

ARES Upgrade for Super-KEKB

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for the KEKB-ARES group

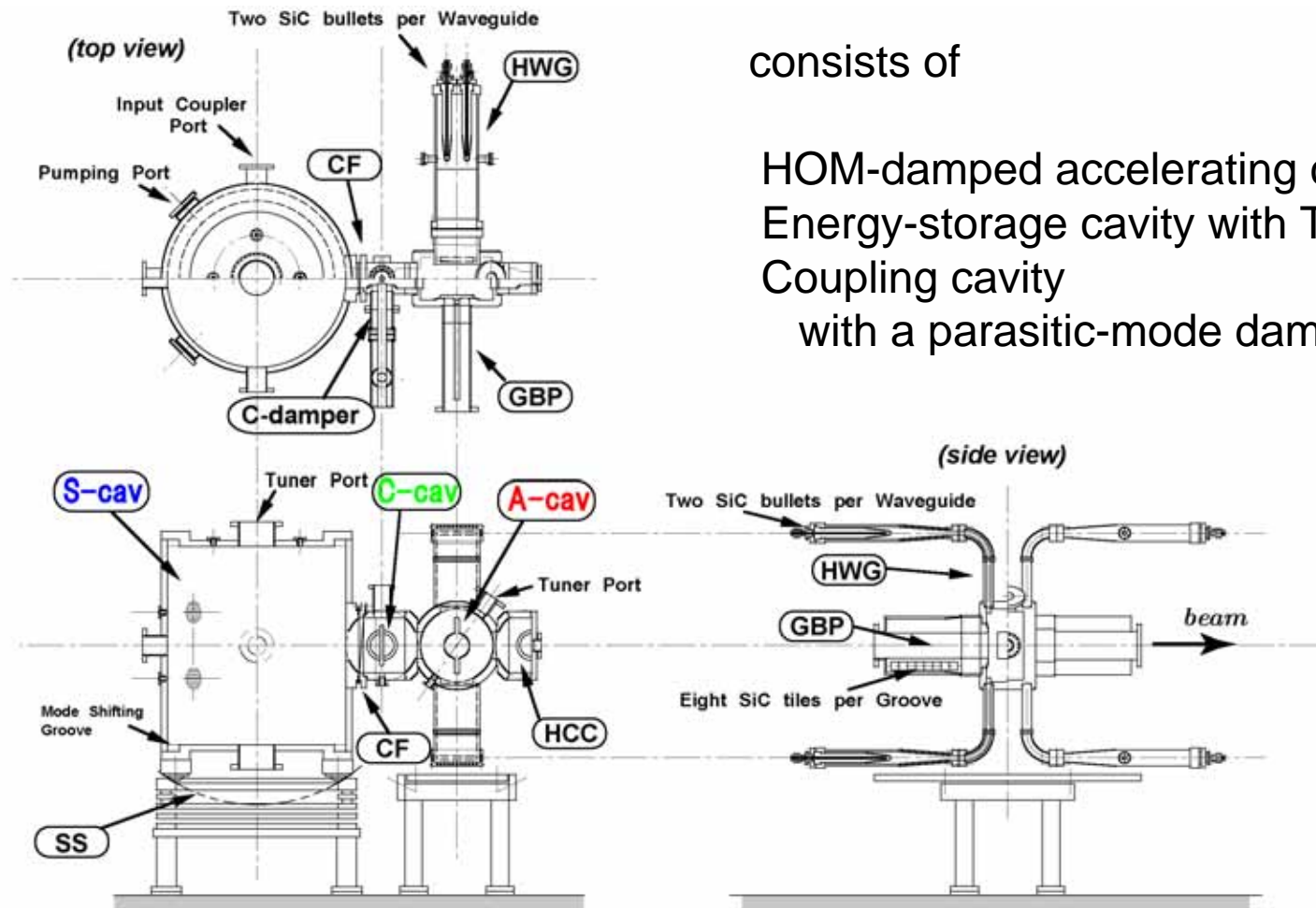
High Energy Accelerator Research Organization (KEK)

〈Outline〉

1. Introduction
2. Upgrade items
3. Change of the stored-energy ratio
4. HOM-load upgrade
5. Coupler R&D
6. Summary

Accelerator Resonantly-coupled with Energy Storage

3-cavity system stabilized with the $\pi/2$ -mode operation



consists of


- HOM-damped accelerating cavity (**A-cav**)
- Energy-storage cavity with TE013 (**S-cav**)
- Coupling cavity (**C-cav**) with a parasitic-mode damper

Operation with the Accelerating $\pi/2$ Mode

 **The stored-energy ratio: U_s/U_a**

→ can be changed

$$\frac{U_s}{U_a} = \frac{k_a^2}{k_s^2}$$

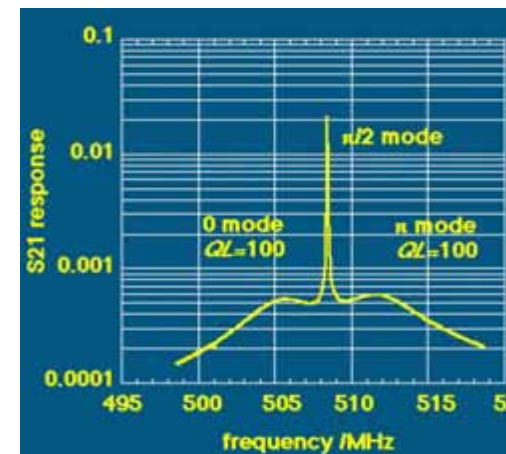
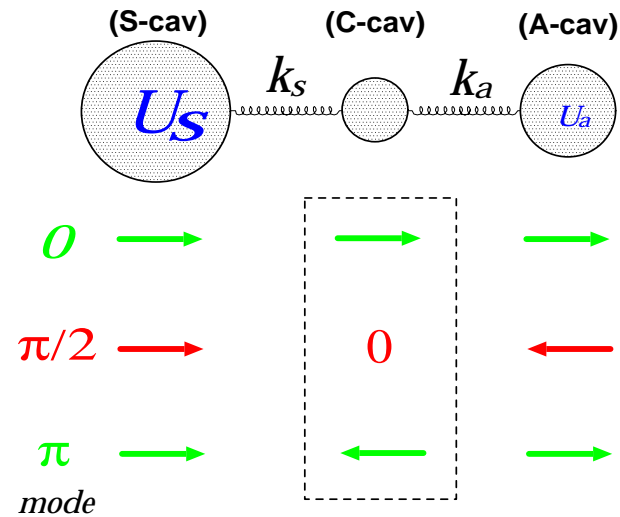
 **The field of the $\pi/2$ mode is the most stable against**

- Beam loading,
- Detuning of A-cav (= f_a).

$$f_{\pi/2} = \frac{f_a}{1 + U_s/U_a}$$

 **The parasitic 0 and π modes**

→ can be damped selectively
out of C-cav (C-damper)



Operation Status @



(Apr.~Jun., 2003)

➤ LER: 20 cavities

- Total $V_c=8.0\text{MV}$
- Beam current (max.): $\sim 1.8\text{A}$
- Input RF power /cav: $\sim 300\text{kW}$
- HOM power: $>\sim 5\text{kW}$
- Trip rate: ~ 1 /cav /3months

➤ HER: 10 cavities (with 8 SCCs)

- Total $V_c = 13\text{MV}$
= $2.84\text{MV}(\text{ARES}) + 10.16\text{MV}(\text{SCC})$
- Beam current (max.): $\sim 1.1\text{A}$



ARES cavities in the LER RF section

Upgrade for



Measures against

Larger detuning

→ Change the energy ratio: $U_s/U_a = 9 \rightarrow 15$ (?)

$$f_{\pi/2} = \frac{f_a}{1 + U_s/U_a}$$

| f_a | = 200 kHz in KEKB (2.6A, 20 sets)

| f_a | = 710 kHz in SuperKEKB (9.4A, 28 sets)

Cf. $f_{rev} = 99\text{kHz}$

Higher HOM power

→ HOM-load upgrade

Higher input RF power (400kW/cav → >800kW/cav)

→ R&D in the new coupler teststand

Change of the Energy Ratio

 $\pi/2$ mode & eq. circuit

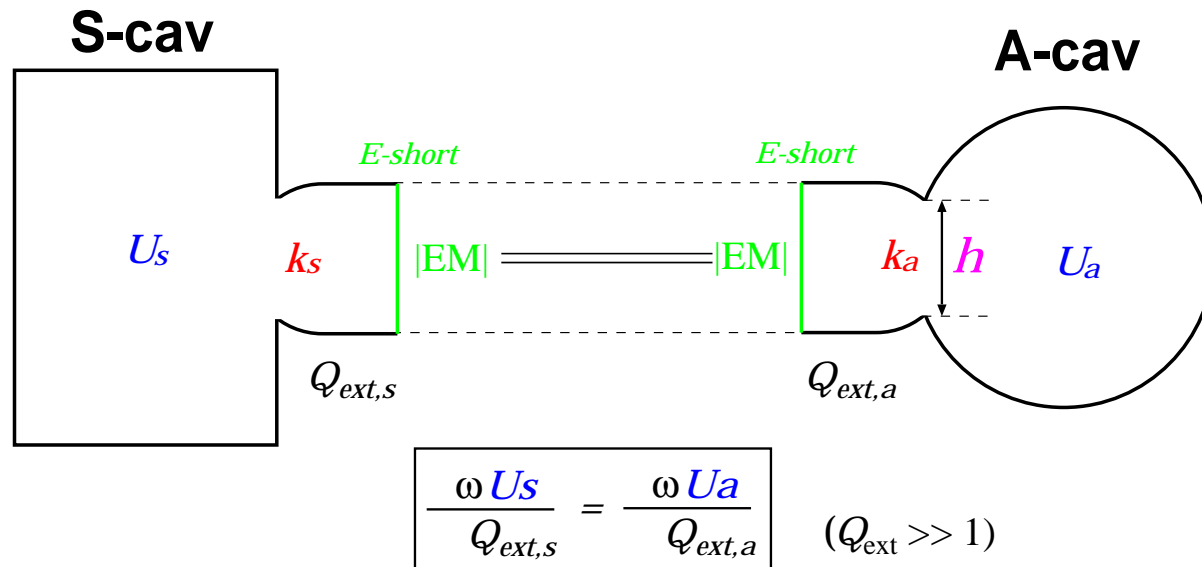
$$\frac{U_s}{U_a} = \frac{k_a^2}{k_s^2}$$

