Coupled-bunch instability driven by resistive wall impedance at SuperKEKB main rings

Accelerator theory group, Accelerator laboratory, KEK

Acknowledgments

M. Tobiyama, T. Ishibashi, M. Migliorati, G. Bassi, A. Blednykh

Mini-workshop on impedance modeling and impedance effects at SuperKEKB and future colliders, KEK, Dec. 15, 2022

Demin Zhou

Outline

- Vacuum chambers
- Optics
- Measurements of TCBI at SuperKEKB
- TCBI theory and predictions of TCBI growth time



Vacuum chambers

- Normal chambers at SuperKEKB rings [1]
 - LER: Round chamber with ante-chambers coating.
 - HER: Race-track chamber ~70%, copper.



Figure 1: Typical cross-section of beam pipes in SuperKEKB. Left: LER with antechamber at arc sections in a sextuple magnet. Right: HER with race-track shape at the arc sections in a quadrupole magnet.

• LER: Round chamber with ante-chambers ~90%, radius 45 mm, aluminum with TiN 0.2 μ m



Vacuum chambers

- IR chamber [1] \bullet
 - Chamber radius from 40 to 10 mm from ± 2.5 m from IP. \bullet
 - Local beta functions vary very fast around IP.



scheme [27].

Do analytic theories of RW impedance apply to SuperKEKB IR chamber?

$$Z_1^{\perp}(\omega) = \frac{f_Y L(\operatorname{sgn}(\omega) - i)}{\pi b^3} \sqrt{\frac{Z_0 c}{2 |\omega| \sigma_c}}$$



FIG. 7. Physical aperture of the HER (a) and LER (b) beam pipes in the IR, as implemented in SAD. Colored lines represent the beam envelope, which is limited by collimators. Arrows indicate the beam direction. The beam optics simulated are those of June 2020: a beta function at the IP of $\beta_{H/V}^* = 60/0.8$ mm and crab sextupoles turned on for a so-called Crab Waist collision

Courtesy of A. Natochii

[1] A. Natochii et al., PRAB 24, 081001 (2021).





Vacuum chambers

- Collimators [1] \bullet
 - KEKB-type collimators are mainly used in HER.
 - type collimators in LER).



FIG. 5. KEKB-type collimators have a single jaw, on only one side of the beam. All dimensions are in mm. (a) Conceptual drawing of the collimator assembly [16]. (b) Schematic drawing of the horizontal collimator chamber.

Do analytic theories of RW impedance apply to SuperKEKB collimators?

$$Z_1^{\perp}(\omega) = \frac{f_Y L(\operatorname{sgn}(\omega) - i)}{\pi b^3} \sqrt{\frac{Z_0 c}{2 |\omega| \sigma_c}}$$

• SuperKEKB-type collimators are mainly used in LER (ante-chambers limit the use of KEKB-





FIG. 6. SuperKEKB-type collimators have two jaws, one on each side of the beam. All dimensions are in mm. (a) Conceptual drawings of the collimator assembly [17]. (b) Schematic drawing of the collimator jaw.

Courtesy of A. Natochii

[1] A. Natochii et al., PRAB 24, 081001 (2021).







Optics

- IR optics
 - TCBI theory depend on beta functions



[1] A. Natochii et al., PRAB 24, 081001 (2021).

See talks by G. Bassi and T. Ishibashi

$$\bar{Z}_{1}^{\perp}(\omega) = \sum_{i} \beta_{yi} Z_{1i}^{\perp}(\omega)$$

Does "smooth approximation" apply to SuperKEKB IR?

















TCBI at HER

- Grow-damp study at HER (2021.06.29, M. Tobiyama)
 - Mode -1 dominates the instability.
 - This instability should be attributed to resistive wall (RW) impedance.







Courtesy of M. Tobiyama





TCBI at HER

- Grow-damp study at HER (2021.06.29, M. Tobiyama)
 - Mode -1 dominates the instability.













SuperKEKB Beam Instrme During collision (by*=1mm, 670mA)

Question: Does the growth rate depend on β_v^* ?



Courtesy of M. Tobiyama





TCBI at LER

- Grow-damp study at LER (2022.03.28, M. Tobiyama)
 - Mode -1 dominates the instability.
 - This instability should be attributed to resistive wall (RW) impedance.

SuperKEKB Beam Instrmentation

Single beam 600mA





Courtesy of M. Tobiyama



TCBI at LER

- Grow-damp study at LER (2022.03.28, M. Tobiyama) \bullet
 - Mode -1 dominates the instability.
 - Growth time around 3.6 ms with Ibeam=600 mA. \bullet
 - This instability should be attributed to resistive wall (RW) impedance.



