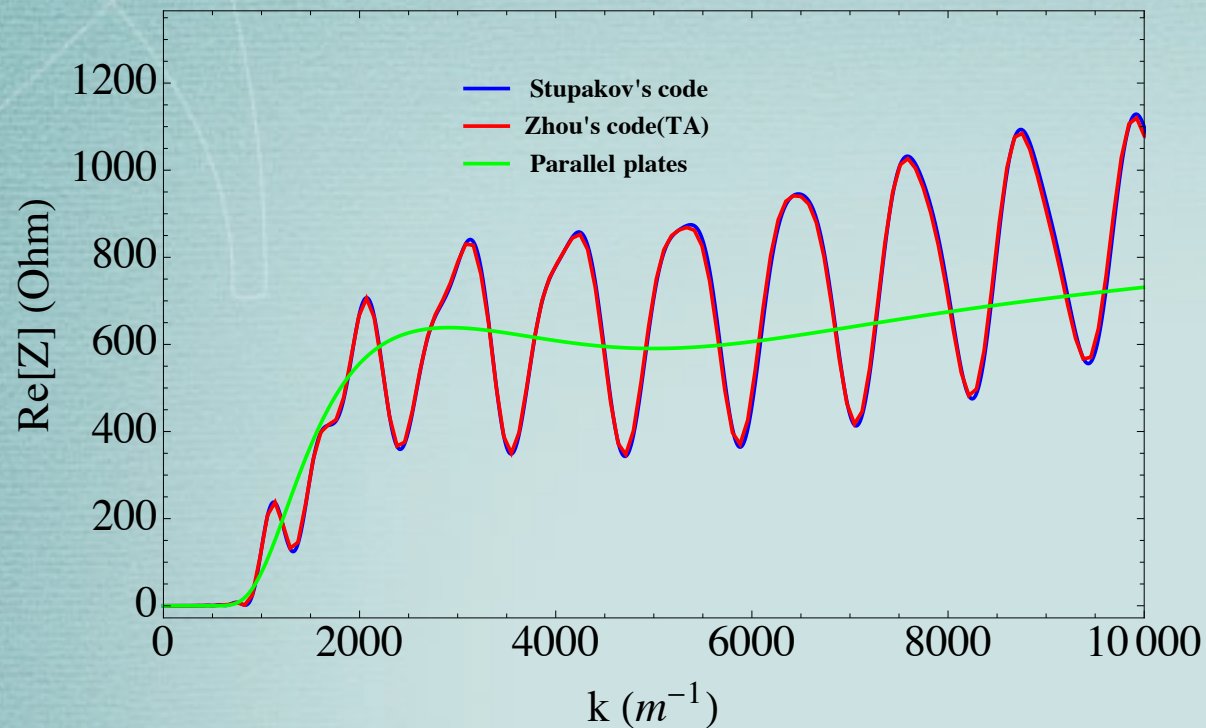


Ref. T. Agoh, Ph.D. Thesis (2004)

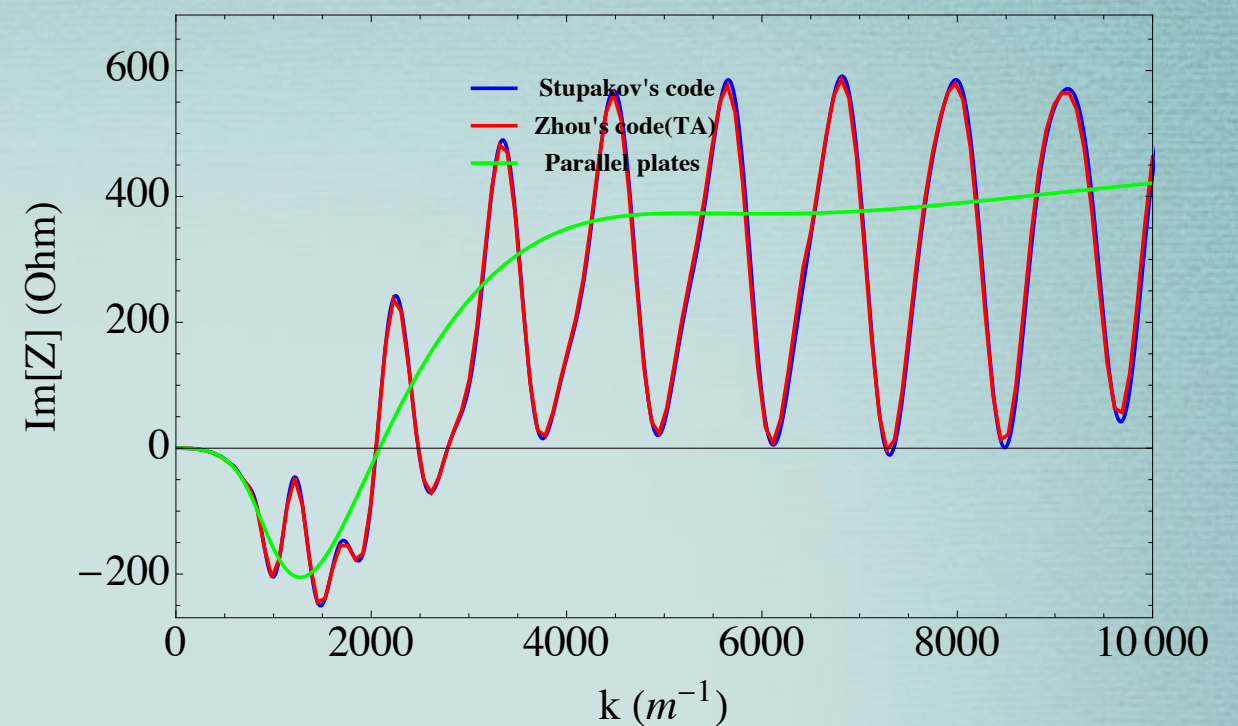
Benchmark results - Single dipole

Collaborate with K. Marit

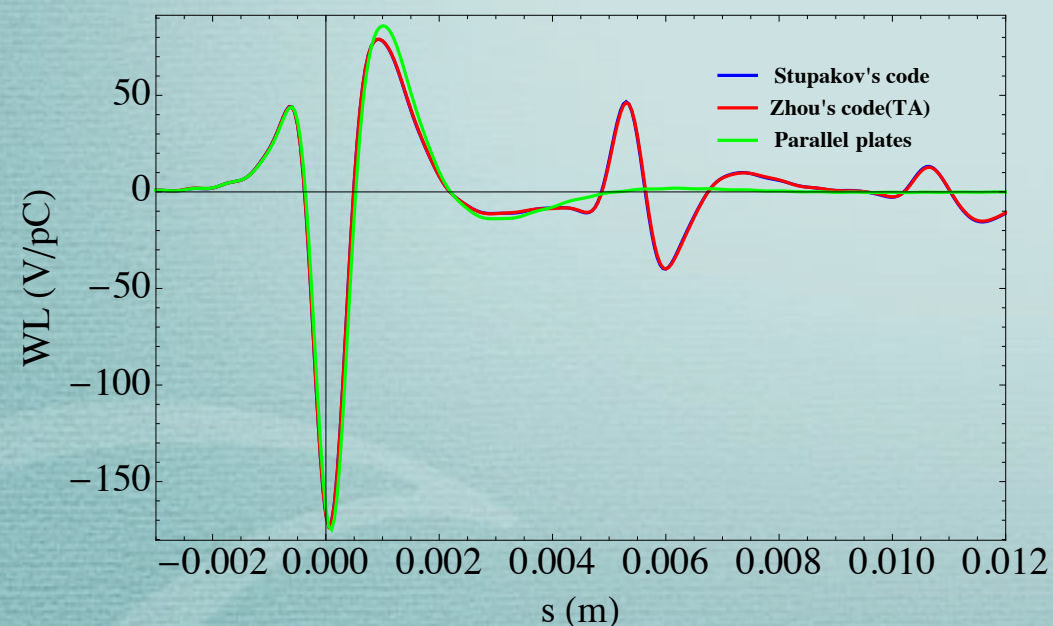
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



Fluctuation in impedance is due to reflections of side walls (see Oide's talk)

ANKA

$w/h=70/32\text{mm}$

$L_{\text{bend}}=2.183\text{m}$

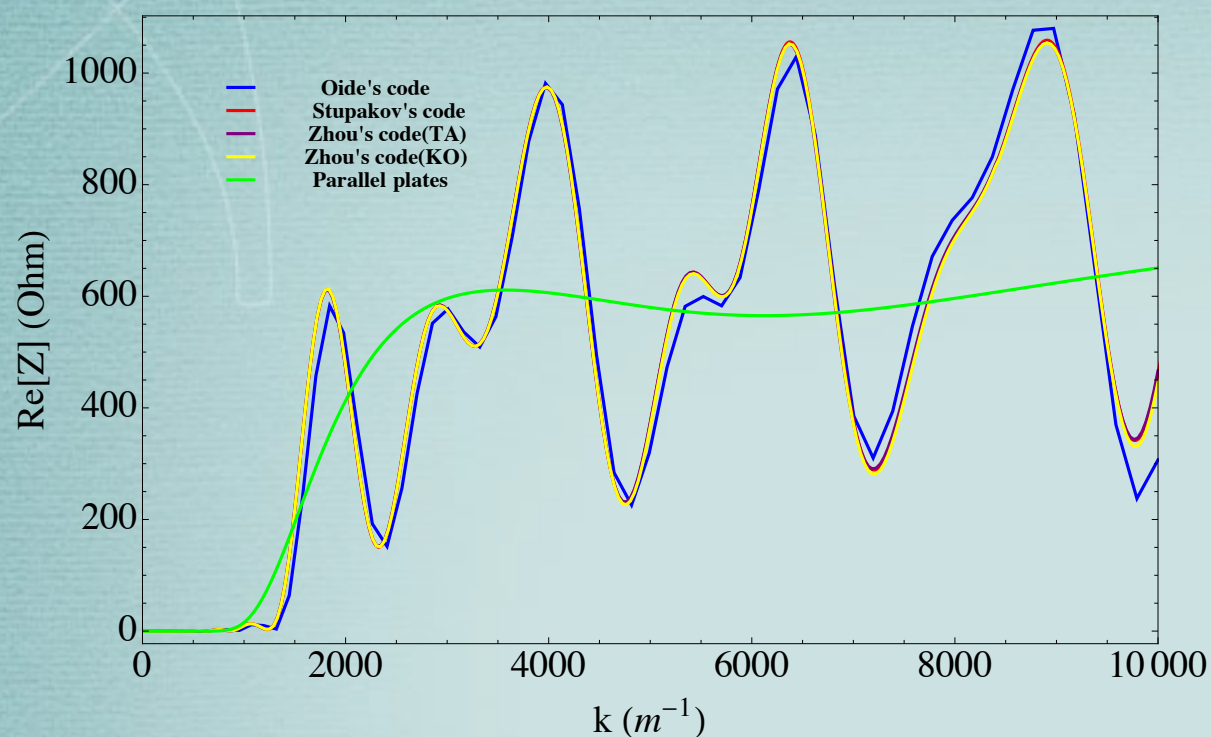
$\rho=5.559\text{m}$

$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

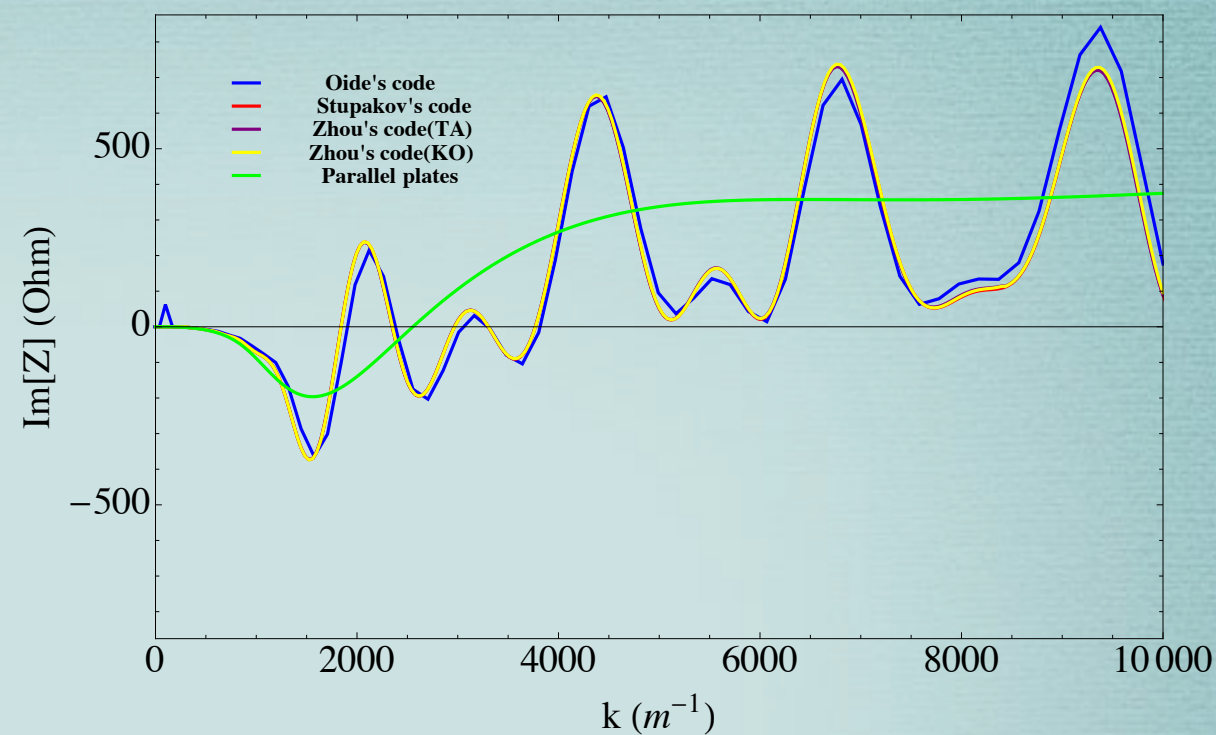
$X_{\text{offset}}=0\text{mm}$

Benchmark results - Single dipole

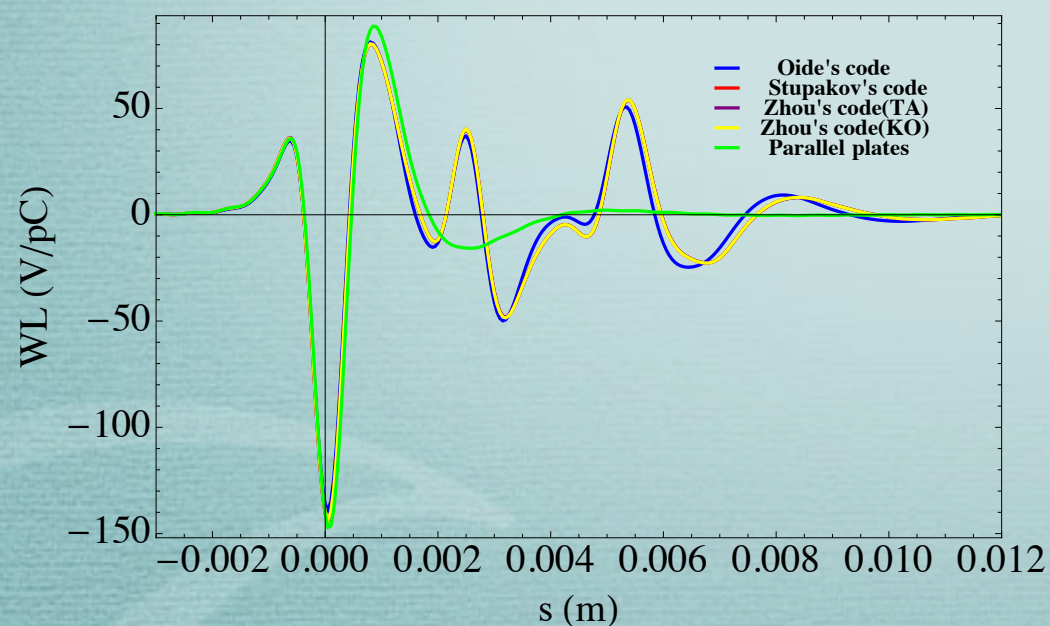
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