 Applying Slater's tuning curve to the $\pi/2$ mode

$$\frac{U_s}{U_a} = \frac{Q_{ext,s}}{Q_{ext,a}}$$

Changing the window height: h ,

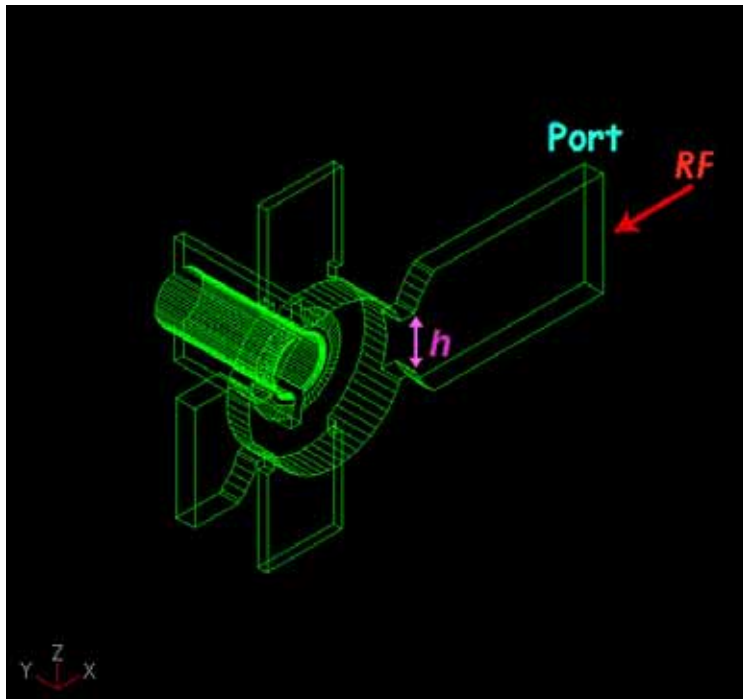
→ U_s/U_a , $Q_{ext,s}/Q_{ext,a}$ can be adjusted.



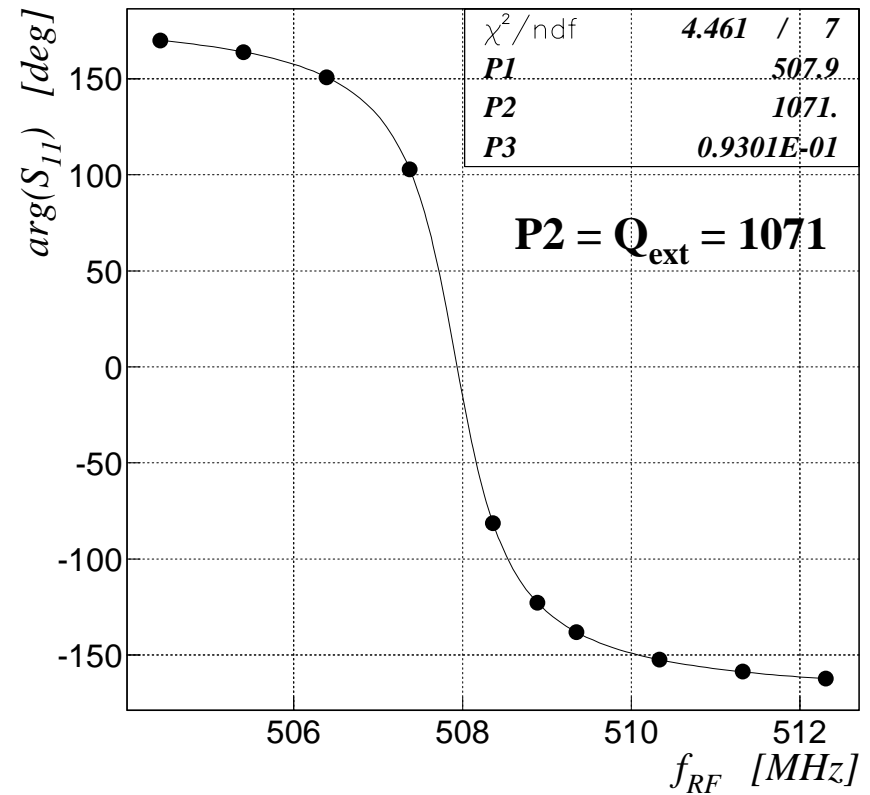
Adjusting the Window Height of A-cav

 **Simulation tool: HFSS**
 → S-parameter calculation

 **Geometry**

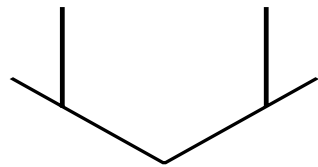


$$\arg(S_{11}) = -2 \tan^{-1} \left\{ P_2 \left(\frac{f_{RF}}{P_1} - \frac{P_1}{f_{RF}} \right) \right\} + P_3$$

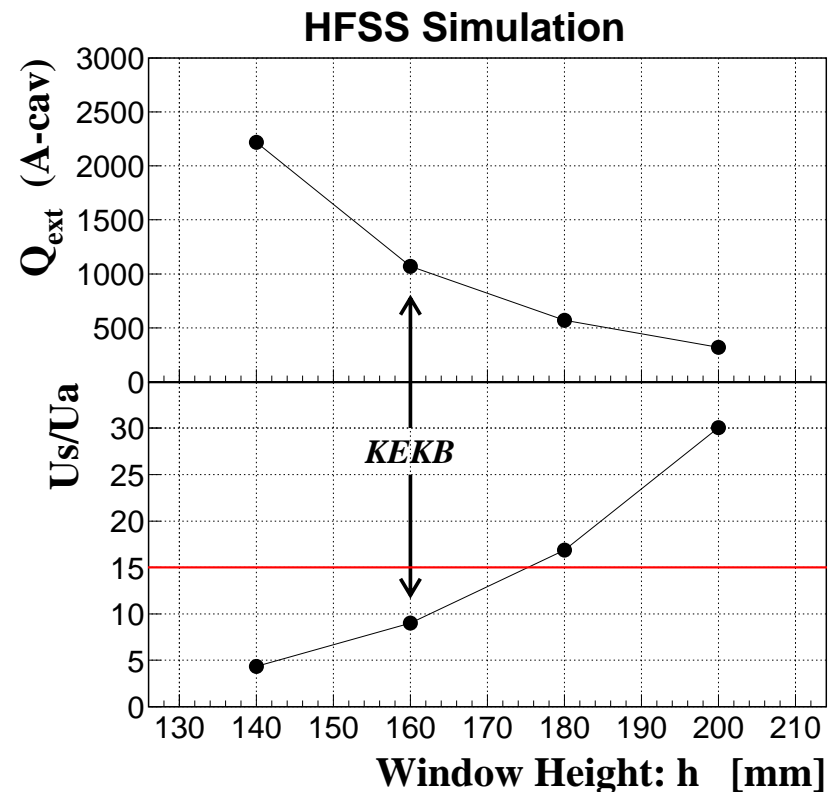


Window Height v.s. Energy Ratio

Modification of the window
height: +15mm (160→175mm)
for $U_s/U_a=15$

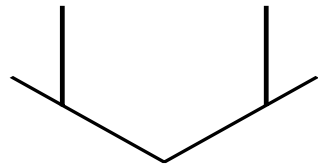


Acceptable for the current
mechanical structure

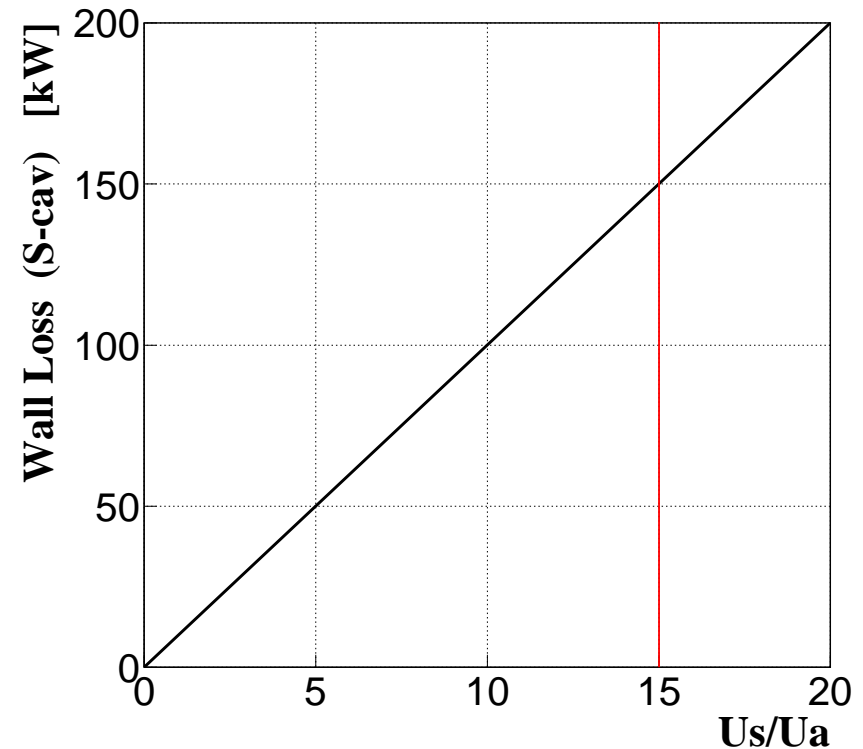


Wall Loss in Energy-storage Cavity

**$P_{\text{wall}}=150\text{kW}$
for $U_s/U_a=15$**



**Record: $P_{\text{wall}}>200\text{kW}$
in the teststand**



Longitudinal Coupled-bunch Instability driven by the $\pi/2$ mode

Larger detuning

- Larger instability driven by the accelerating $\pi/2$ mode
- Cured by increasing the energy ratio: U_s/U_a