Courtesy of M. Tobiyama



- Assume a uniform filling pattern. The n-th bunch takes the motion of [1] $y_n^{\mu}(t) = A e^{2\pi i \frac{\mu n}{M}} e^{-i\Omega_{\mu}^{U}t}$ (1)
- M=5120 for SuperKEKB. The eigenvalues Ω^U_{μ} are given by [2]

$$\Omega^U_\mu = -i \frac{I_0}{2T_0(E/e)} \sum_{p=-\infty}^{+\infty} |$$

growth rate

$$\frac{1}{\tau_{\mu}^{U}} = -\frac{I_{0}}{2T_{0}(E/e)} \sum_{p=-\infty}^{+\infty} |\lambda(\tilde{p}')|$$

[1] A. Wolski, "Beam dynamics in high energy particle accelerators", Imperial College Press, 2014. [2] G. Bassi et al, PRAB 25, 014402 (2022).

 $|\lambda(\tilde{p}')|^2 \bar{Z}_1^{\perp}(p')$ (2)

• $p' = (pM + \mu + \nu_v)\omega_0$, $\omega_0 = 2\pi f_0 = 2\pi/T_0 = 2\pi/(C/c)$ with C = 3016.315 m for SuperKEKB. I_0 is the total beam current. E is the beam energy. The imaginary part of Ω^U_μ determines the

 $|^{2}$ **Re** $[\bar{Z}_{1}^{\perp}(p')]$ (3)

- The transverse average impedance $\bar{Z}_1^{\perp}(\omega)$ (weighted by local beta functions) is $\bar{Z}_1^{\perp}(\omega) = \sum \beta_y$
- The major contribution to the TCBI is from low-frequency resistive wall impedance [1]

$$Z_1^{\perp}(\omega) = \frac{f_Y L(\operatorname{sgn}(\omega) - i)}{\pi b^3} \sqrt{\frac{Z_0 c}{2 |\omega| \sigma_c}}$$
(5)

• f_Y is the geometric factor (Yokoya factor): For components with round geometry, $f_Y=1$; For TCBI.

$$_{yi}Z_{1i}^{\perp}(\omega)$$
 (4)

components with parallel-plates geometry, $f_Y = \pi^2/12$. L is the length of the component. b is the half aperture (chamber radius). σ_c is the electrical conductivity. Since only impedance at low frequency $\omega \approx \omega_0$ is important for TCBI, coating (such as TiN) is negligible in the evaluation of





- Benchmark of impedance formulae with IW2D (Green lines, by M. Migliorati) for LER
- Analytic theory for RW: Simple model (Eq.(5)) and two-layer model [1]



[1] M. Ivanyan and V. Tsakanov, PRST-AB 7, 114402 (2004).

• Good agreement was seen in the frequency range ($f_0 \approx 100$ kHz) of interest for TCBI analysis.



• The growth rate of RW driven TCBI scale as

$$\frac{1}{\tau_{\mu}^{U}} \propto \frac{I_0 L \beta_y}{b^3 \sqrt{\sigma_c}} \quad (6)$$

• The fasted growth rate of RW driven TCBI modes is given by

$$\frac{1}{\tau_y} = \frac{I_0}{2T_0(E/e)} \operatorname{Re}[\bar{Z}_1^{\perp}(-(1-Q_y)\omega_0)] = \frac{I_0}{2T_0(E/e)} \frac{1}{\sqrt{1-Q_y}} \operatorname{Re}[\bar{Z}_1^{\perp}(\omega_0)] \quad \text{(7)}$$

The fractional part of ν_y : $Q_y = \nu_y - \operatorname{Int}[\nu_y]$. The above equation is determined by [1]
 $p' = (pM + \mu + \nu_y)\omega_0 = -(1-Q_y)\omega_0 \quad \text{(8)}$
 $p = -1, \ \mu_m = M - (\nu_y + 1 - Q_y) = M - \operatorname{Int}(\nu_y) - 1, \text{ assuming } 0 \le \mu < M.$ The fast is the first set of the formula of the f

- Q_v is th
- It gives μ_m corresponds to the "-1 mode" in measurement.

[1] A. Wolski, "Beam dynamics in high energy particle accelerators", Imperial College Press, 2014.

Question: Does Eq.(6) imply the collimators (small b) and IR (large $\beta_{\rm y}$) can be important for TCBI?



Effect of slow head-tail effect

• Positive chromaticity generates head-tail damping [1,2]



[1] G. Bassi, Talk to TWIICE, 2016. [2] G. Bassi et al., NIMA 810 (2016) 151-163.



Effect of uneven filling pattern

• With a gap ratio w<0.3, the simple theory with an even filling pattern seems to work well [1]

Gennady Stupakov SLAC National Accelerator Laboratory, Menlo Park, CA 94025

Gap w = 0.3 in the bunch train

 $[v_{\beta}] = 0.05$, gap w = 0.3 with the same beam current I as in a uniform fill.

Red—uniform fill, blue—a fill with 0.3 gap, 41 modes, green—a fill with 0.3 gap, 61 modes.



[1] G. Stupakov, "Multi-bunch instability with uneven fills", presented at HSC meeting, CERN, Apr. 18, 2016.