TA: Agoh's algorithm
KO: Oide's algorithm

$w/h=60/40\text{mm}$

$L_{\text{bend}}=4\text{m}$

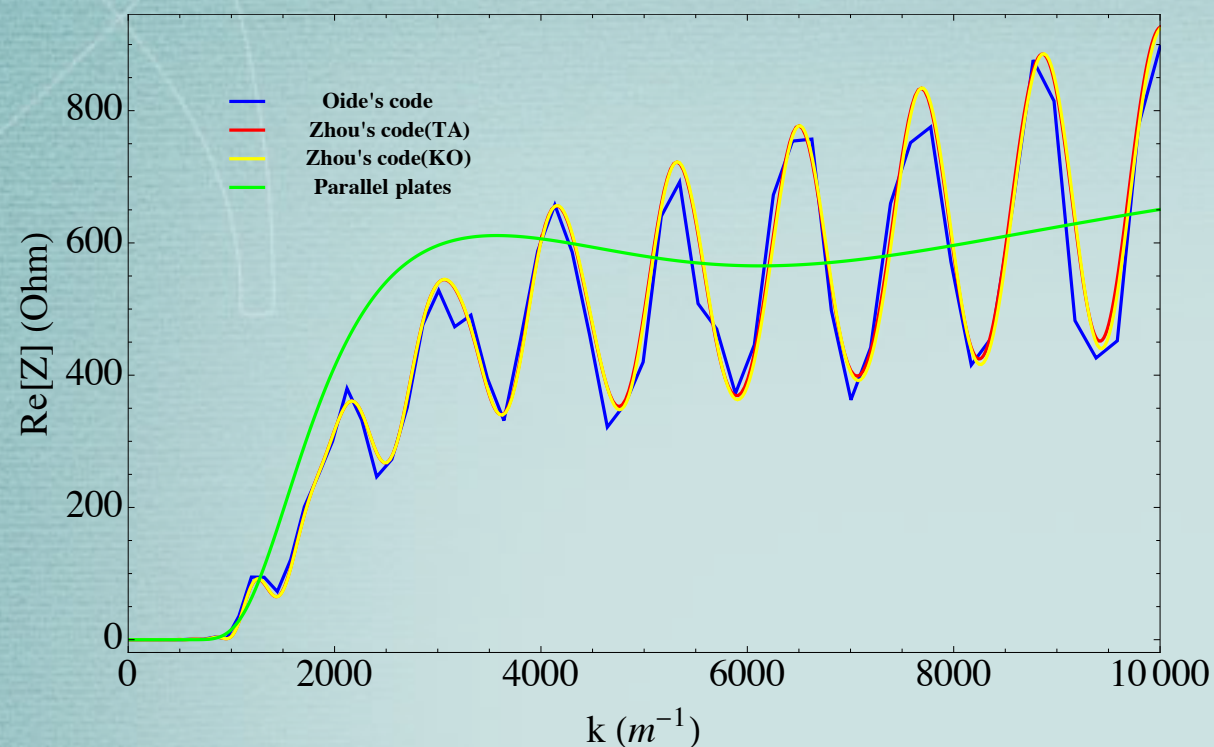
$\rho=16.3\text{m}$

$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

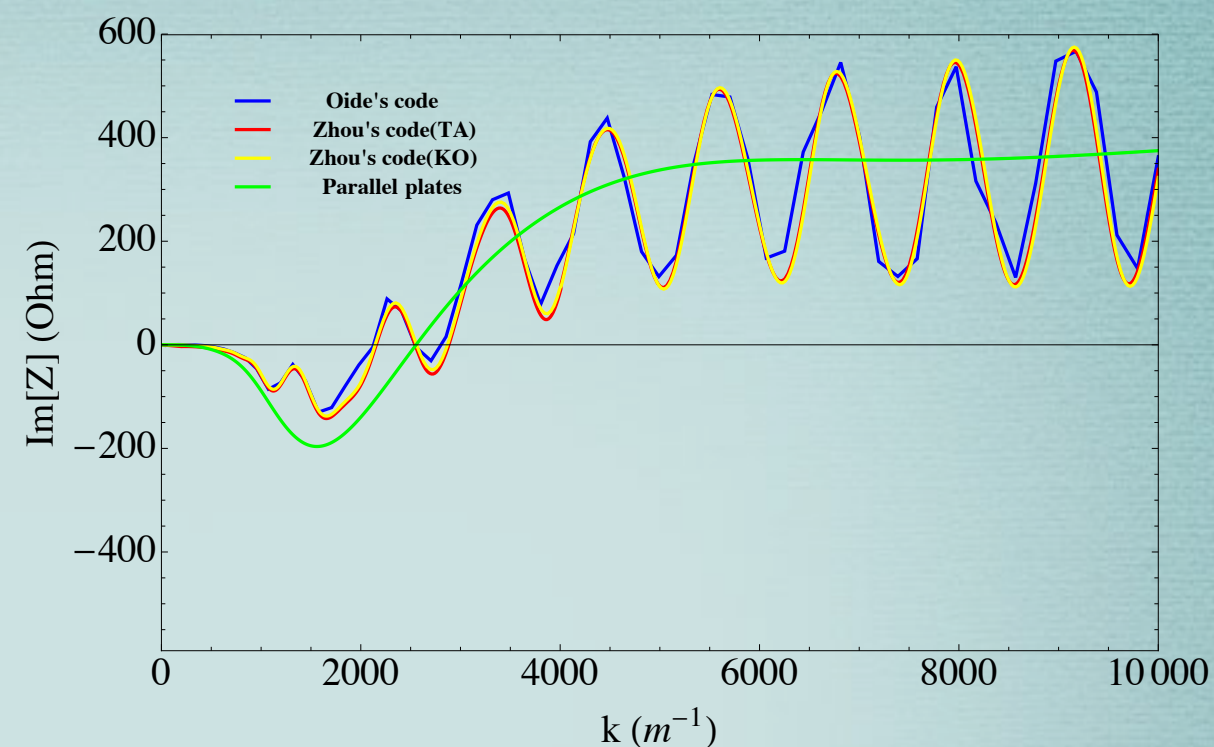
$X_{\text{offset}}=0\text{mm}$

Benchmark results - Single dipole

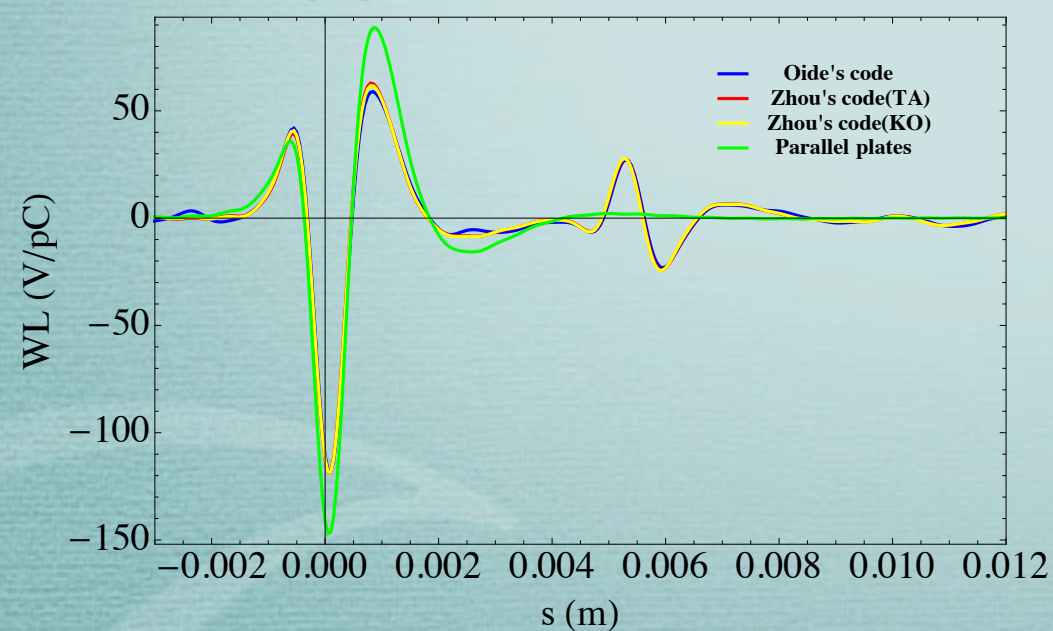
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



TA: Agoh's algorithm
KO: Oide's algorithm

$w/h=60/40\text{mm}$

$L_{\text{bend}}=4\text{m}$

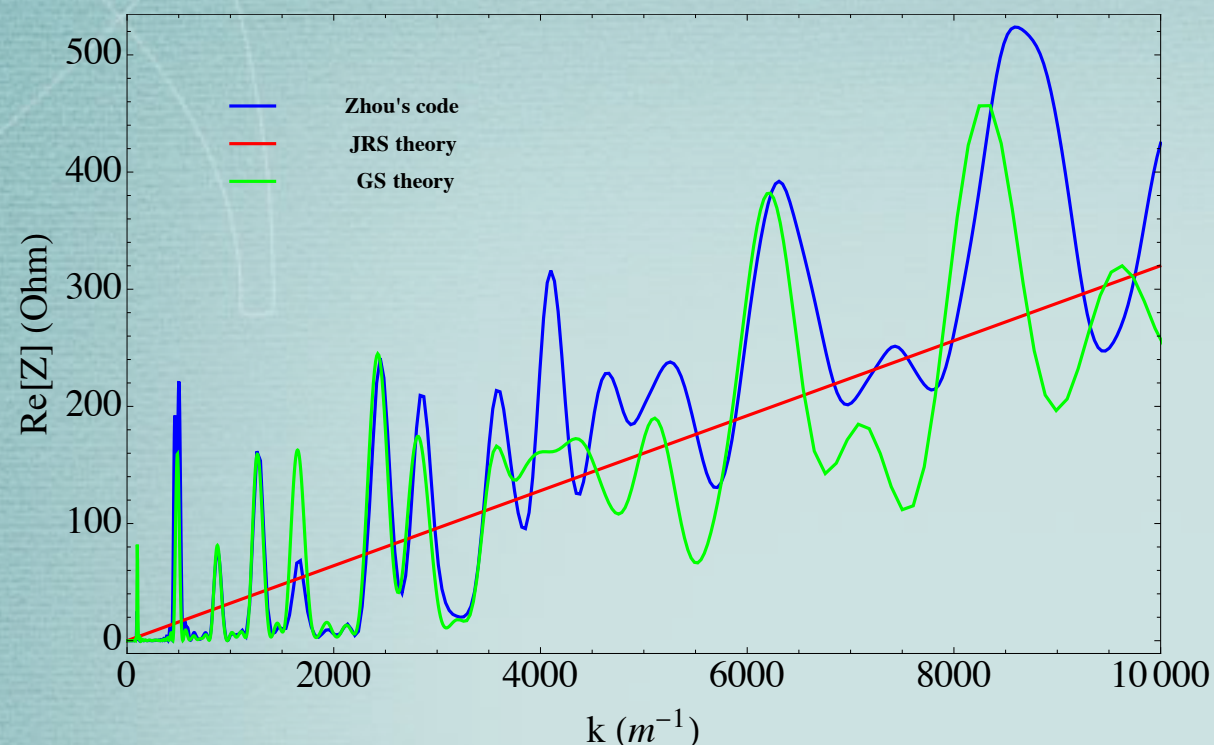
$\rho=16.3\text{m}$

$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

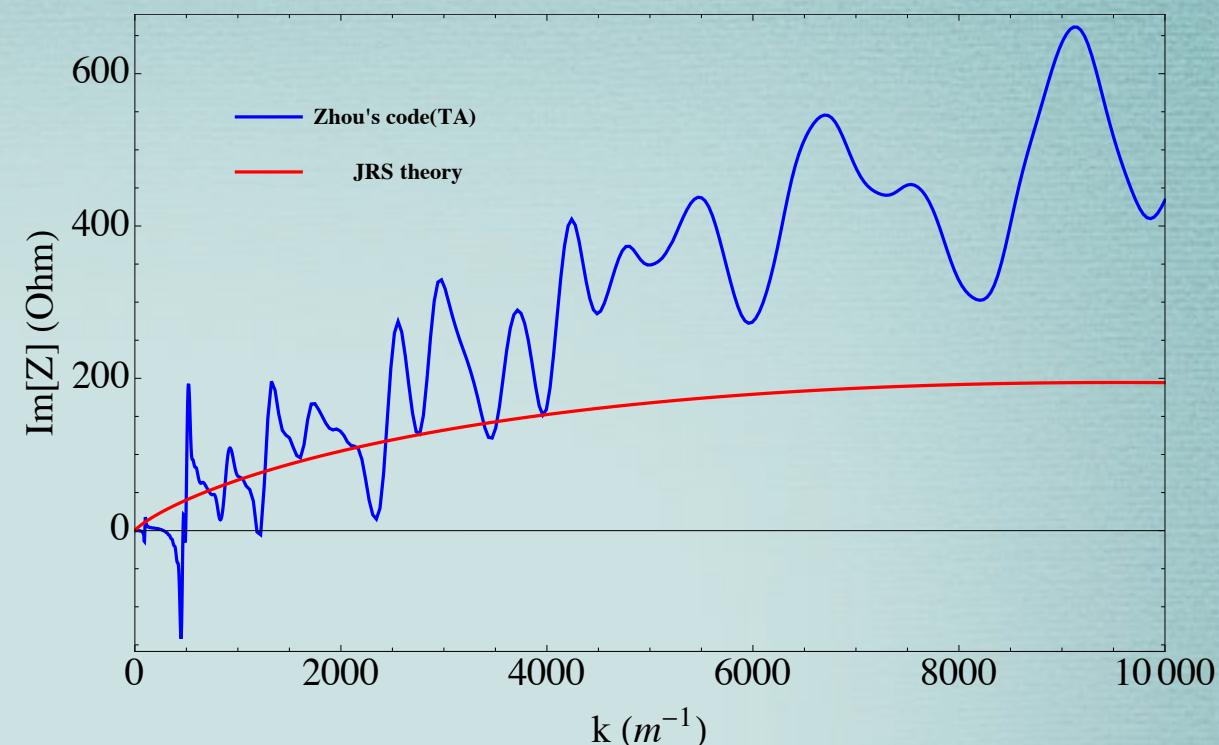
$X_{\text{offset}}=-20\text{mm}$ (To inner wall)

Benchmark results - Wiggler

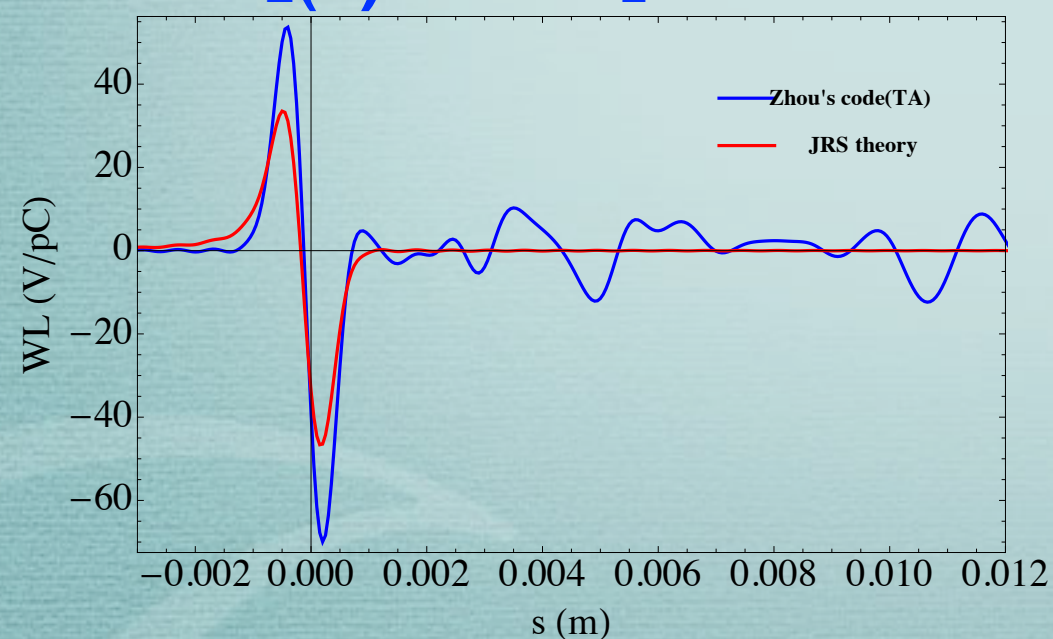
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