$$f_{\pi/2} = \frac{f_a}{1 + U_s/U_a}$$

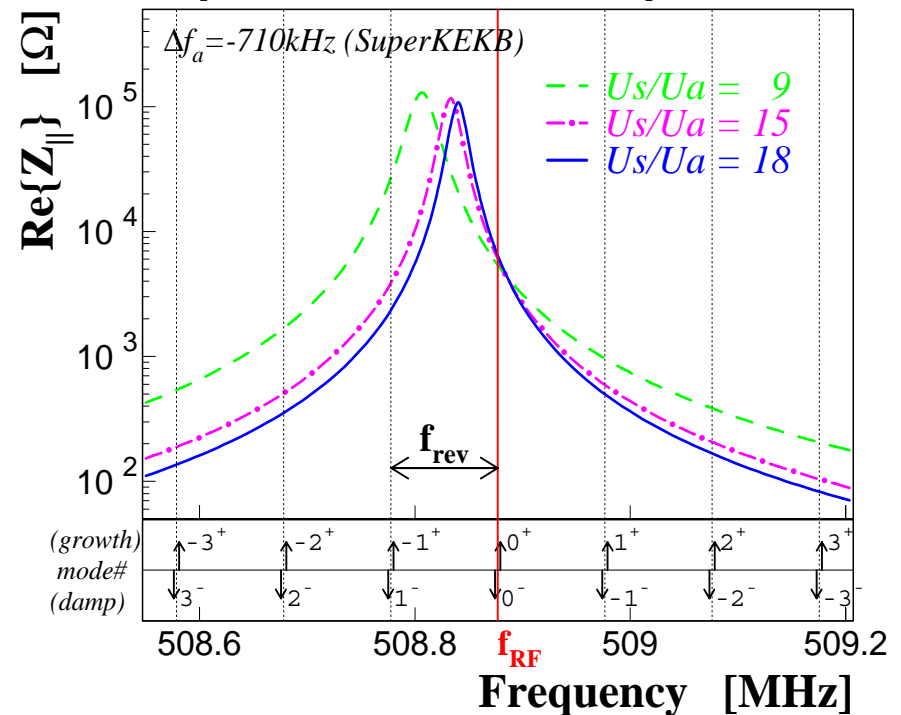
| f_a | = 200 kHz (in KEKB)

| f_a | = 710 kHz (in SuperKEKB)

Cf. $f_{rev} = 99\text{kHz}$

We need a feedback?

Impedance/cav of the $\pi/2$ Mode

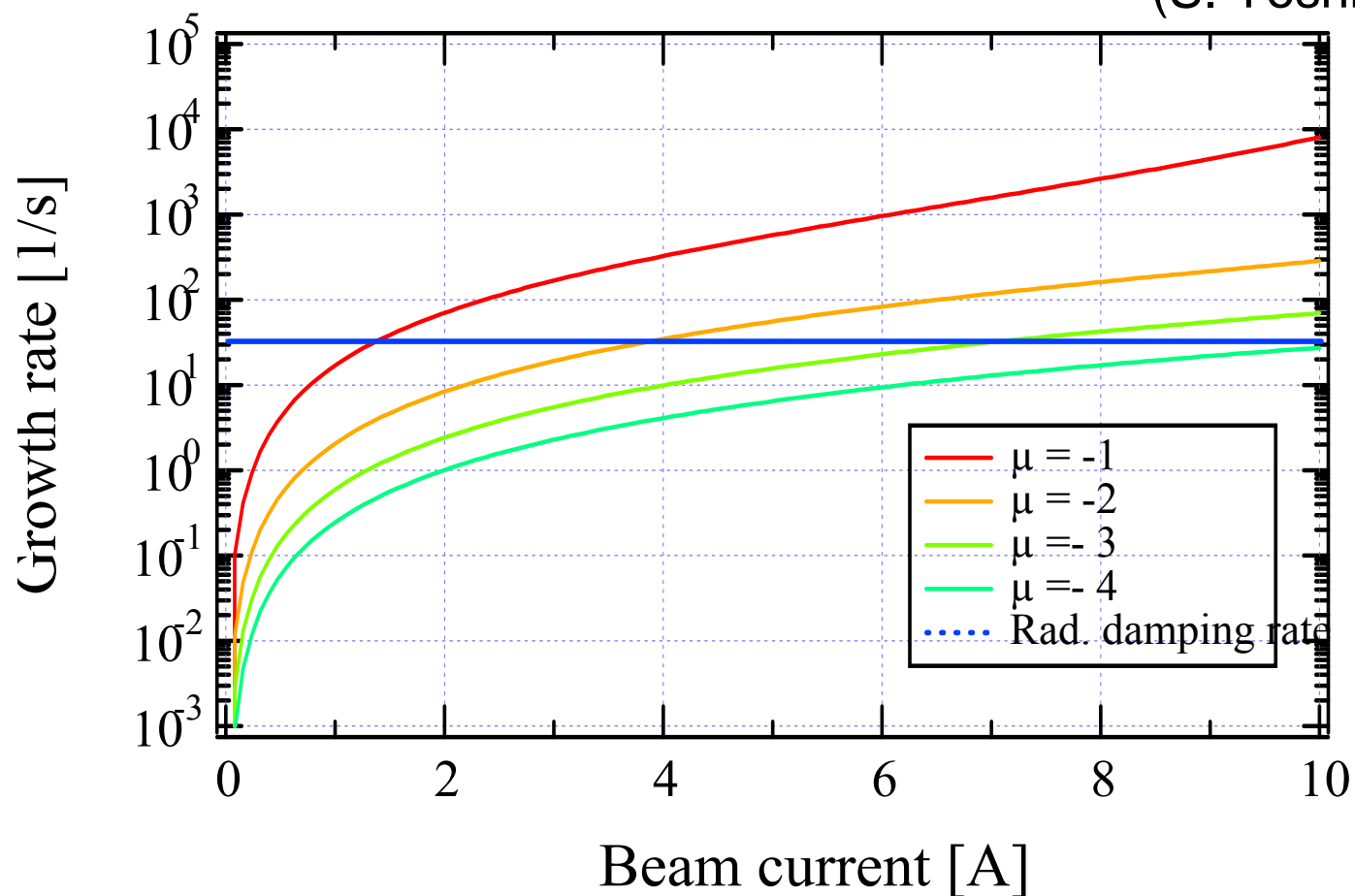


Growth Rate(1)

SuperKEKB
LER
ARES 28 sets

$U_a : U_s = 1 : 9, V_c = 0.5 \text{ MV}$

(S. Yoshimoto)

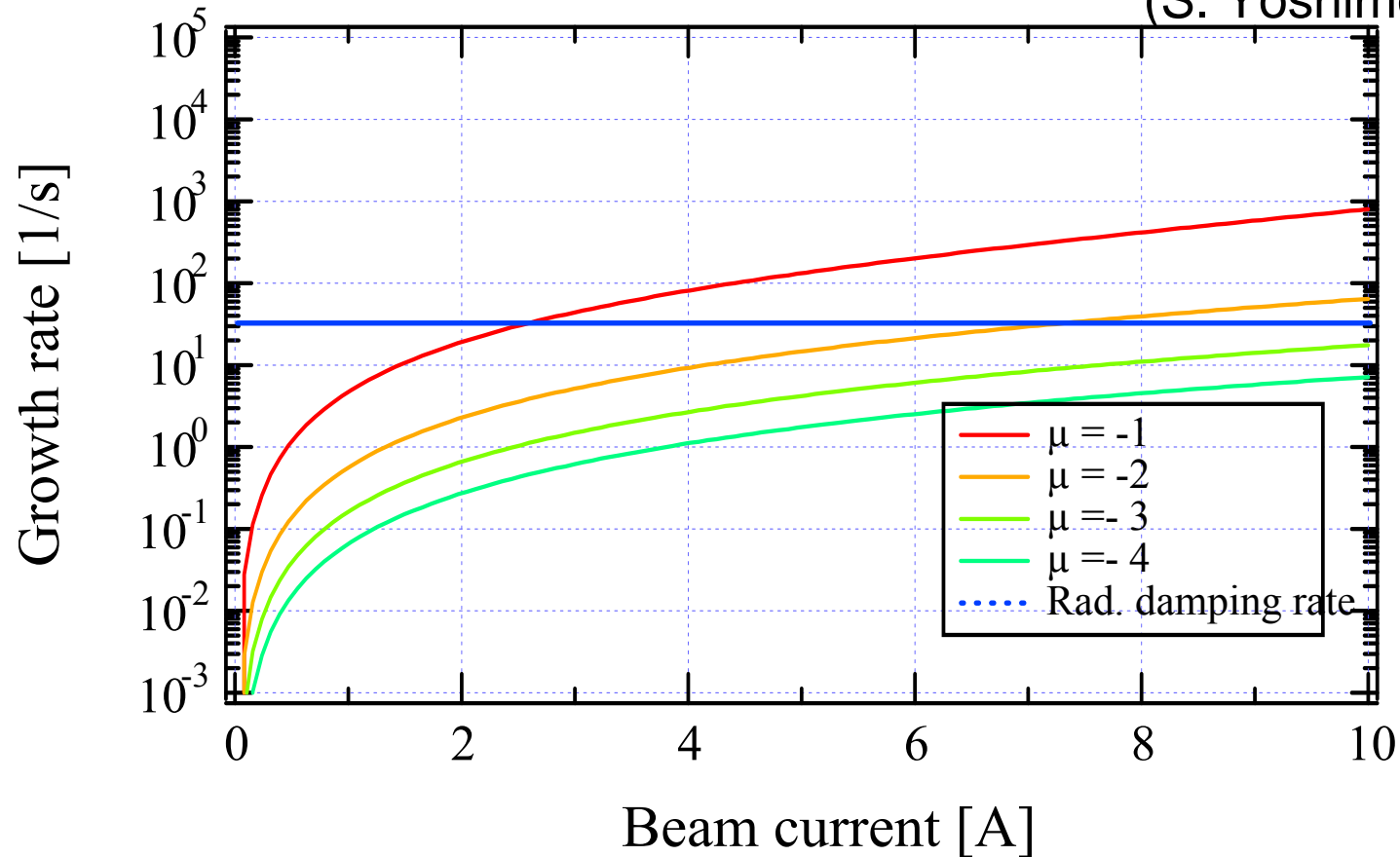


Growth Rate(2)

SuperKEKB
LER
ARES 28 sets

$U_a : U_s = 1 : 15, V_c = 0.5 \text{ MV}$

(S. Yoshimoto)