Multi-bunch instability with uneven fills

CERN, April 18, 2016

Summary

- With the number of bunches in the collider $M \gg 1$ one can use a continuous approximation to calculate the transverse MBI with non-uniform fills. An integral equation is derived for the coherent frequency shift of the beam oscillations in fluid approximation. For a given fill pattern, this equation can be easily solved using the Fourier expansion.
- For the RW MBI, gaps up to w = 0.3 do not noticeably change the growth rate of the most unstable mode (assuming the same averaged current of the beam)

I am interested in finding other applications for this technique and making comparison with computer simulations.

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TCBI at LER (Machine conditions of 2022.03.28)

- For IR chambers, $\tau_{v2}=1.14$ ms with $I_0=600$ mA and $\beta_v^*=1$ mm.
- For collimators, τ_{v3} =23.1 ms with I_0 =600 mA.
- SR radiation damping time τ_{vSR} =-45.7 ms.
- Head-tail damping time with $\xi_v = +1.5$, $\tau_{vHT} = -17.9$ ms. (This value seems to be consistent with the findings of Refs.[1,2] (to be confirmed))
- In total, we obtain a growth time of $\tau_v^{Theory} = 1$ ms. This cannot explain the experimental data of τ_v^{Exp} =3.6 ms (see page.11).

[1] J. Keintzel et al., IPAC2021, TUPAB010. [2] N. Kuroo et al., IPAC2017, THPVA012.

• For SuperKEKB LER, the main sources of RW impedance are: 1) Normal chambers with b=45mm; 2) IR chambers with large β_v and $b \approx$ 10 mm; 3) Small-gap collimators with b ~1 mm.

- For normal chambers, we take b=45 mm, L=3011 m, σ_c =3.8e7 S/m for aluminum, β_v =25.3 m for the arc and straight sections. The growth time of the fast mode is τ_{v1} =6.65 ms with I_0 =600 mA.





TCBI at HER (Machine conditions of 2021.06.29)

- collimators with $b \sim 1.4 4.0$ mm.
- For IR chambers, $\tau_{v2}=0.82$ ms with $I_0=600$ mA and $\beta_v^*=1$ mm.
- For collimators, τ_{y3} =5.25 ms with I_0 =600 mA (Total jaw length is longer than that of LER).
- SR radiation damping time τ_{ySR} =-58 ms.
- Head-tail damping time with $\xi_v = +1.5$, $\tau_{vHT} = ?$ ms (Not estimated yet).
- In total, we obtain a growth time of $\tau_v^{Theory}=0.5$ ms. This cannot explain the experimental data of τ_v^{Exp} =1.6 ms.

• For SuperKEKB LER, the main sources of RW impedance are: 1) Normal chambers with b=25mm, considering Yokoya factor; 2) IR chambers with large β_v and $b \approx$ 10 mm; 3) Small-gap

- For normal chambers, we take b=25 mm, L=3011 m, σ_c =5.8e7 S/m for copper, β_v =25.8 m for the arc and straight sections. The growth time of the fast mode is $\tau_{v1}=1.68$ ms with $I_0=600$ mA.



Open questions



Do Eqs. (4-5) with $\omega_0 = 2\pi f_0$ apply to the SuperKEKB-type collimator (*L* and *b* are simultaneously very small)?

 $\bar{Z}_1^{\perp}(\omega) =$

 $f_Y L(sgn)$ $Z_1^{\perp}(\omega) = \frac{J_2}{-}$ πl

Courtesy of A. Natochii





$$\sum \beta_{yi} Z_{1i}^{\perp}(\omega)$$
 (4)

i

$$\frac{\omega(\omega) - i}{b^3} \sqrt{\frac{Z_0 c}{2 |\omega| \sigma_c}}$$
(5)

Do Eqs. (4-5) with $\omega_0 = 2\pi f_0$ apply to the SuperKEKB IR (tapered structure with fast variation in beta functions)?

Summary

- filling pattern) with a simple resistive wall model.
- Questions
 - chamber lengths are small)?
 - Are there any missing factors affecting TCBI growth time?
- and vertical collimators (due to smaller gaps).

The TCBI observed in SuperKEKB cannot be well explained by the simple CBI model (uniform)

 The theories of RW impedance assume a smooth chamber in the s-direction. Are these theories applicable to the cases of 3D structures like IR chambers and collimators (where

• Squeezing β_v^* may cause more contributions to TCBI from the interaction region (due to larger β_v)





TCBI at HER

- Grow-damp study at HER (2021.06.29, M. Tobiyama)
 - Mode -1 dominates the instability.
 - This instability should be attributed to resistive wall (RW) impedance.

HER vertical CBI

- Measurement of instability growth rate and feedback damping rate using transient domain analysis with iGp12 digital filters.
 - turn off FB (10ms 15ms) and turn-on again, record 12MB data
- by*=8mm (200mA, 370mA), by*=1mm (200mA, 400mA, 600mA) with normal filling pattern of current runs.

SuperKEKB Beam Instrmentation

Courtesy of M. Tobiyama

SuperKEKB Beam Instrmentation

by*=8mm 200mA