JRS: Wu-Stupakov-Raubenheimer theory
J. Wu et al., PRST-AB 6, 040701 (2003)

$N_{\text{period}}=10$

$w/h=94/94\text{mm}$

$\lambda_w=1.088\text{m}$

$\rho=15.483\text{m}$

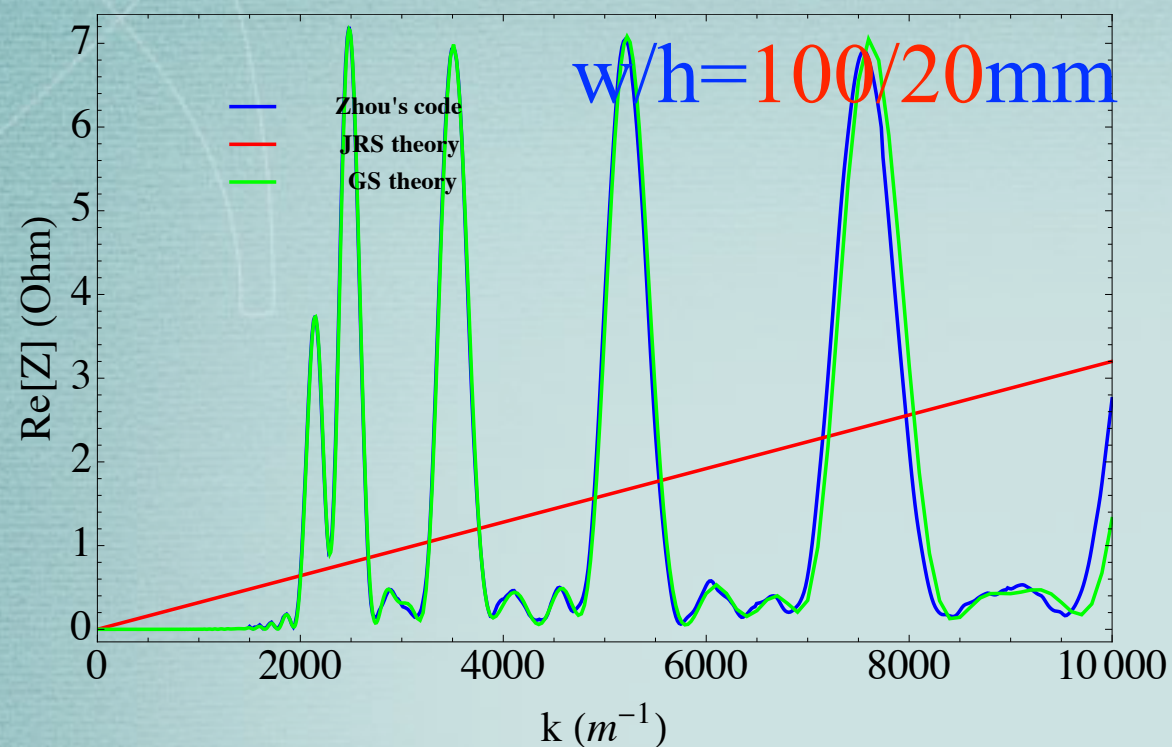
$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

$X_{\text{offset}}=0\text{mm}$

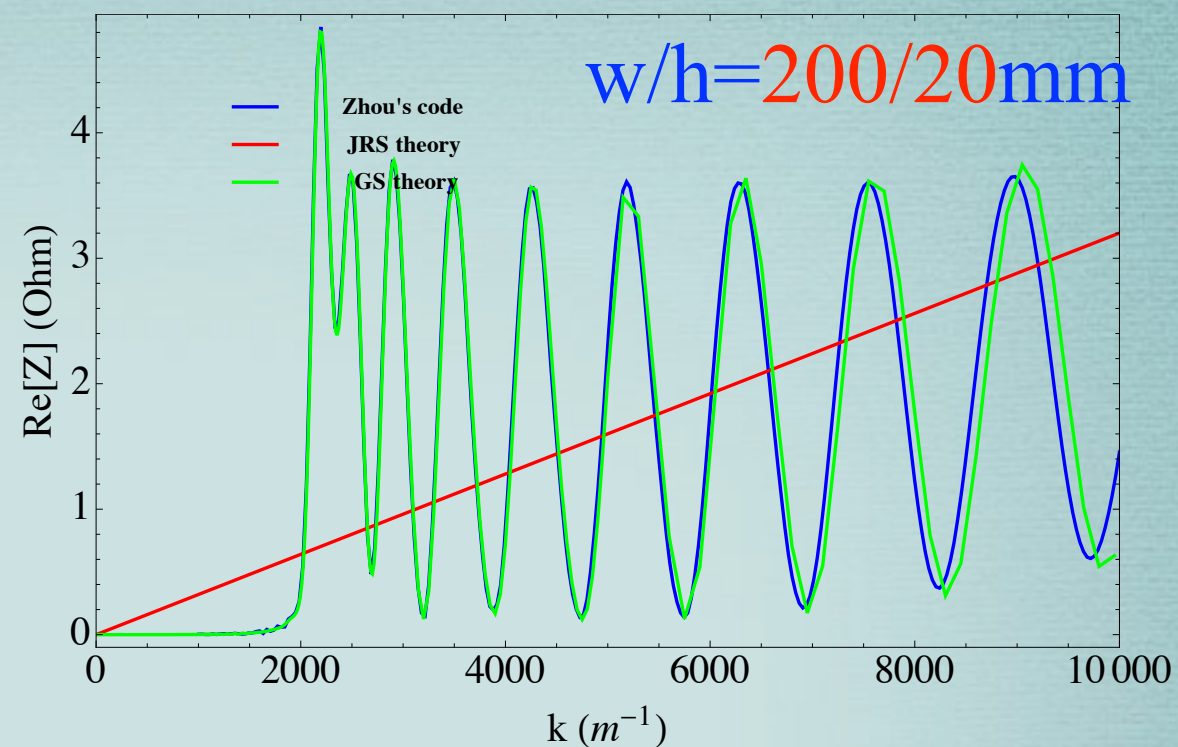
**KEKB-LER
type**

Benchmark results - Wiggler

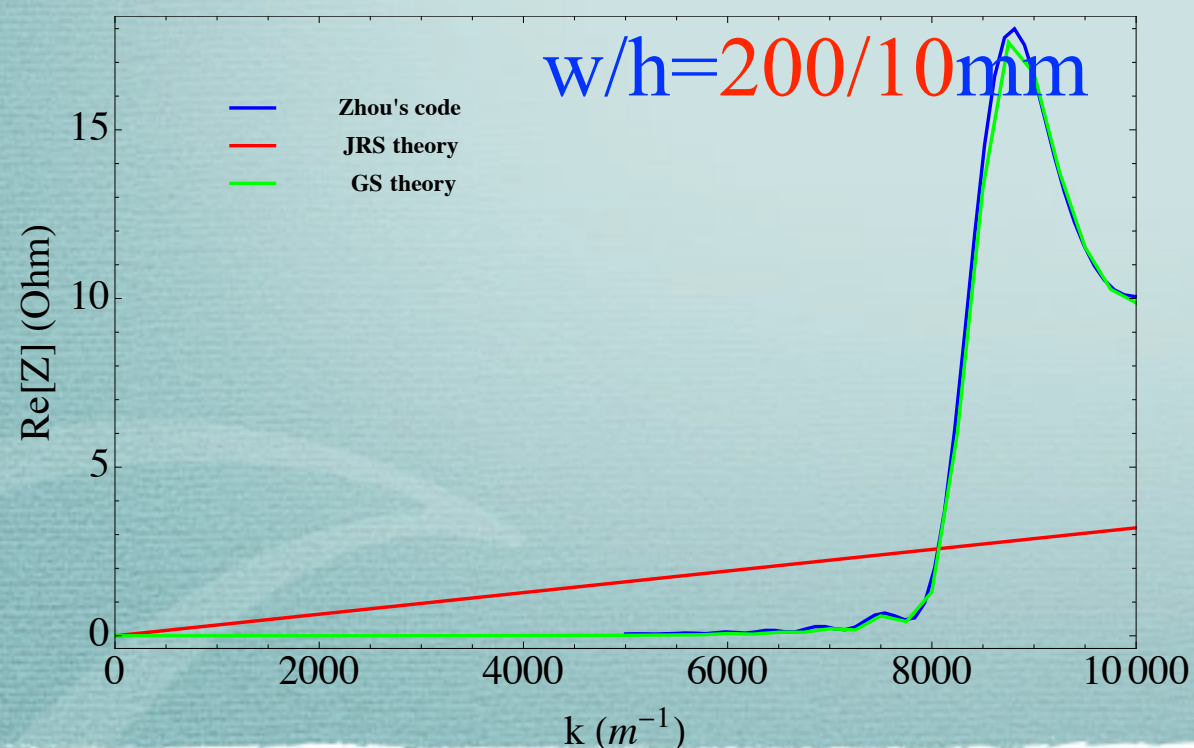
Re. $Z_L(k)$



Re. $Z_L(k)$



Re. $Z_L(k)$



**Note: “Wiggling pipe”
is not good enough!**

$N_{\text{period}}=10$

$\lambda_w=1.088\text{m}$

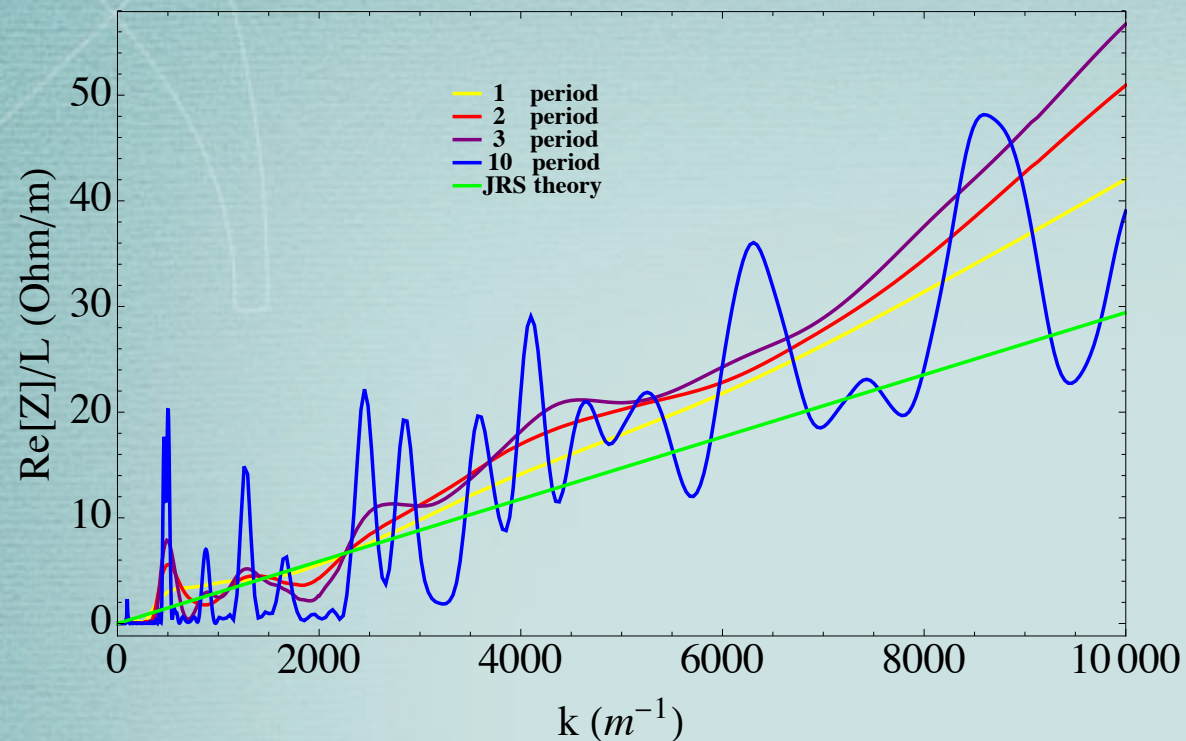
$\rho=154.83\text{m}$

$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

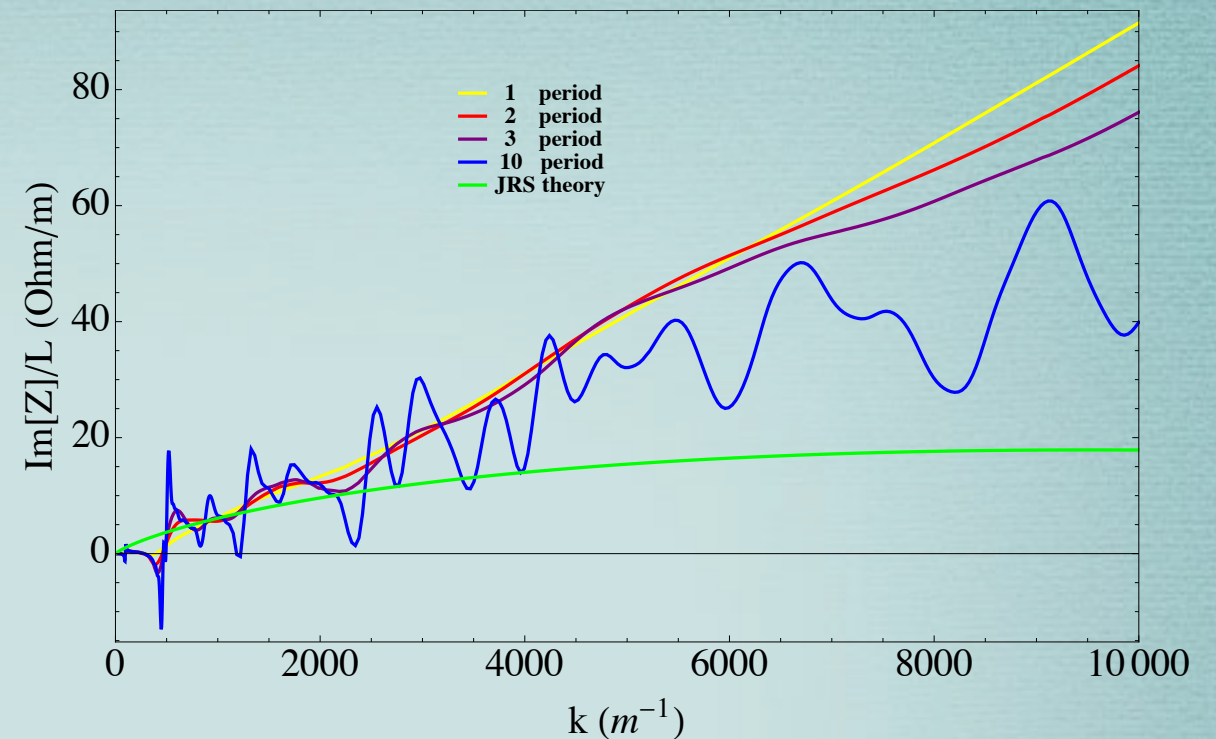
$X_{\text{offset}}=0\text{mm}$

CSR in wigglers - KEKB LER

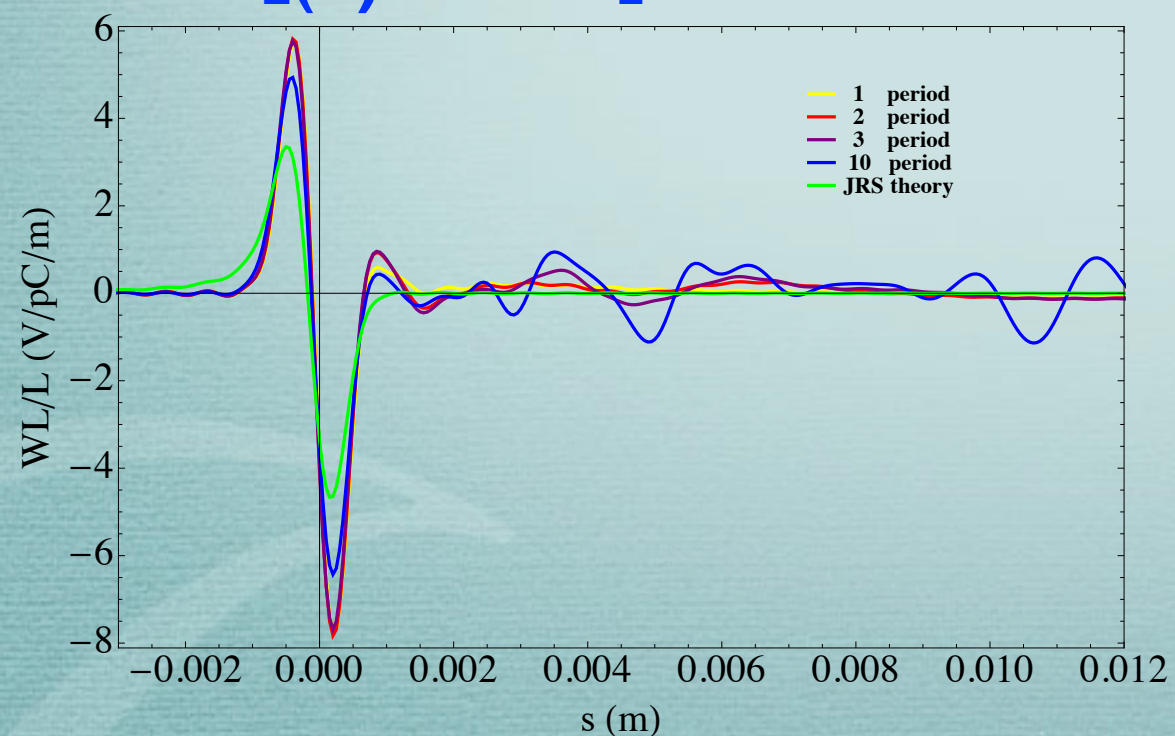
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