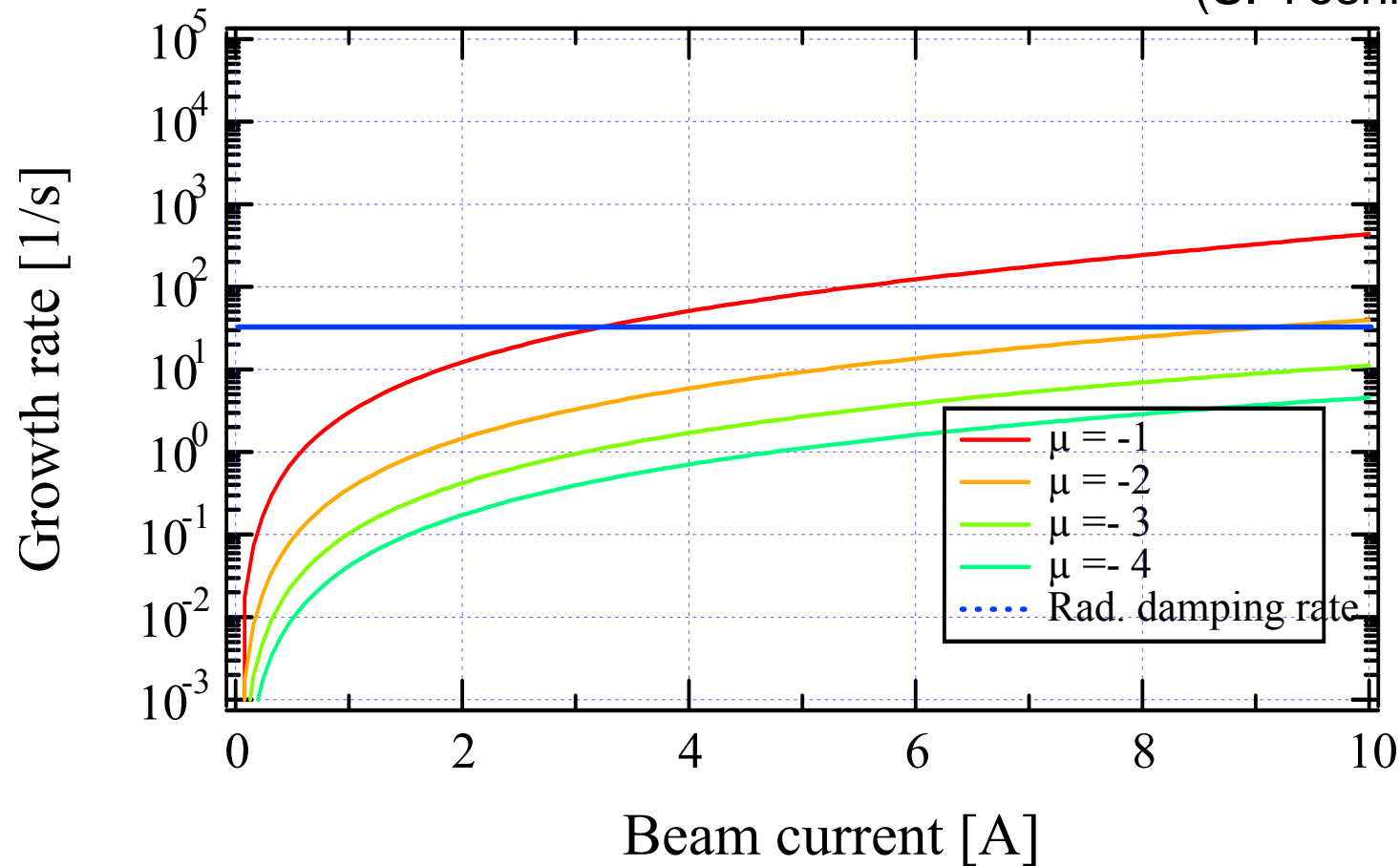


Growth Rate(3)

SuperKEKB
LER
ARES 28 sets

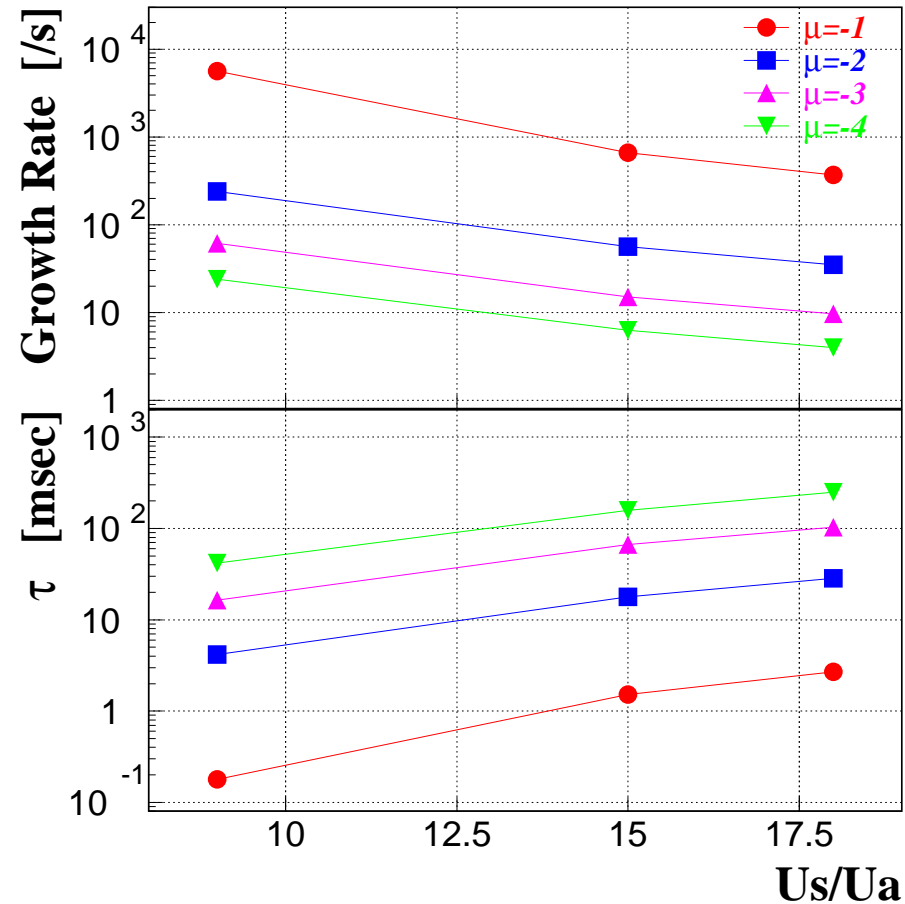
$U_a : U_s = 1 : 18, V_c = 0.5 \text{ MV}$

(S. Yoshimoto)



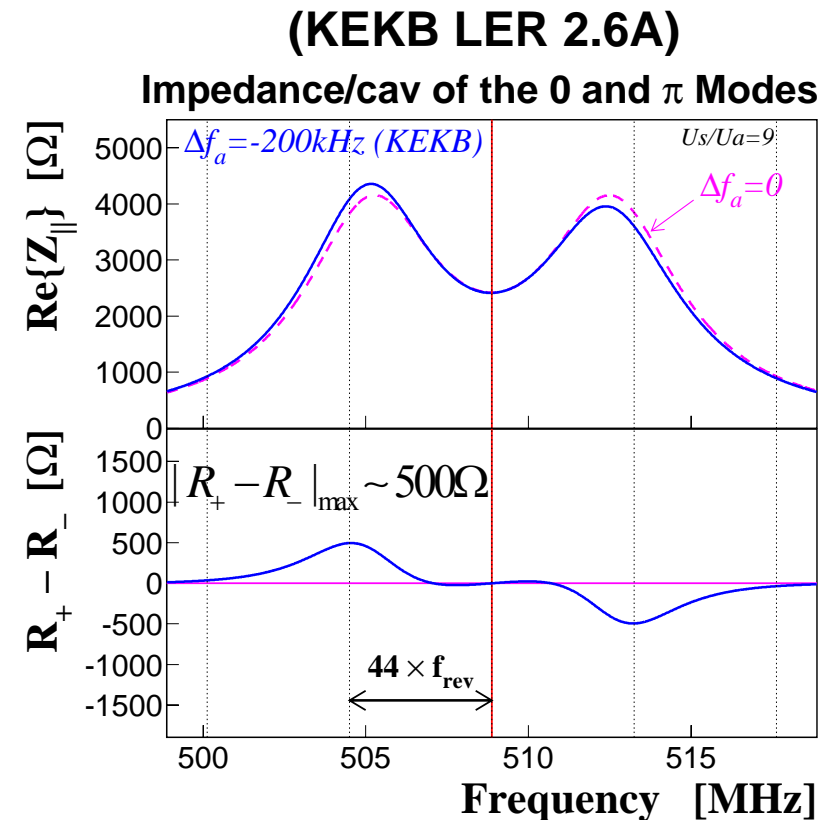
Longitudinal Coupled-bunch Instability ($\pi/2$ mode)

(SuperKEKB LER with 9.4A, ARES 28 sets, $V_c=0.5\text{MV/cav}$)



Longitudinal Coupled-bunch Instability driven by the 0 and π modes

- ✎ **Ua:Uc = 1:1 ($\Delta f_a = 0$)**
subject to the perturbation
of order of $\Delta f_a / (f_\pi - f_0)$
where $f_\pi - f_0 \propto k_a \propto \sqrt{U_s/U_a}$ (k_s : fixed)
- ✎ **Detuning: $\Delta f_a < 0$**
→ Ua>Uc (0 mode) → Asymmetric
→ Ua<Uc (π mode) → $\text{Re}\{Z_{\parallel}\}$
- ✎ **KEKB: $\Delta f_a = -200\text{kHz}$**
→ Small asymmetry on $\text{Re}\{Z_{\parallel}\}$
→ $\tau \sim 46\text{ msec}$ (no problem)
(Cf. $\tau_{\text{rad}} \sim 23\text{ msec}$)
- ✎ **Super-KEKB: $\Delta f_a = -710\text{kHz}$**
→