$N_{\text{period}}=1/2/3/10$

$w/h=94/94\text{mm}$

$\lambda_w=1.088\text{m}$

$\rho=15.483\text{m}$

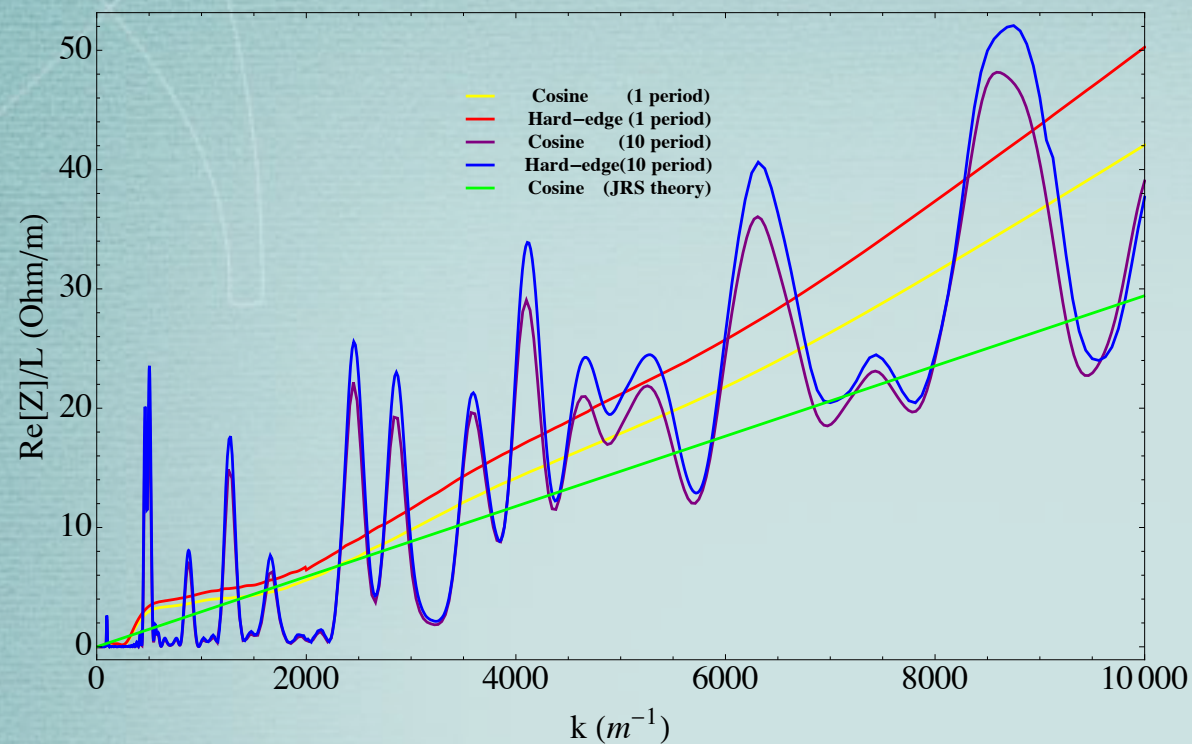
$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

$X_{\text{offset}}=0\text{mm}$

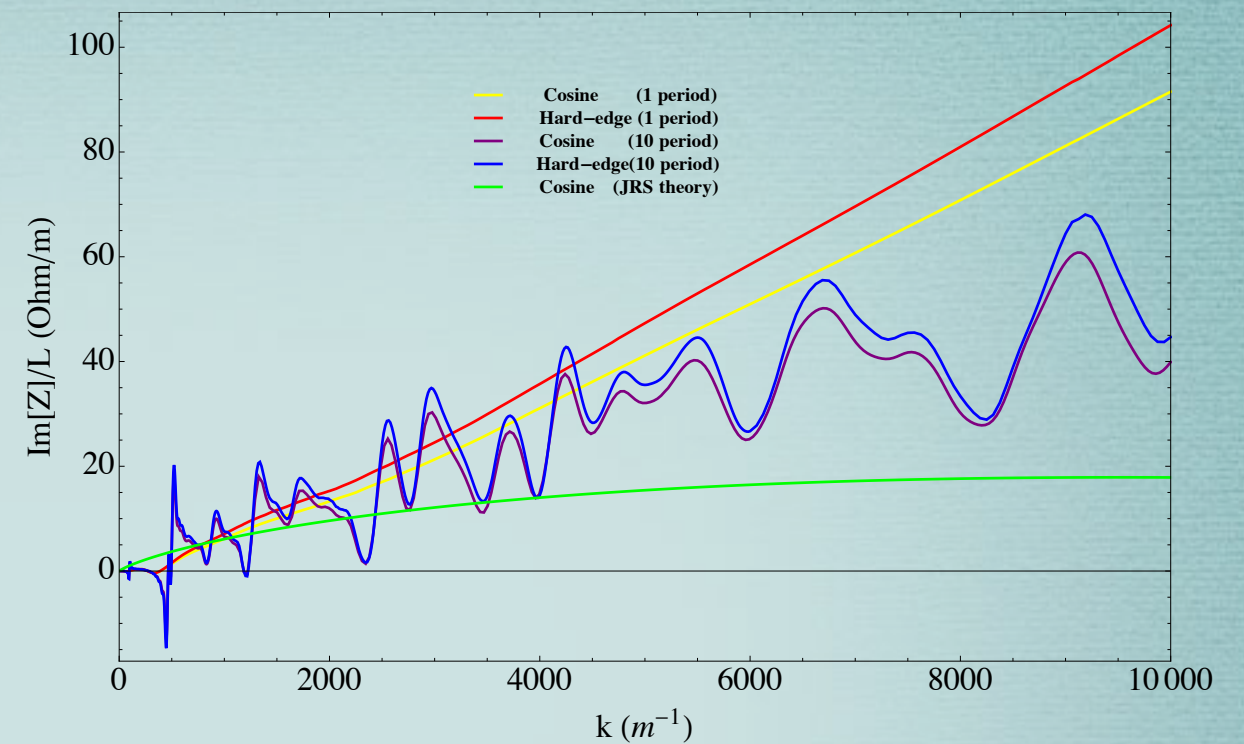
Field distribution: Cosine

CSR in wigglers - Hard-edge approximation

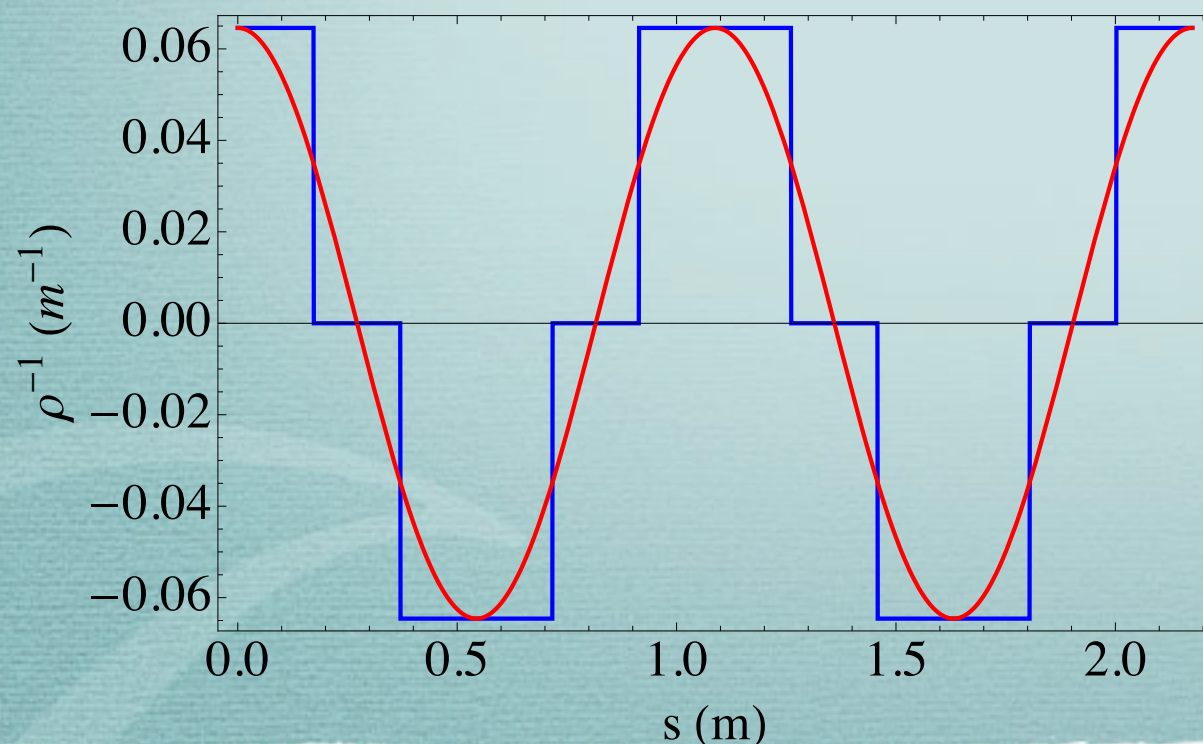
Re. $Z_L(k)$



Im. $Z_L(k)$



Field distribution



H.E. model looks to be good?

$N_{\text{period}}=1/10$

$w/h=94/94\text{mm}$

KEKB-LER

$\lambda_w=1.088\text{m}$

$\rho=15.483\text{m}$

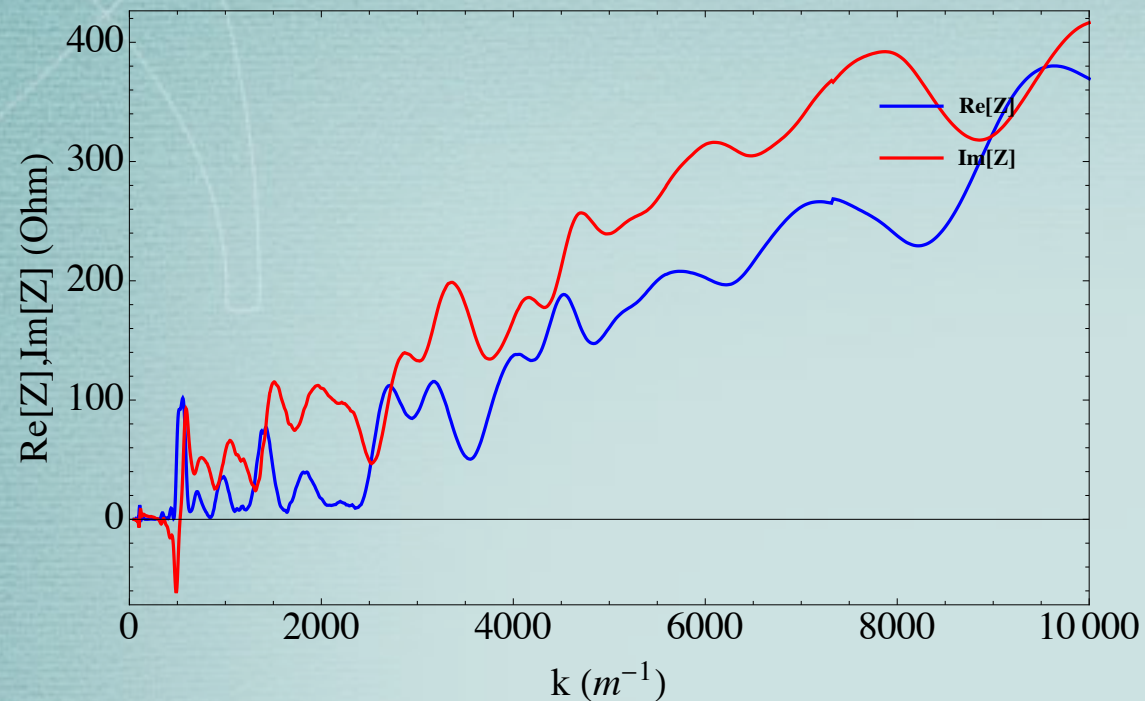
$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

$X_{\text{offset}}=0\text{mm}$ (To inner wall)

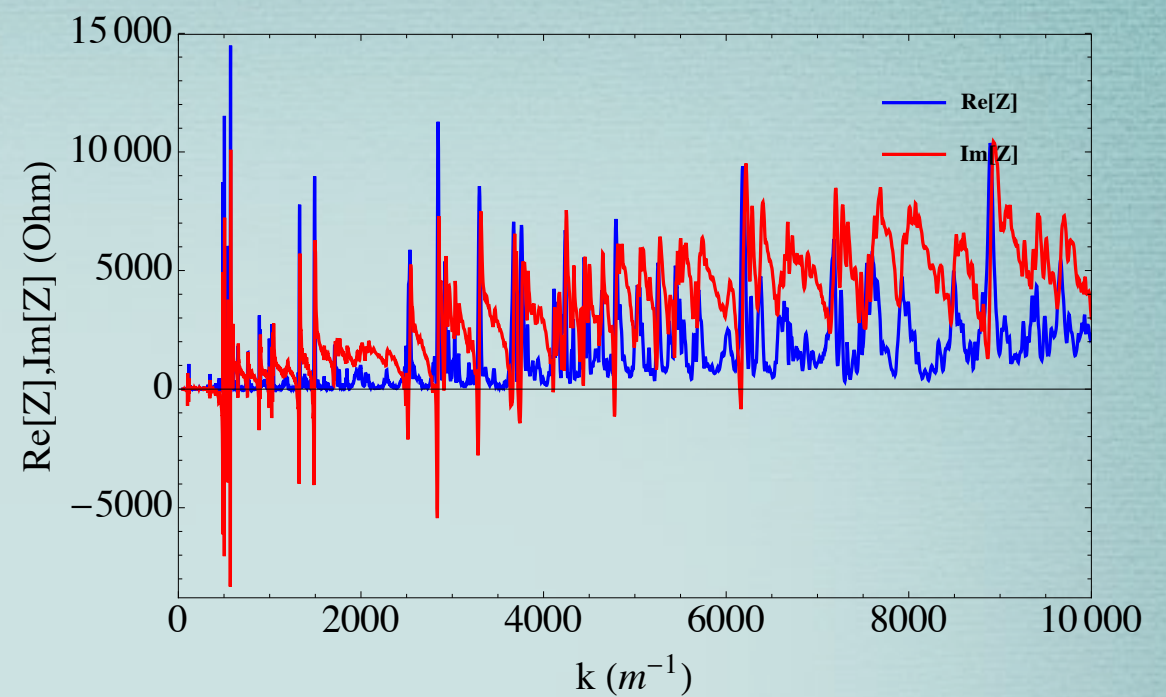
Field distribution: Cosine/H.E.