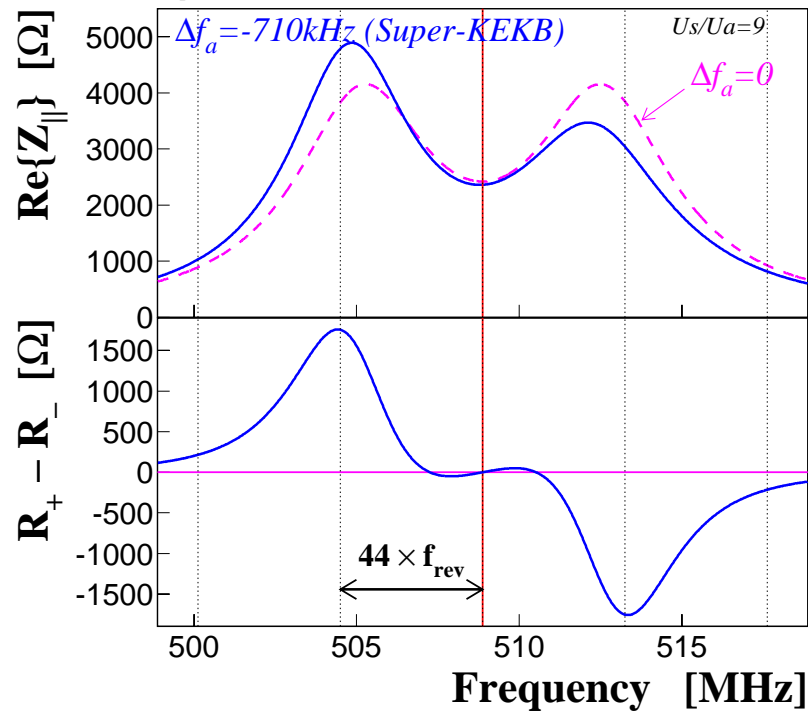


Super-KEKB

LER 9.4A
ARES 28 sets

Us/Ua=9

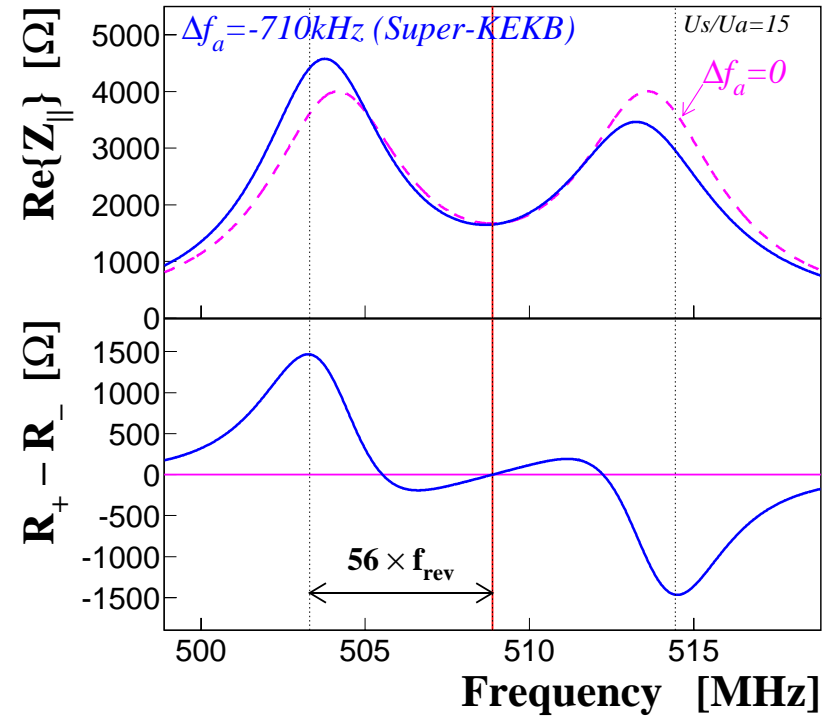
Impedance/cav of the 0 and π Modes



$\rightarrow \tau \sim 3.3 \text{ msec}$

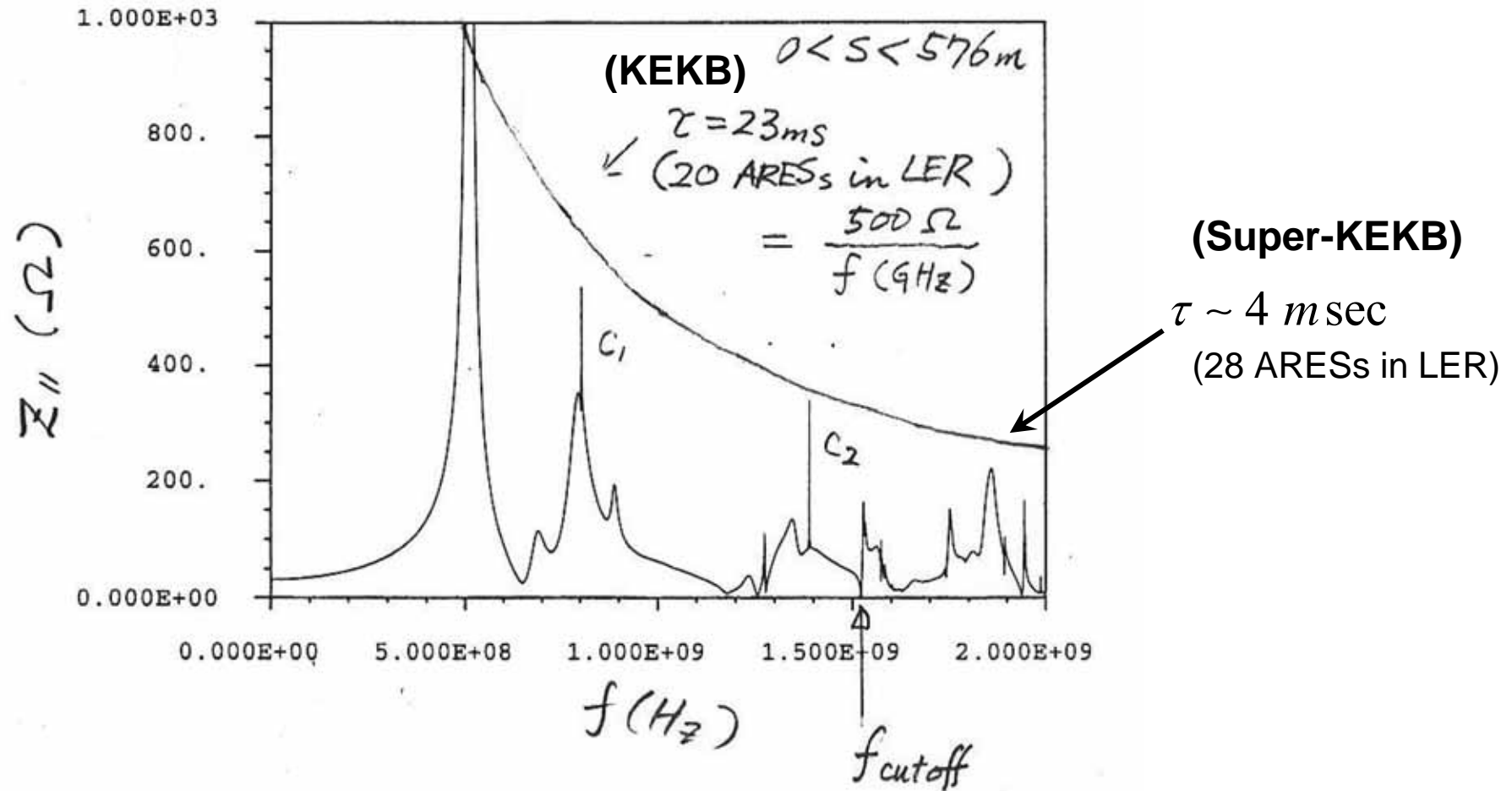
Us/Ua=15

Impedance/cav of the 0 and π Modes



$\rightarrow \tau \sim 4.0 \text{ msec}$

Longitudinal Coupled-bunch Instability driven by the HOMs



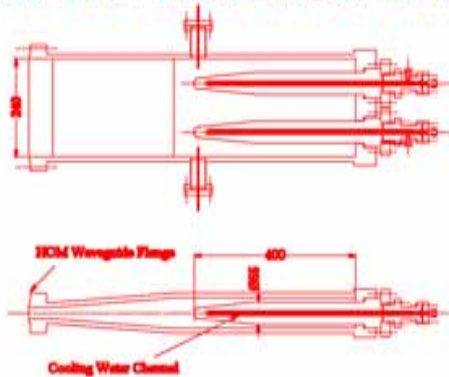
Summary on the Energy Ratio

 **Us/Ua = 9 (KEKB) → 15 (Super-KEKB)** (tentative)

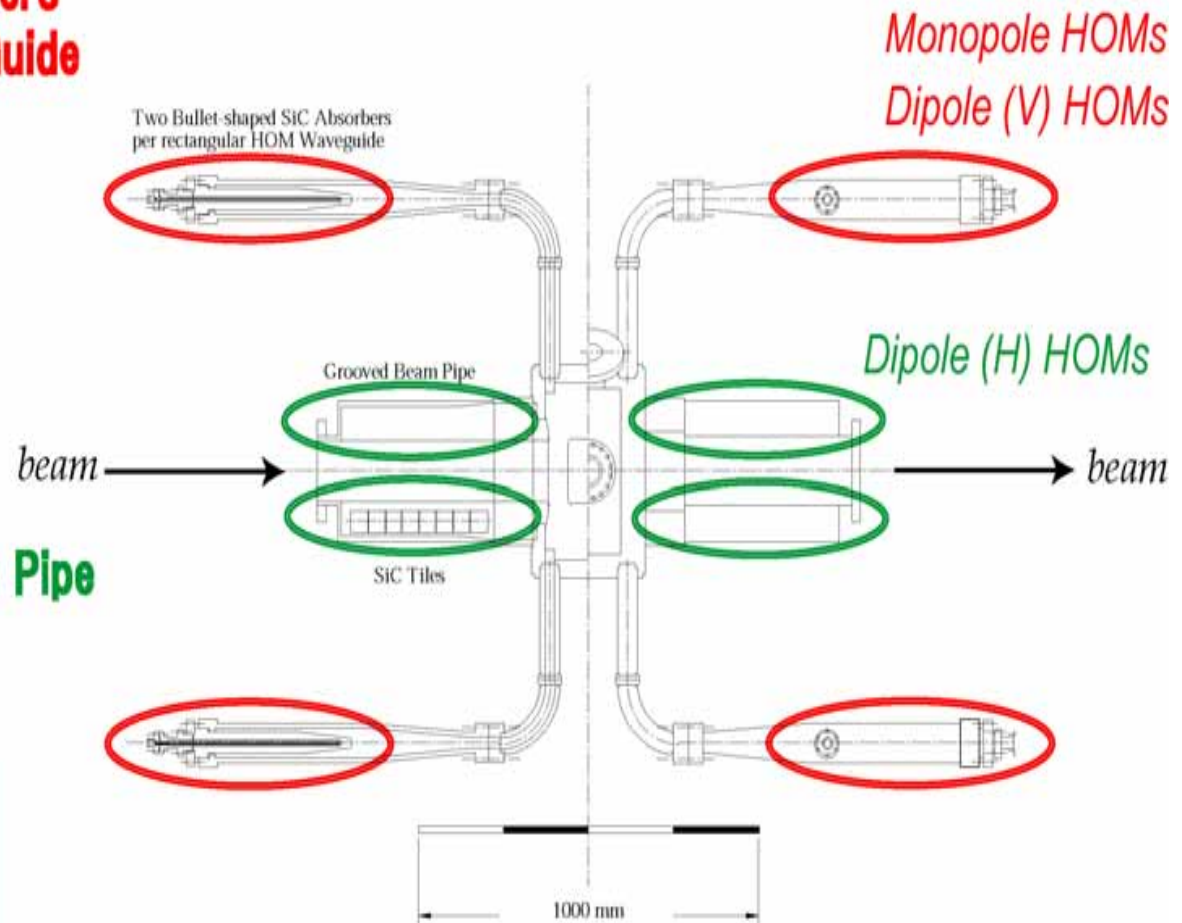
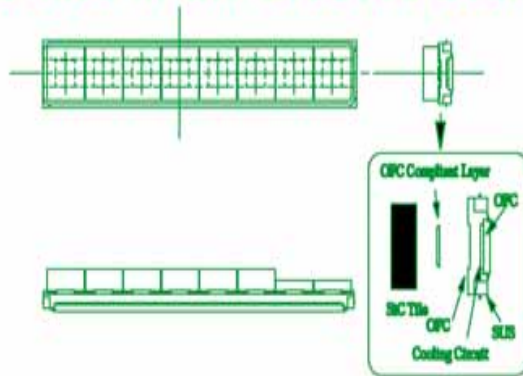
- Small modification on the window size of A-cav
- The wall loss in S-cav is acceptable.
- The CBI driven by the $\pi/2$ mode can be reduced into $\tau_{\mu=-1}^{\pi/2 \text{ mode}} > 1 \text{ m sec.}$