CSR in wigglers - SuperKEKB LER

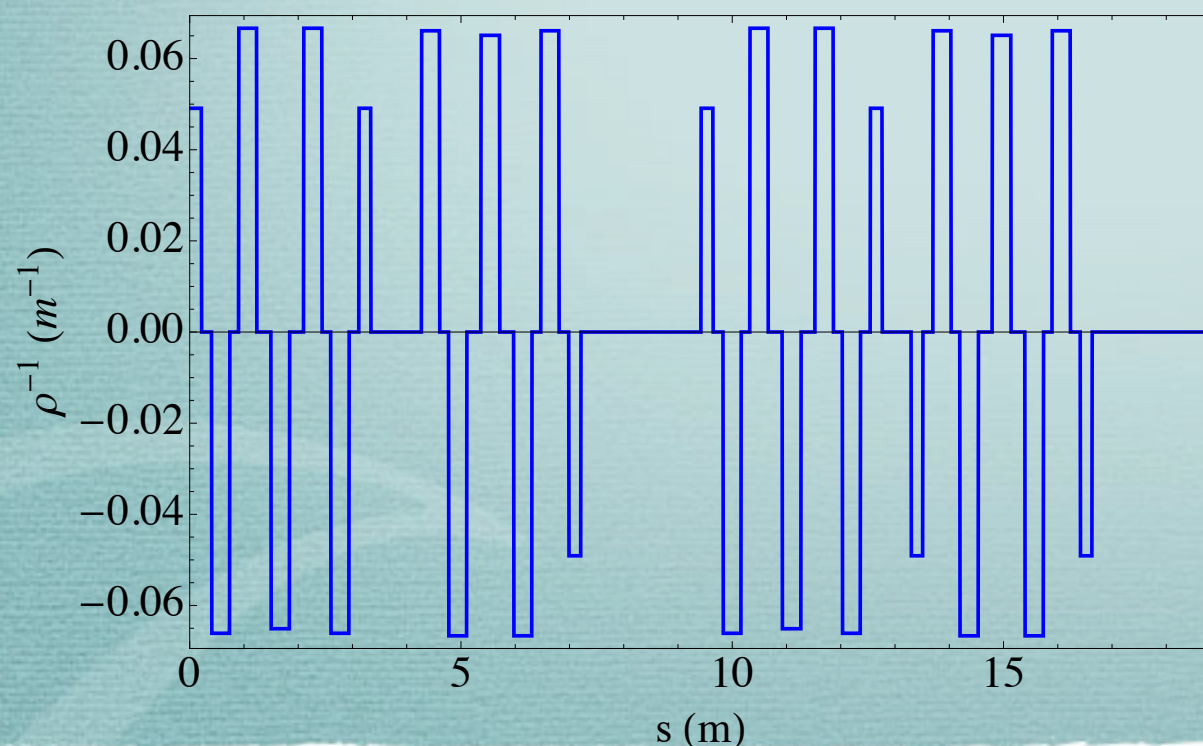
$Z_L(k)$,1 Super-period



$Z_L(k)$,15 Super-periods



Field distribution



$N_{\text{super-period}}=1/15$

$w/h=90/90\text{mm}$

$L_w=140\text{m}$

$\rho \approx 15\text{m}$

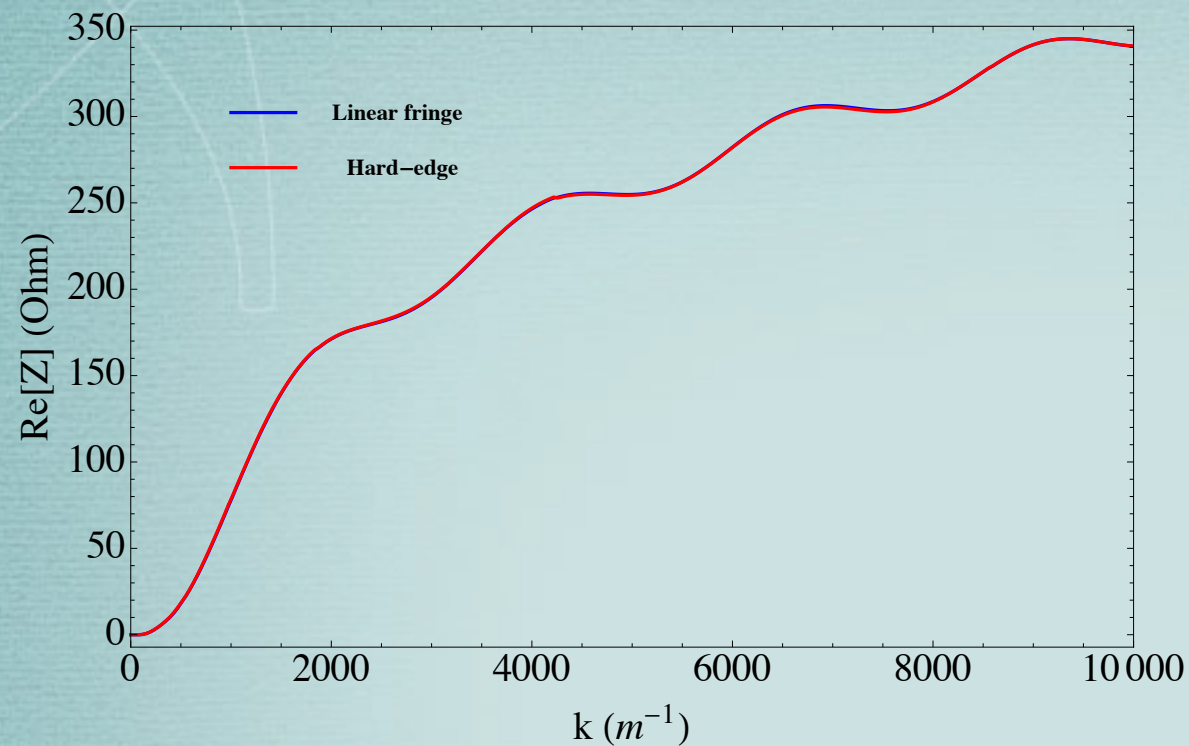
$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

$X_{\text{offset}}=0\text{mm}$

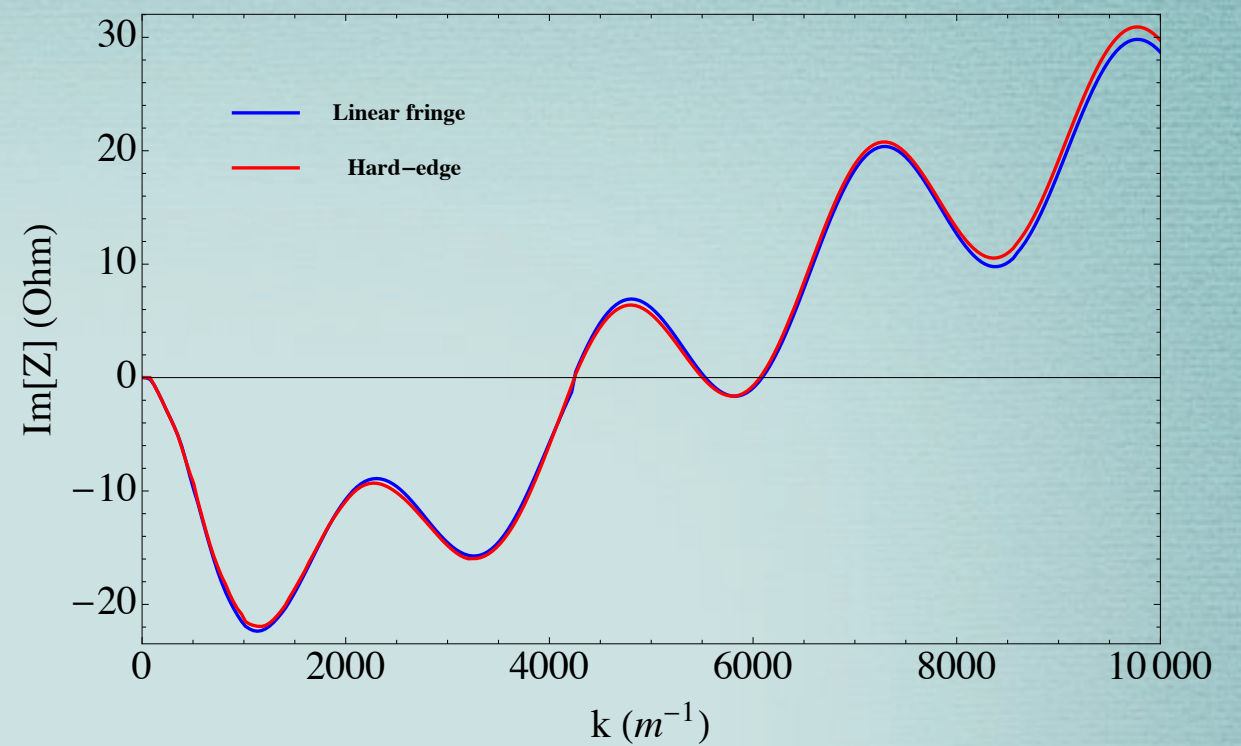
Field distribution: Hard-edge

Fringe field - KEKB LER

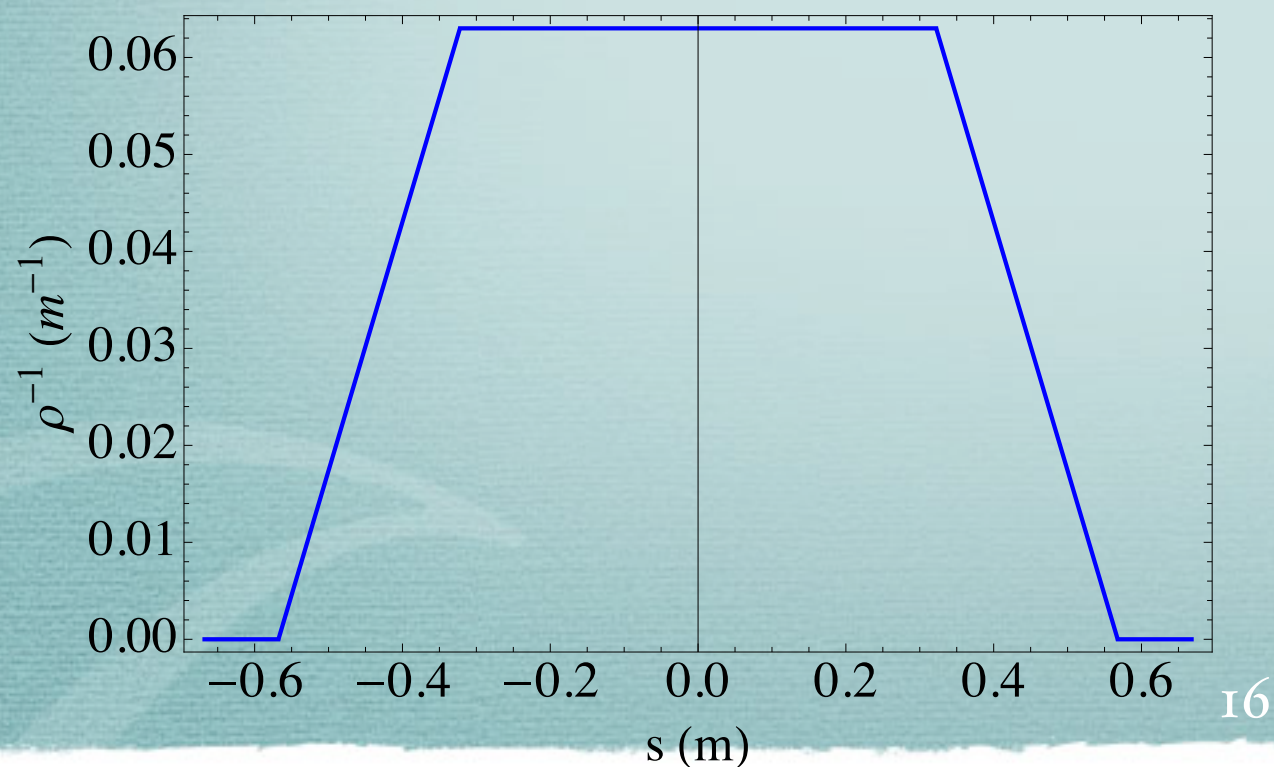
Re. $Z_L(k)$



Im. $Z_L(k)$



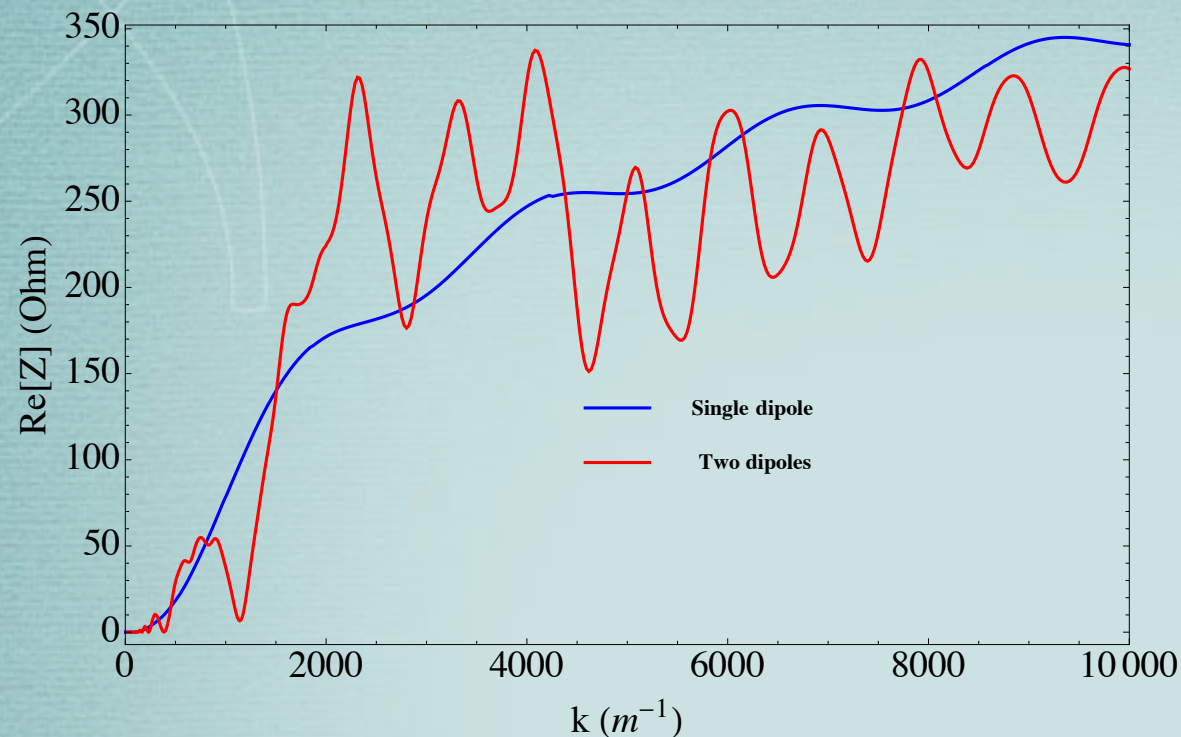
Field distribution



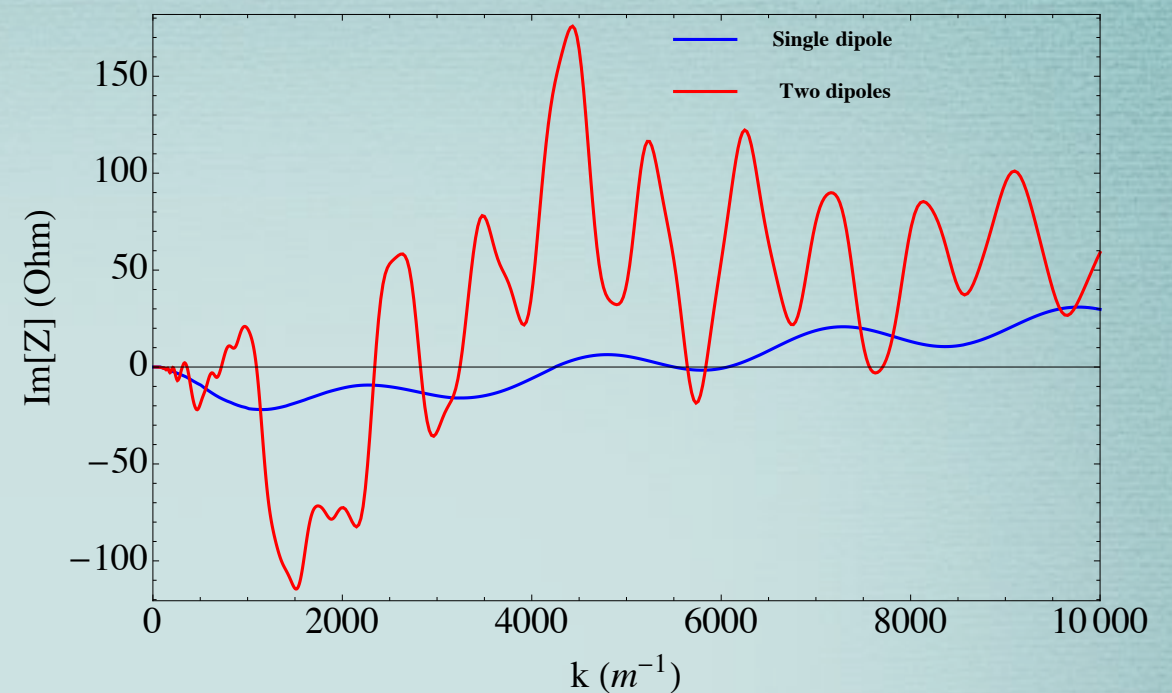
“Fringe effect” is negligible?