 - to be feedbacked by the RF control system
- The CBI driven by the 0 and π modes can be slightly reduced into $\tau_{\mu \sim -56}^{0, \pi \text{ modes}} \sim 4 \text{ m sec.}$
 - to be feedbacked by longitudinal feedback kickers
 - comparable with $\tau^{\text{HOMs}} \sim 5 \text{ m sec}$ driven by the HOMs

Upgrade of HOM loads

Two Bullet-shaped SiC-absorbers at the end of the HOM WaveGuide



SiC-tiles in the Grooved Beam Pipe



SiC Absorbers

In the HOM WaveGuide(WG)

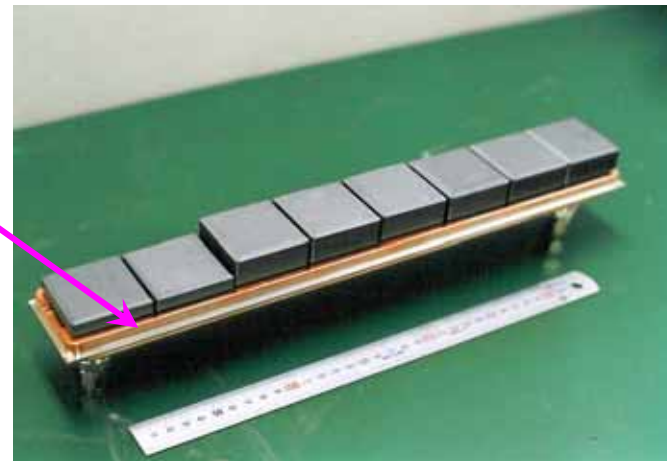
- Limit: $>3.3\text{kW/bullet}$ (HPT)
- Direct water cooling



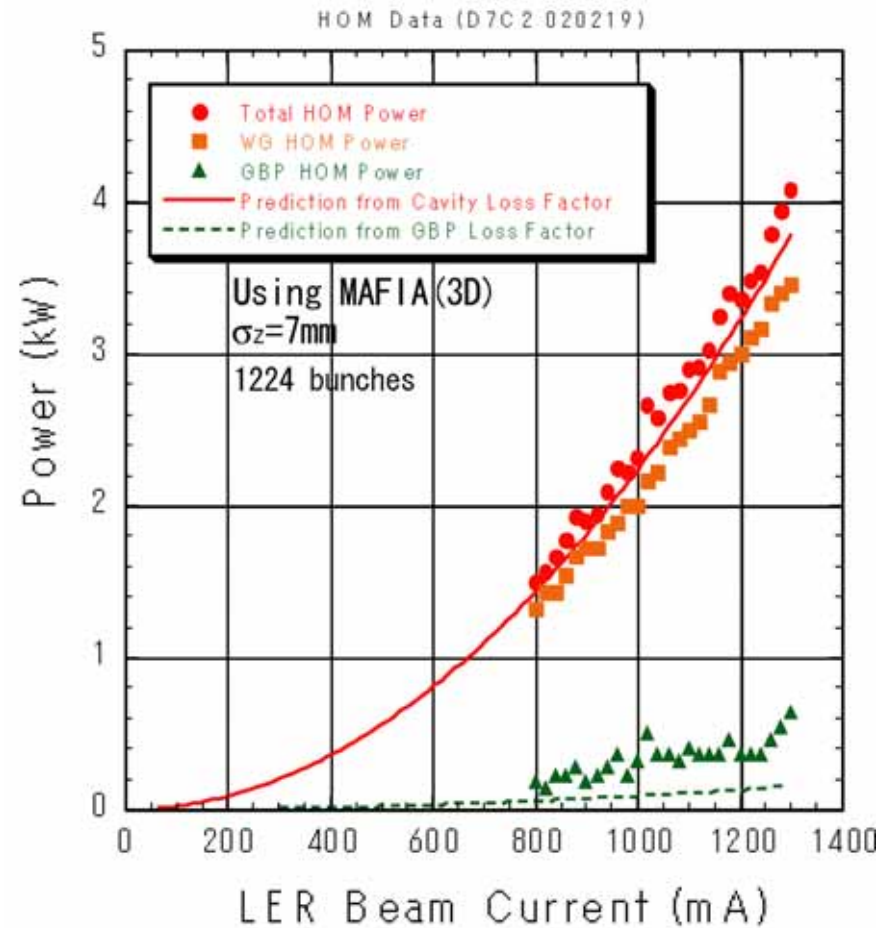
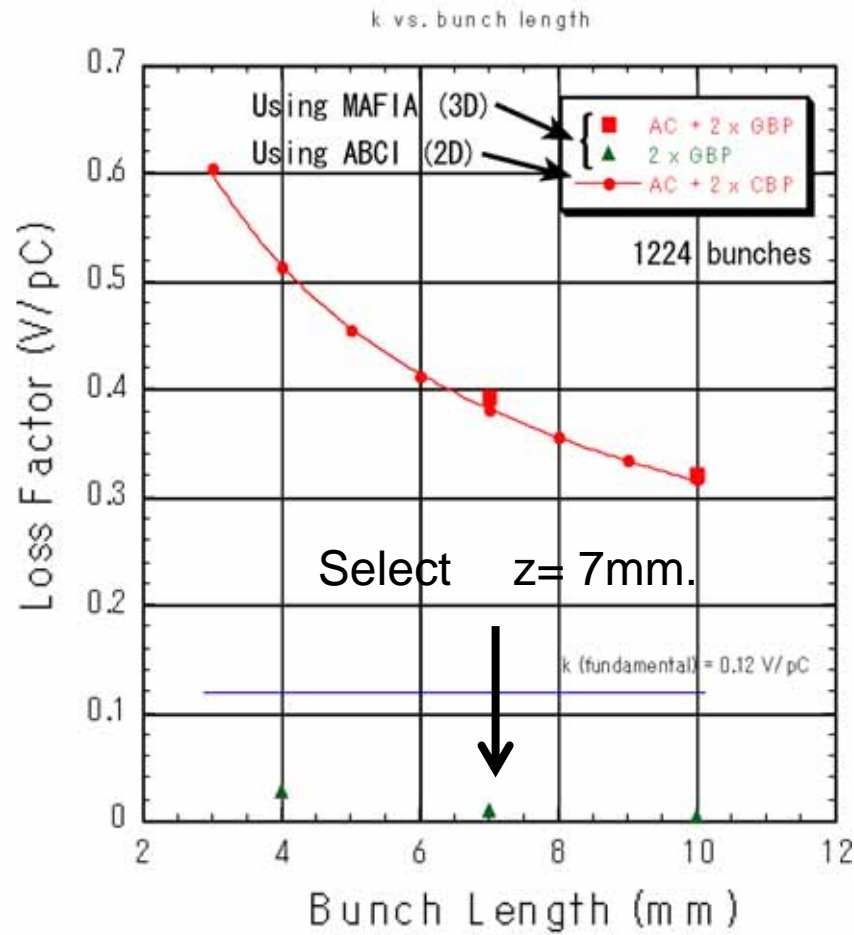
In the Grooved Beam Pipe (GBP)