Interference - KEKB LER

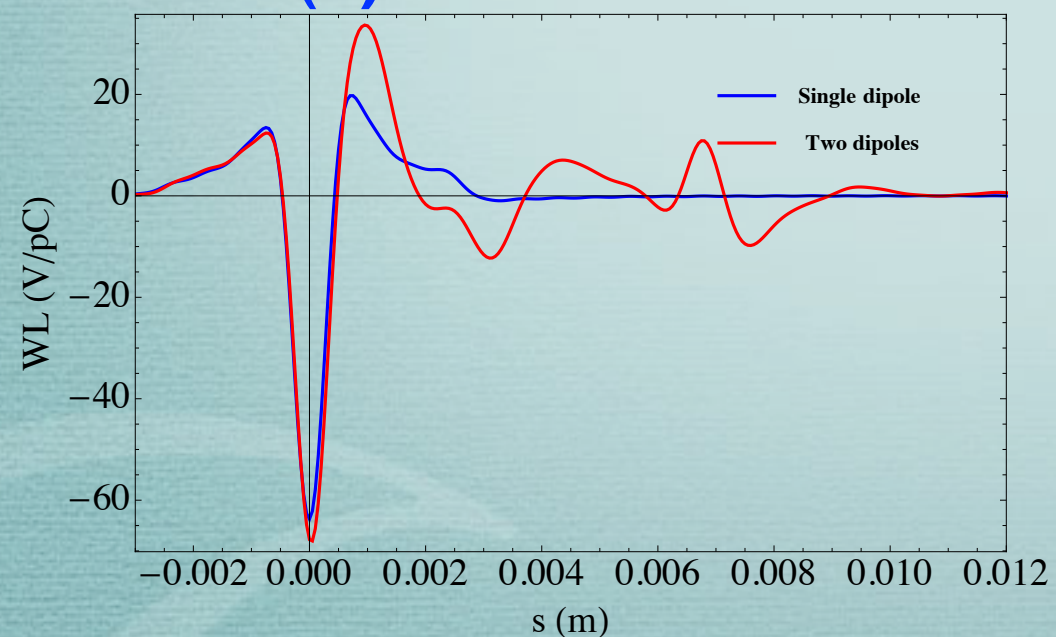
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



Two dipoles

$w/h=94/94\text{mm}$

$L_{\text{bend}}=0.89\text{m}$

$L_{\text{drift}}=5.65\text{m}$

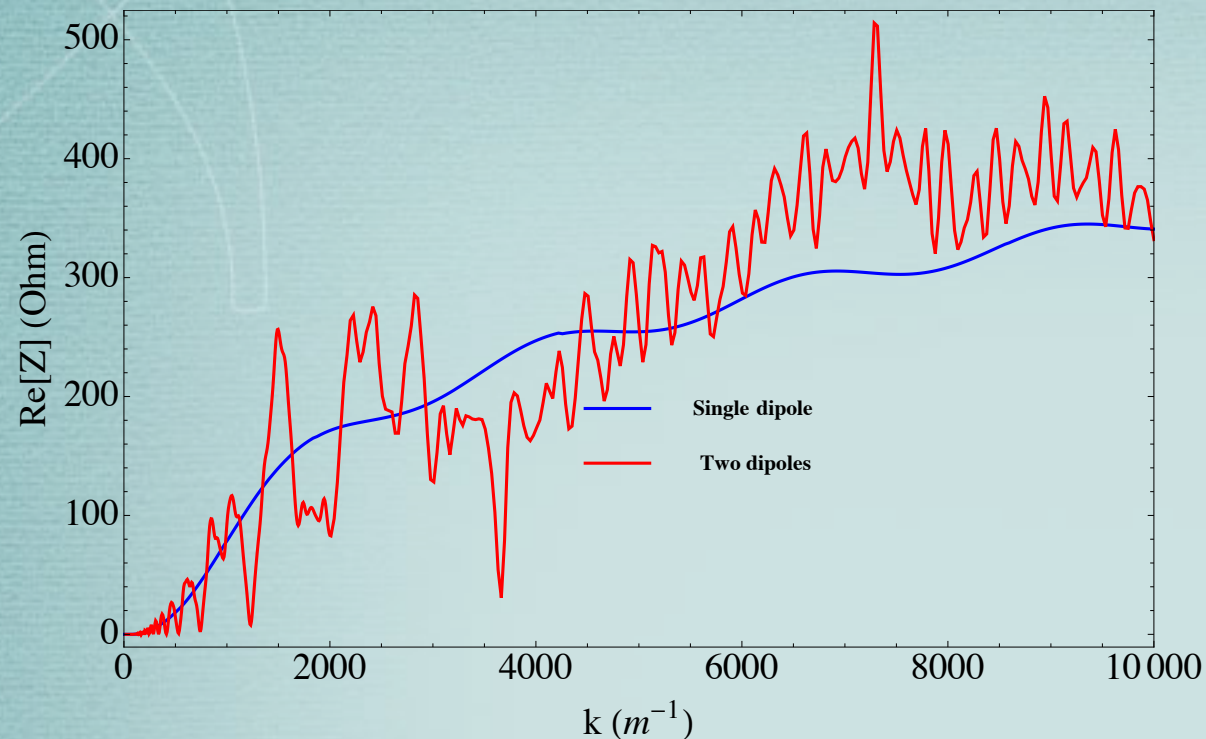
$\rho=15.872\text{m}$

$L_{\text{exit}}=\text{Infinity (pipe after exit)}$

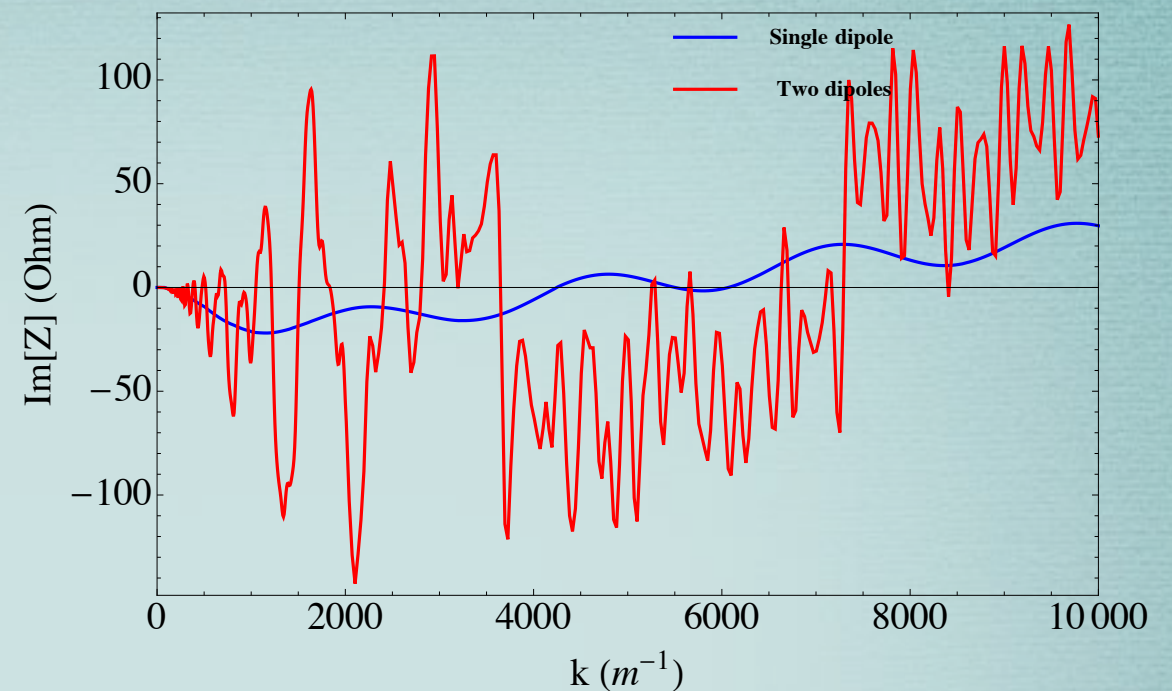
$X_{\text{offset}}=0\text{mm}$

Interference - KEKB LER

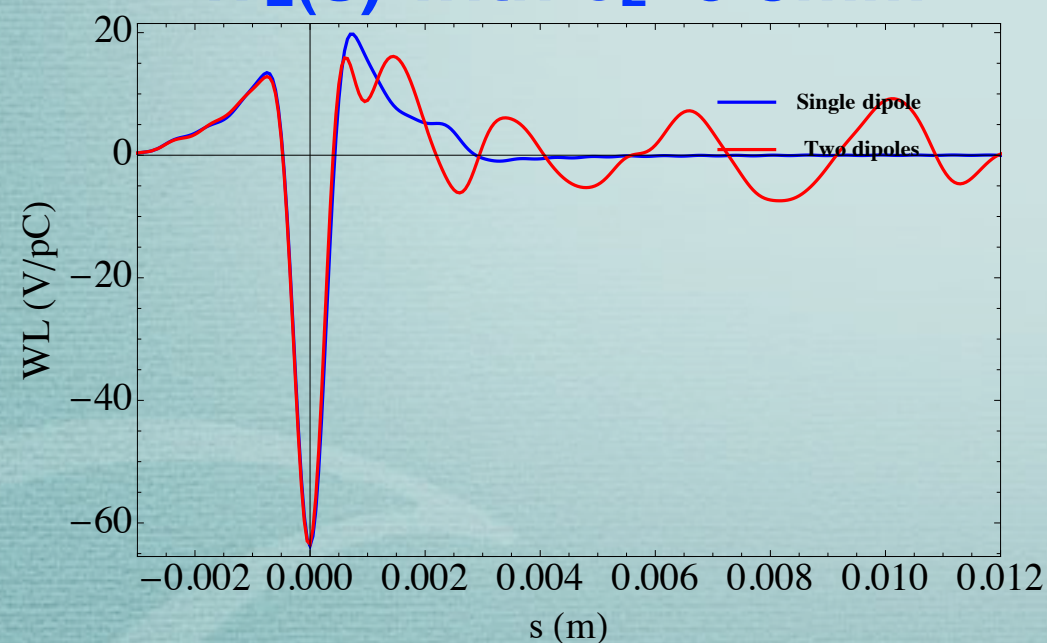
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



Two dipoles

$w/h=94/94\text{mm}$

$L_{\text{bend}}=0.89\text{m}$

$L_{\text{drift}}=20\text{m}$

$\rho=15.872\text{m}$

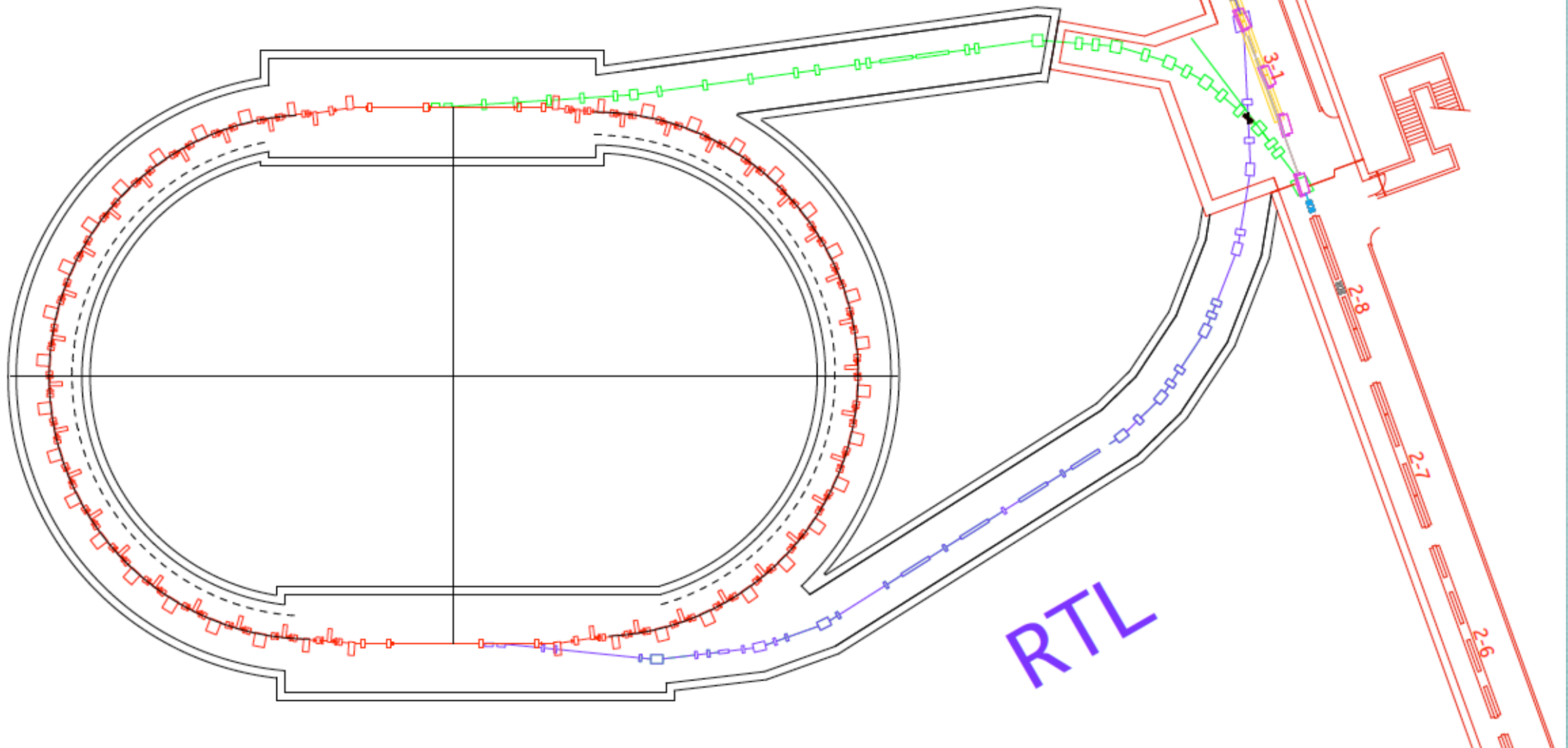
$L_{\text{exit}}=\text{Infinity (pipe after exit)}$

$X_{\text{offset}}=0\text{mm}$

Interference - SuperKEKB DR

Layout of SuperKEKB DR

LTR



RTL

M. Kikuchi

Interference - SuperKEKB DR

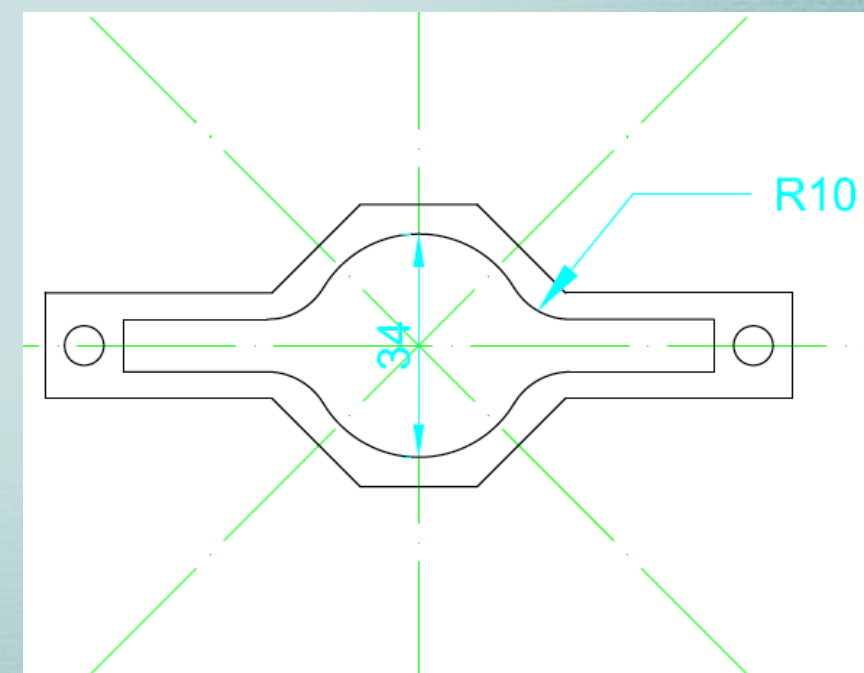
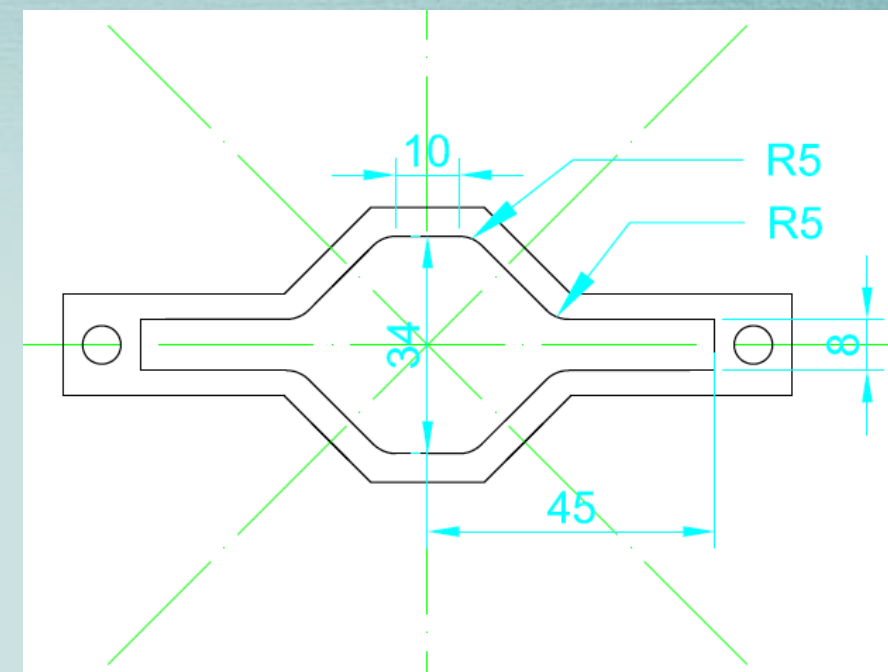
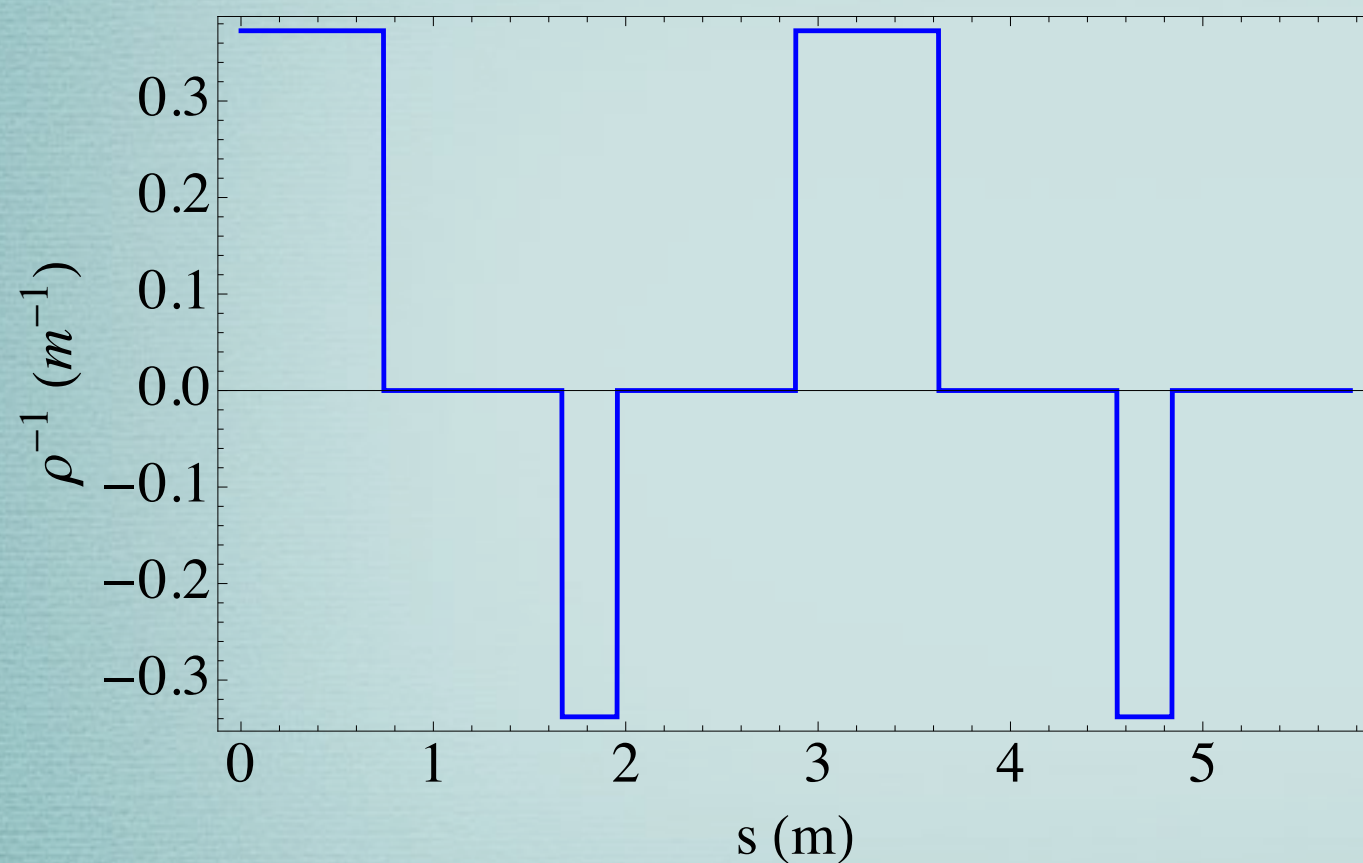
SuperKEKB DR parameters

parameter	Value
Beam energy (GeV)	1.1
Circumference (m)	135.502
Bunch Length (mm)	11.1
Rel. Energy spread (10^{-4})	5.53
Beam pipe height in bends (mm)	34
Beam pipe width in bends w/o antechamber (mm)	34
Effective Length of bends (B1/B2/B3/B4)	0.74248/0.28654/0.39208/.47935
Number of bends (B1/B2/B3/B4)	32/38/4/4
Bending radius (m) (B1/B2/B3/B4)	2.68/2.96/3.15/3.15

Interference - SuperKEKB DR

Vacuum chamber (candidates)

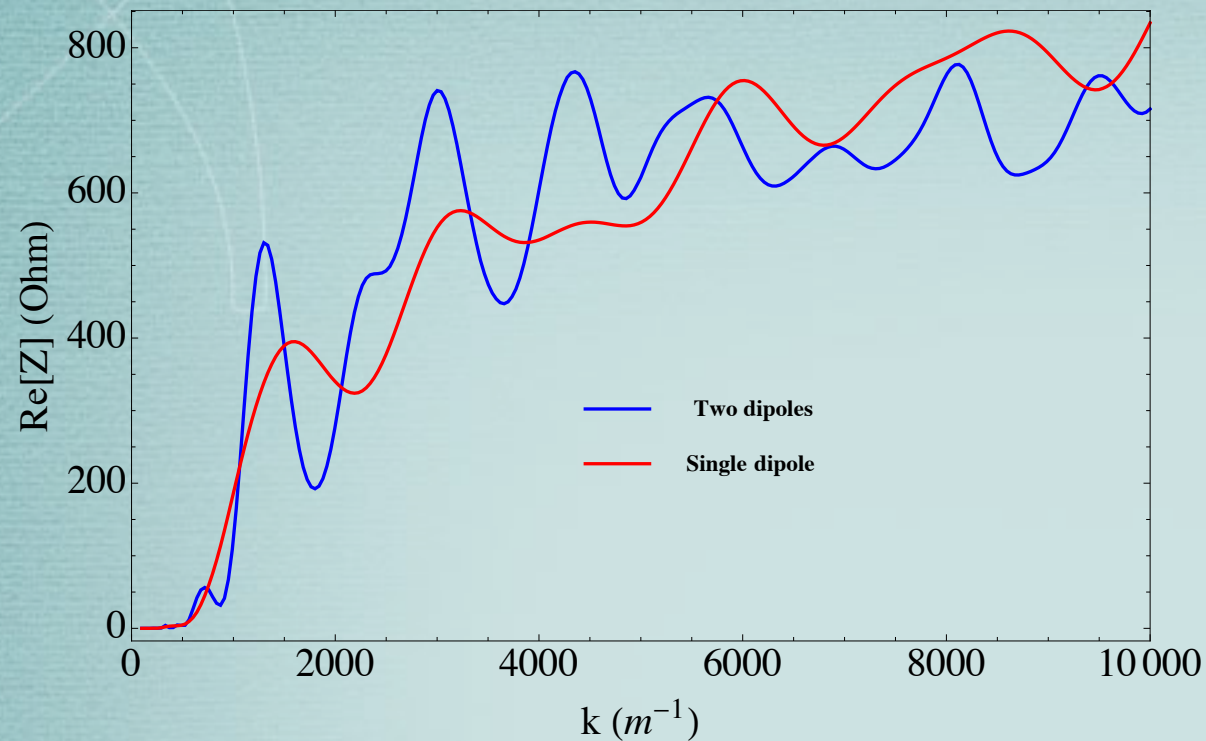
Field distribution (2 cells)



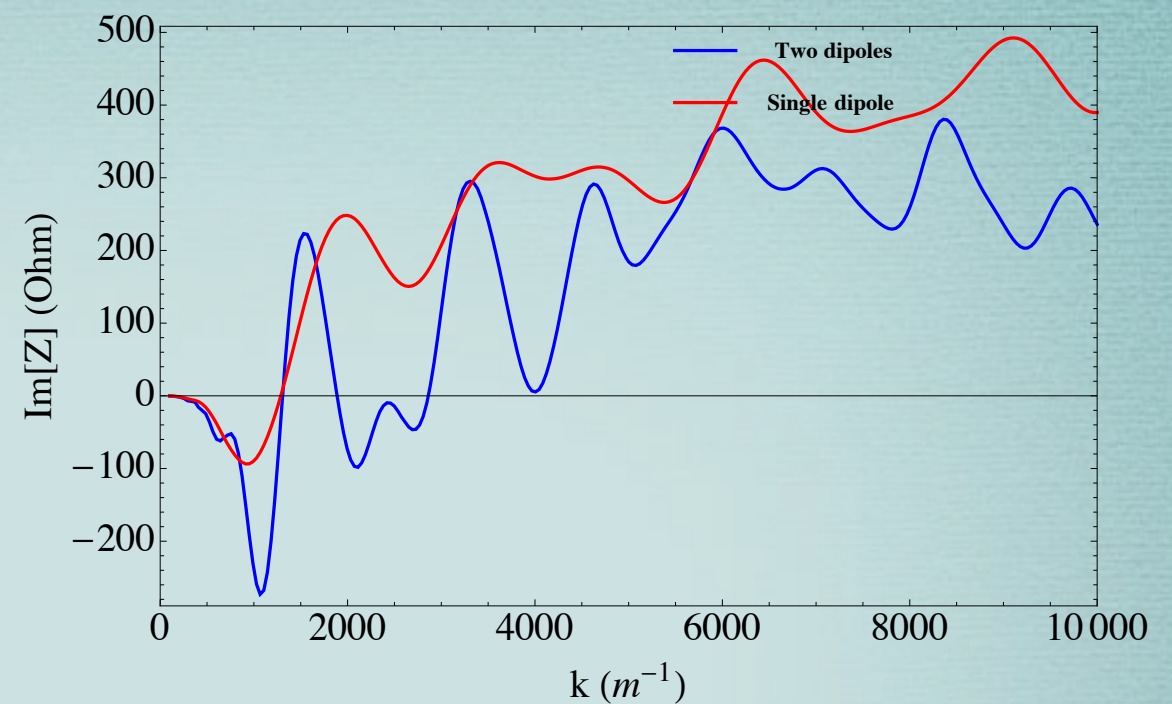
K. Shibata

Interference - SuperKEKB DR

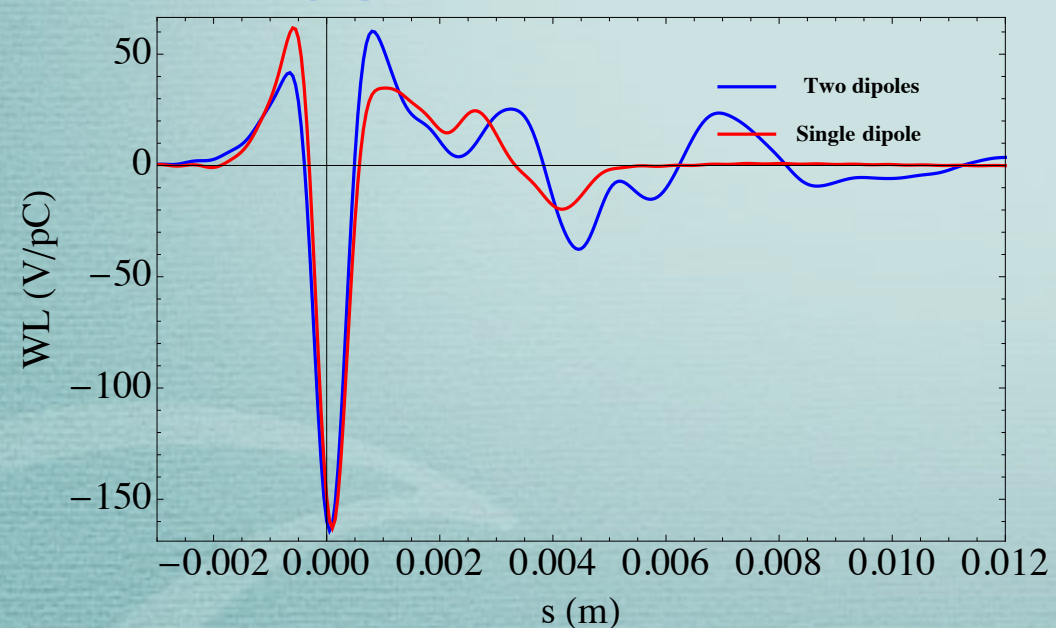
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