- Limit: $\sim 0.5\text{kW/unit}$ (HPT)
- Indirect water cooling

Cu plate



HOM loss in KEKB



HOM Extrapolation for Super-KEKB LER

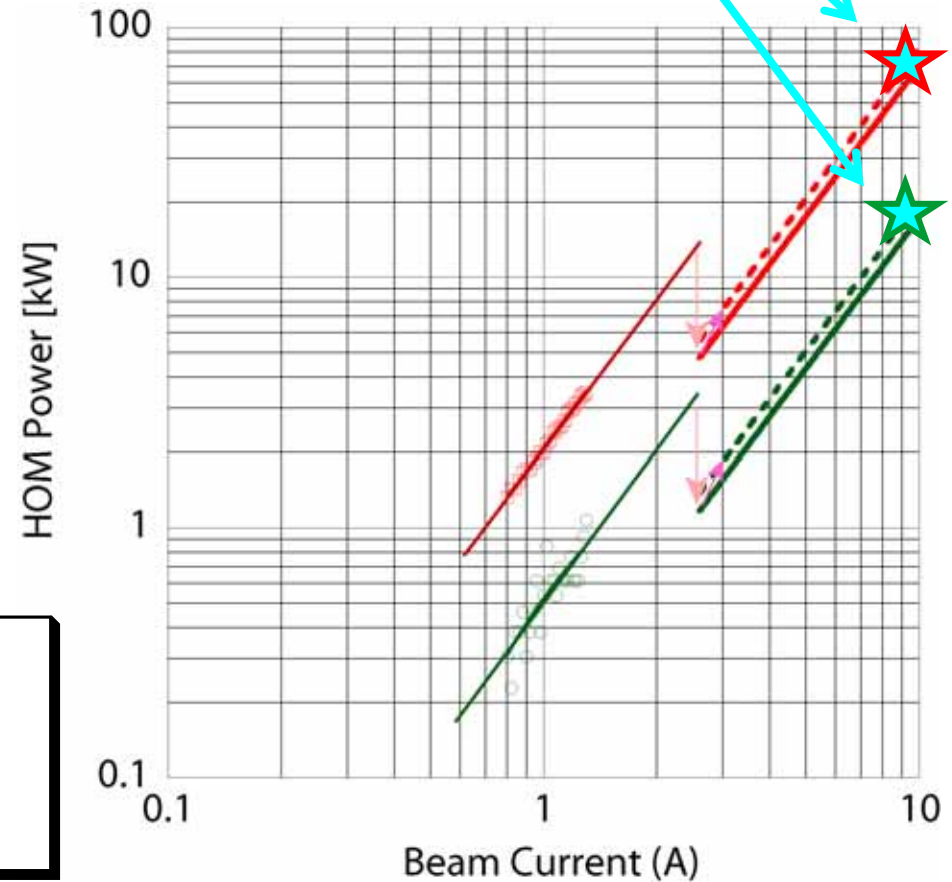
HOM in WG load (LER):
26kW/cav (HPT)
→ 80kW/cav (SuperKEKB)

- Perform HPT over 26kW
- Increase # of absorbers /WG
- Enhanced water cooling

HOM in GBP load (LER):
2kW/cav (HPT)
→ 20kW/cav (SuperKEKB)
 → Direct water cooling like...

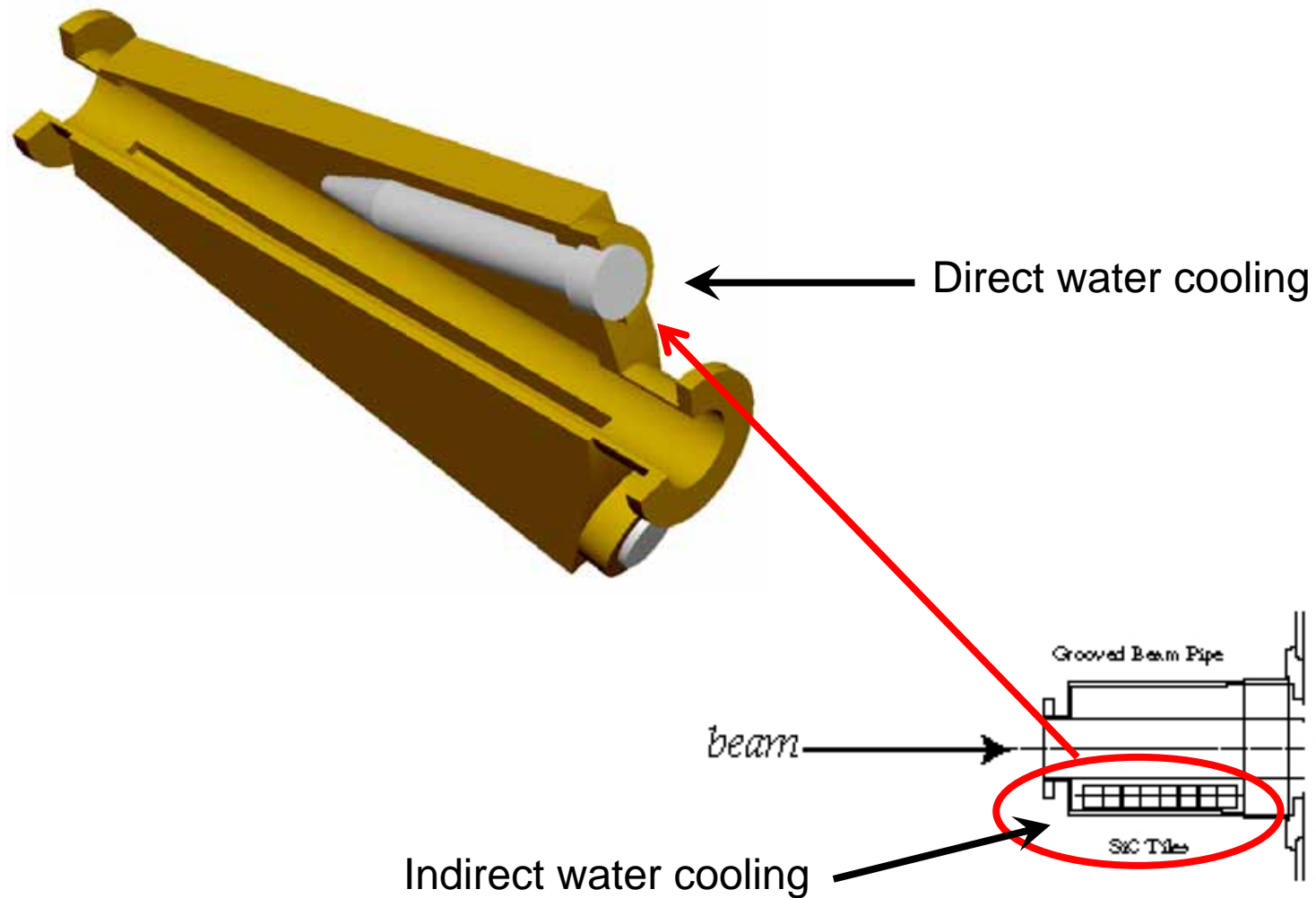
(KEKB)	(Super-KEKB)
Nb: 1224	→ 4896 (full)
σ_z : 7mm	→ 3mm

—○—	2 x GBP (Nb=1224, BL=7mm)
—■—	2 x GBP (Nb=4896, BL=4mm)
- - -○- - -	2 x GBP (Nb=4896, BL=3mm)
—□—	4 x HOM WG (Nb=1224, BL=7mm)
—■—	4 x HOM WG (Nb=4896, BL=4mm)
- - -□- - -	4 x HOM WG (Nb=4896, BL=3mm)



Winged chamber loaded with SiC Absorbers

(used in the movable-mask sections)



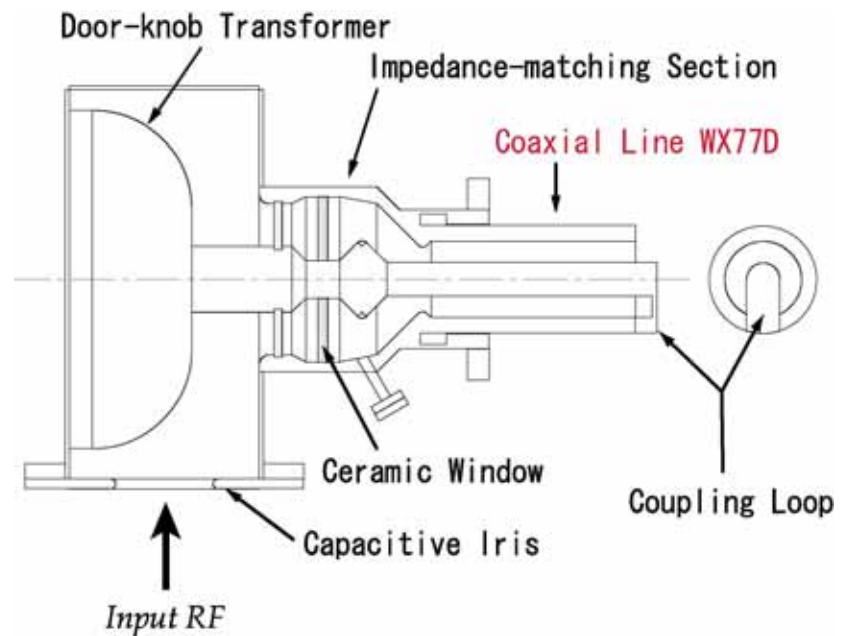
Coupler R&D

Over- and under-cut type for impedance matching

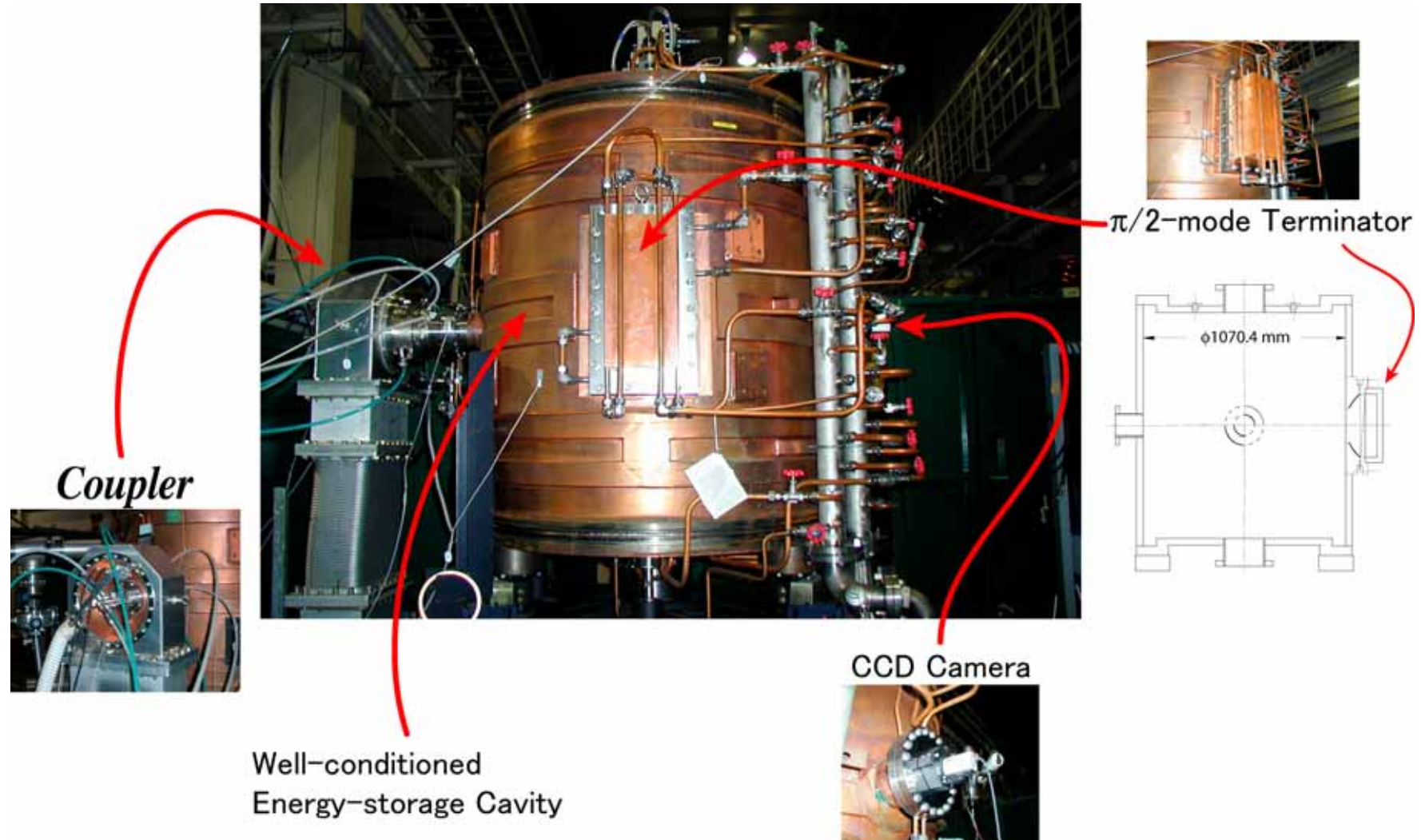
- HPT done up to 1MW in the testbench with a 1MW dummy load
- Good performance in KEKB
- But **multipacting problem in the coaxial line**