1 cell

w/h=34/34mm

B1+B2

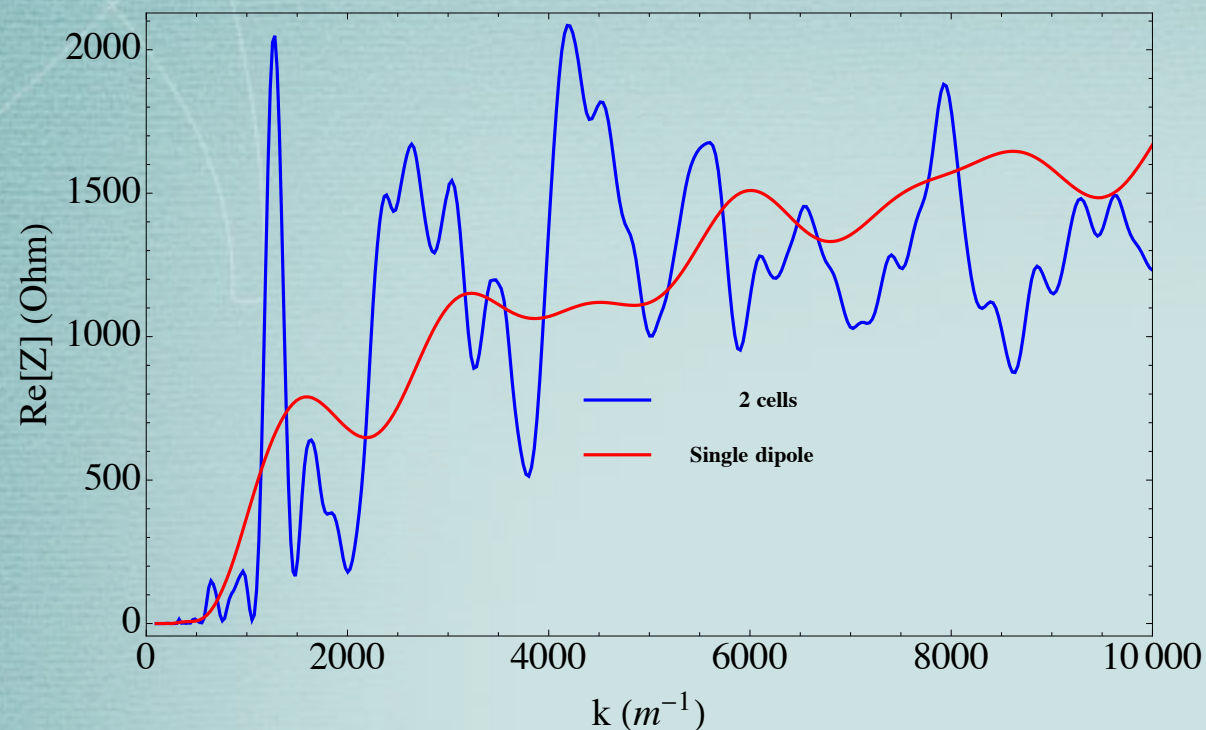
$L_{\text{drift}}=0.93\text{m}$

$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

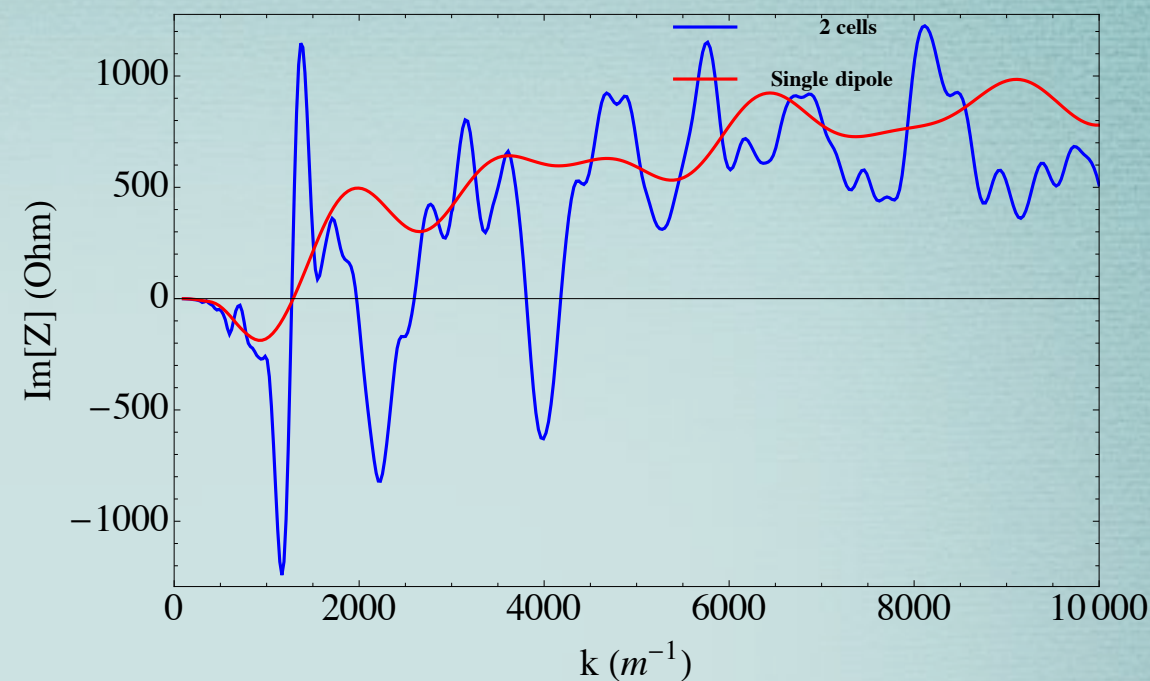
Xoffset=0mm

Interference - SuperKEKB DR

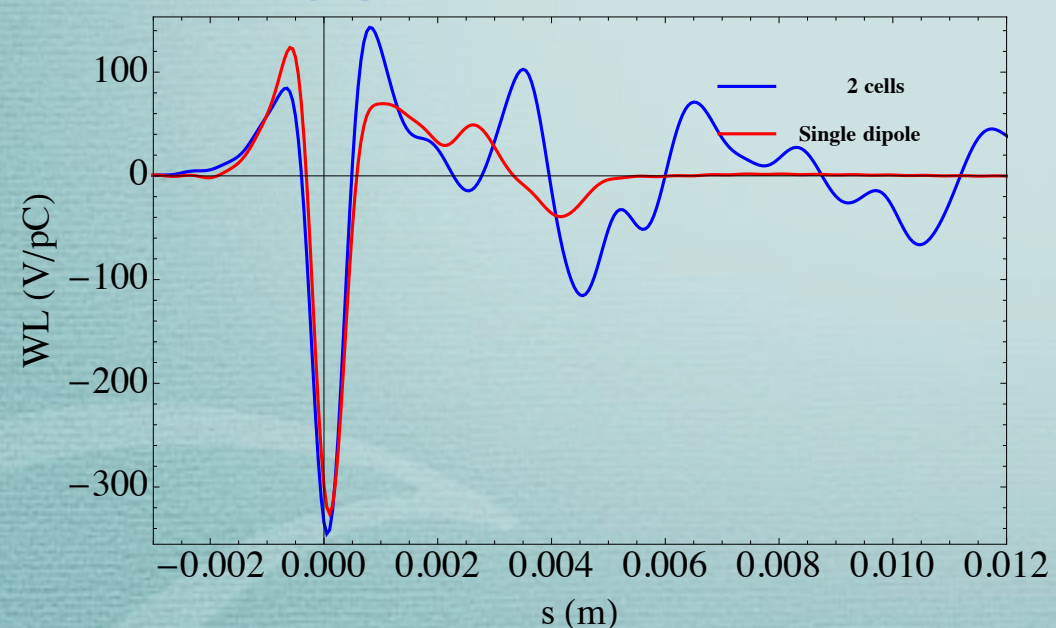
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



2 cells

$w/h=34/34\text{mm}$

$2 \times (B1+B2)$

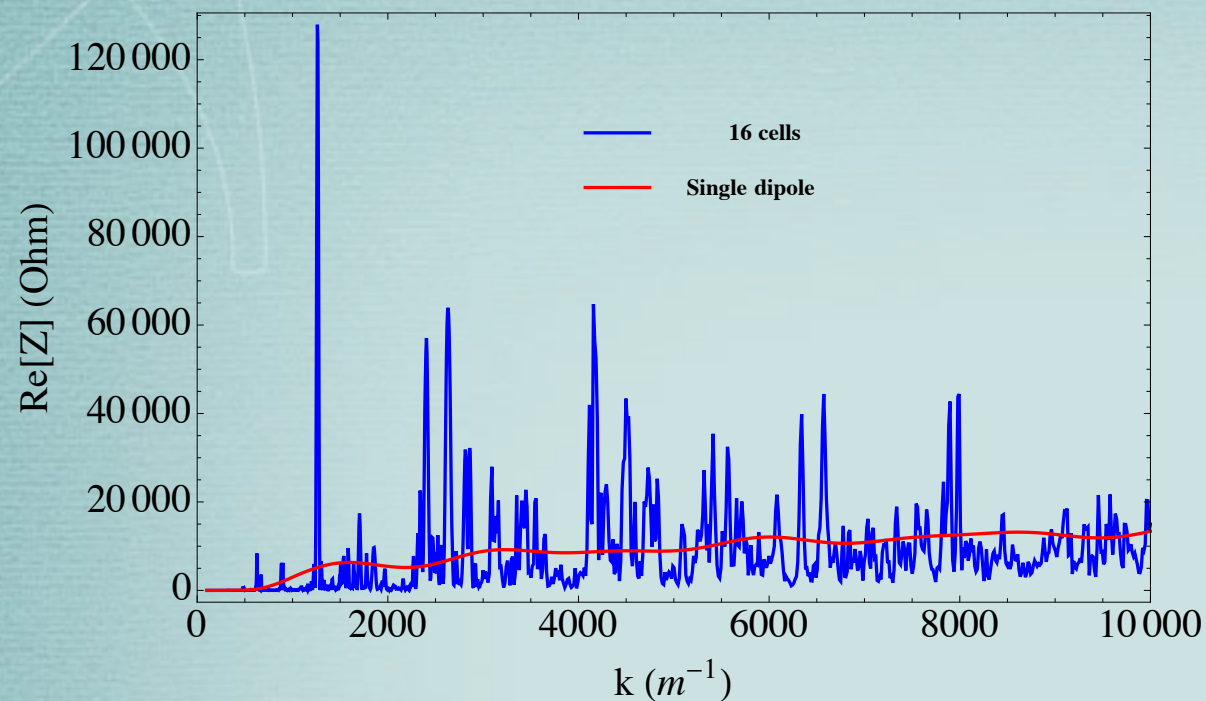
$L_{\text{drift}}=0.93\text{m}$

$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

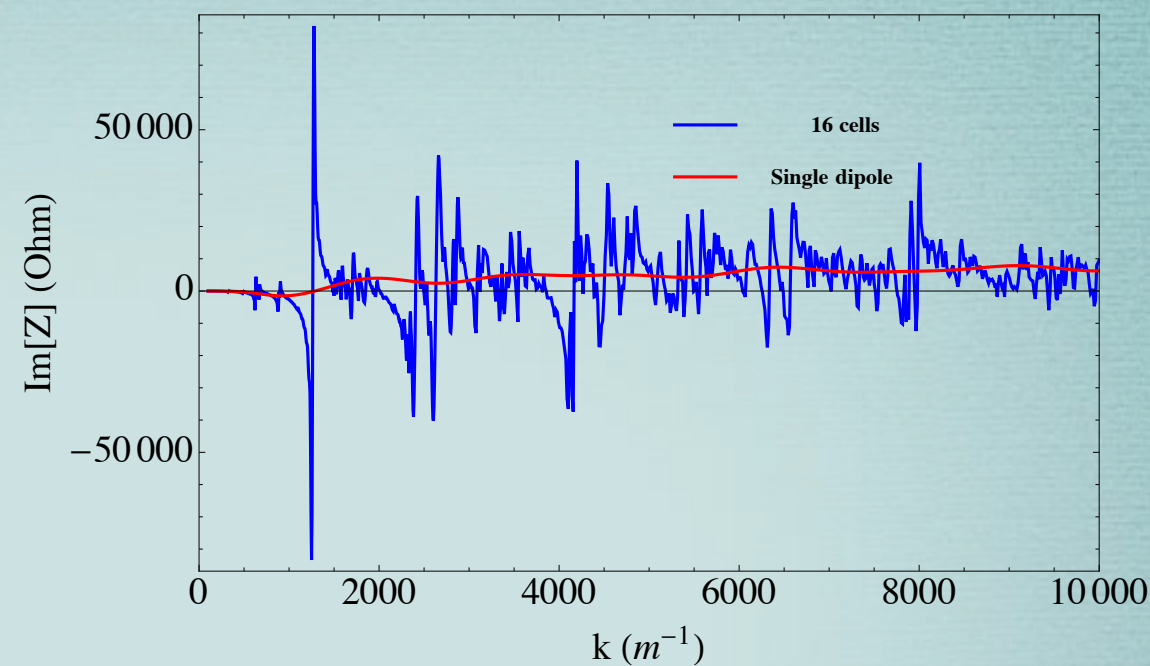
$X_{\text{offset}}=0\text{mm}$

Interference - SuperKEKB DR

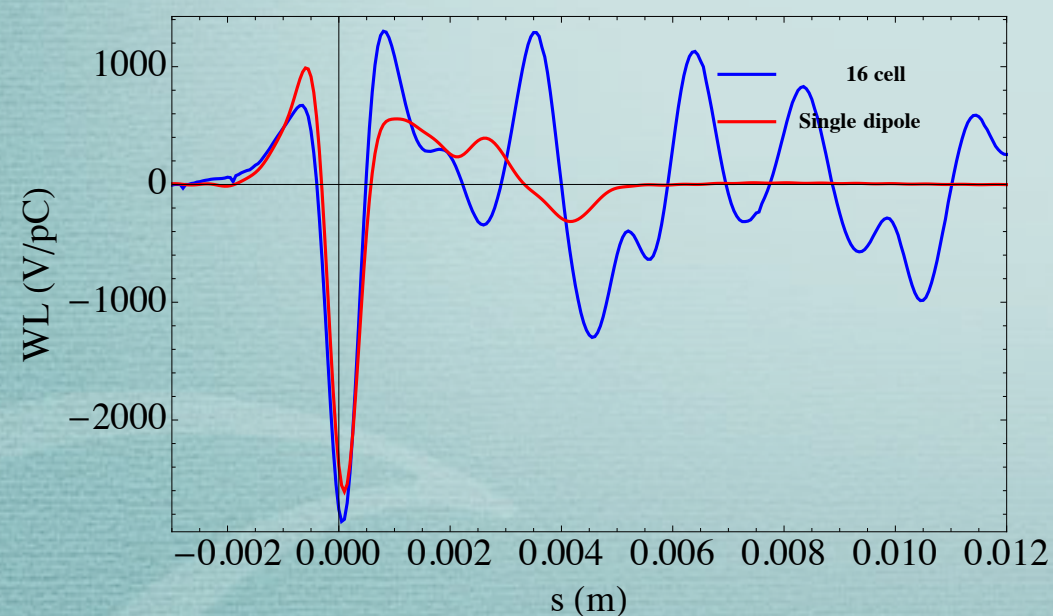
Re. $Z_L(k)$



Im. $Z_L(k)$



$W_L(s)$ with $\sigma_z=0.3\text{mm}$



16 cells

w/h=34/34mm

16×(B1+B2)

$L_{\text{drift}}=0.93\text{m}$

$L_{\text{exit}}=\text{Infinity}$ (pipe after exit)

Xoffset=0mm

Summary

1. Features of the new CSR code (CSRZ):

- 1.1 Low noise level
- 1.2 Allow for s-dependent bending radius (fringe field, wigglers, interference between consecutive dipoles)
- 1.3 Allow for resistive wall (not discussed in this talk and to be benchmarked)

2. Achievements

- 2.1 Limitations in all three codes (GS, KO, DZ) improved after careful benchmark work
- 2.2 Narrow-band impedances (spikes) due to CSR of wigglers were observed which are unexpected according to traditional theories
- 2.3 Interference between consecutive dipoles can be significant and leads to narrow-band CSR impedances (with perfect wall)
- 2.4 CSR calculation for SuperKEKB project

3. Challenges

- 3.1 Computing time is not quite acceptable at high freq. or very long components which require refinements in meshes or huge integration steps
- 3.2 “Wiggling pipe” is not good approximation
- 3.3 Treating pipe with arbitrary cross section is unavailable