New teststand started...

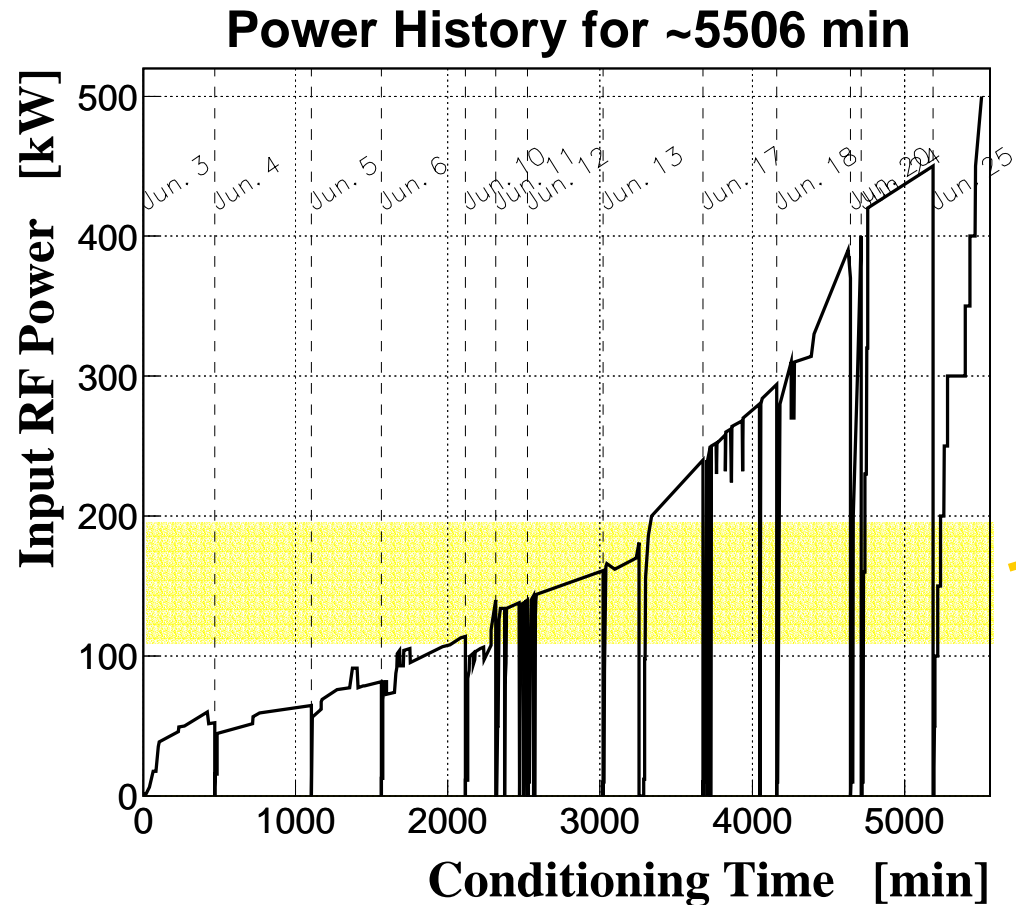
- Coupler connected to S-cav alone
- Without A-cav
- Free from multipacting discharge in A-cav



New ARES Coupler Teststand



Example of the data



Discharge seen with
the CCD camera
@ ~ 180kW

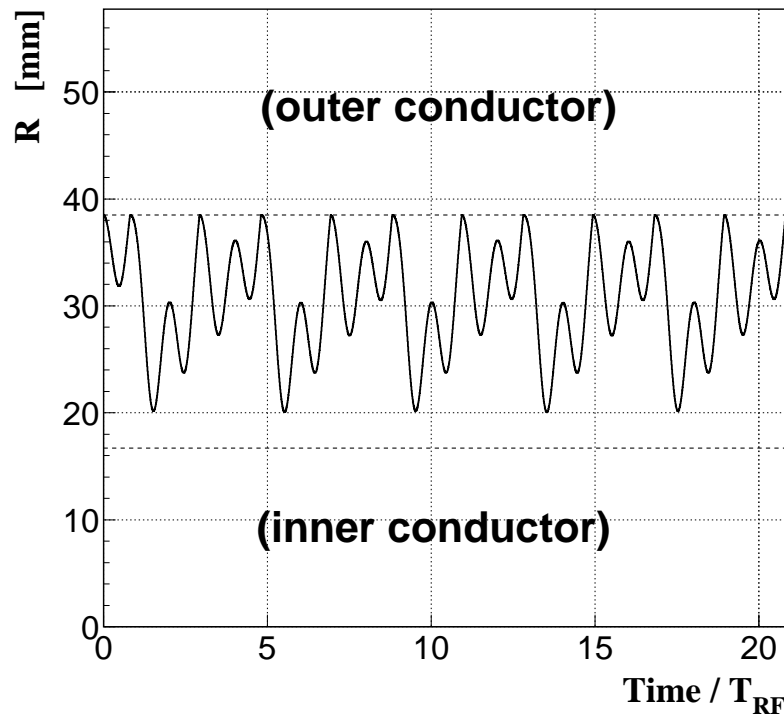


One-side multipacting
on the surface of
the outer conductor?

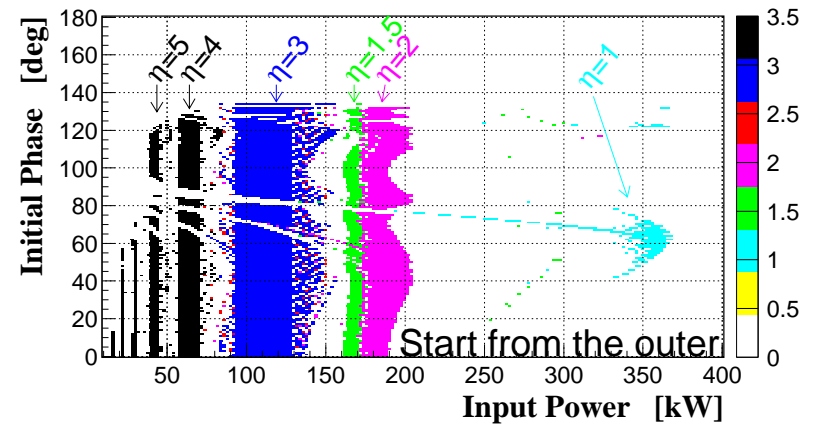
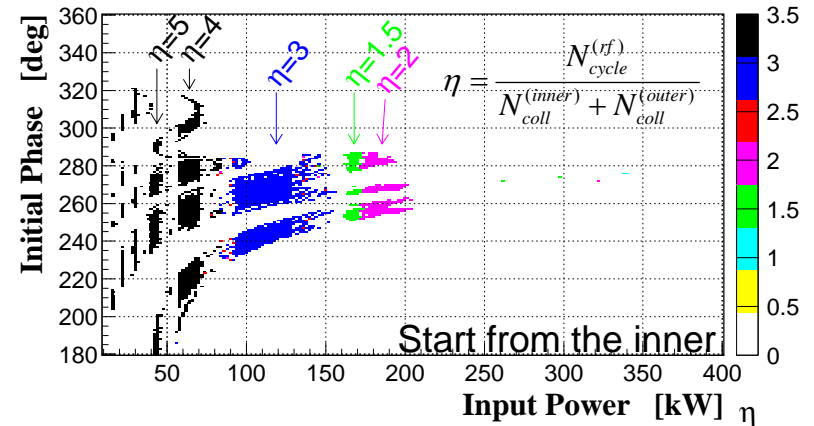
Consideration to the data

Simulation studies ongoing...

Example of the orbits



Multipacting zone from the simulation



Summary



Change of the energy ratio: $U_s/U_a = 9 \rightarrow 15$

→ No serious problems found so far

- $\tau_{\mu=-1}^{\pi/2 \text{ mode}} > 1 \text{ m sec}$ to be feedbacked by the RF control system
- $\tau_{\mu \sim -56}^{0, \pi \text{ modes}} \sim 4 \text{ m sec}$ to be feedbacked by longitudinal FB kickers
- $\tau^{\text{HOMs}} \sim 5 \text{ m sec}$



HOM-load upgrade

→ Resuming High Power Tests...

→ **Only the design of A-cav
needed to be modified**



Coupler R&D

→ HPTs and simulation studies ongoing...

Future Plan

- **2003** **A-cav design to be fixed**
- **2004** **Prototype fabrication**
- **2005** **High power tests** and **beam tests**
- **2006** **Mass production**
- **2007** **Mass production** and **Partial Installation**
during the long shutdown
- **2008** **Super-KEKB starts?**
- **2008~** **Mass production** and
Installation of remaining cavities